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Prediction of limit cycle oscillations under uncertainty using a Harmonic Balance method

Hayes, R., & Marques, S. P. (2015). Prediction of limit cycle oscillations under uncertainty using a Harmonic Balance method. *Computers & Structures*, 148, 1-13. <https://doi.org/10.1016/j.compstruc.2014.10.010>

Published in:
Computers & Structures

Document Version:
Peer reviewed version

Queen's University Belfast - Research Portal:
[Link to publication record in Queen's University Belfast Research Portal](#)

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Elsevier Editorial System(tm) for Computers and Structures
Manuscript Draft

Manuscript Number: CAS-D-13-00860R1

Title: Prediction of Limit Cycle Oscillations under Uncertainty using a Harmonic Balance Method

Article Type: Research Paper

Keywords: Aeroelasticity;
Harmonic Balance;
Limit-Cycle Oscillations;
Uncertainty;
Bifurcation;
Nonlinear

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Abstract: The Harmonic Balance method is an attractive solution for computing periodic responses and can be an alternative to time domain methods, at a reduced computational cost. The current paper investigates using a Harmonic Balance method for simulating limit cycle oscillations under uncertainty. The Harmonic Balance method is used in conjunction with a nonintrusive polynomial-chaos approach to propagate variability and is validated against Monte Carlo analysis. Results show the potential of the approach for a range of nonlinear dynamical systems, including a full wing configuration exhibiting supercritical and subcritical bifurcations, at a fraction of the cost of performing time domain simulations.

Prediction of Limit Cycle Oscillations under Uncertainty using a Harmonic Balance Method

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Abstract

The Harmonic Balance method is an attractive solution for computing periodic responses and can be an alternative to time domain methods, at a reduced computational cost. The current paper investigates using a Harmonic Balance method for simulating limit cycle oscillations under uncertainty. The Harmonic Balance method is used in conjunction with a non-intrusive polynomial-chaos approach to propagate variability and is validated against Monte Carlo analysis. Results show the potential of the approach for a range of nonlinear dynamical systems, including a full wing configuration exhibiting supercritical and subcritical bifurcations, at a fraction of the cost of performing time domain simulations.

Keywords: Aeroelasticity, Harmonic Balance, Limit Cycle Oscillations, Uncertainty, Bifurcation, Nonlinear.

1. Introduction

As design complexity increases, new materials and novel technologies are introduced to new airframes, empirical methods become increasingly difficult to apply, hence a clear need for physics based modelling tools has emerged. Aeroelasticity in particular is a good illustration of this trend and a need for physics based modelling tools has been identified by Noll *et al*[1]. Furthermore, predicting the aeroelastic stability of an aircraft should also identify the consequences of variability or uncertainty in model parameters, as discussed by Pettit[2]. Marques *et al* demonstrated the significant impact of structural variability on transonic flutter predictions[3, 4]. When nonlinearities are present, the amplitude of oscillations can become limited and limit

cycle oscillations are observed. This is a problem of considerable practical interest and is well documented for *in-service* aircraft[5, 6]. When nonlinearities are de-stabilizing (softening) a subcritical limit-cycle exists. As discussed by Stanford and Beran[7], unstable LCOs can occur below the flutter speed and lead to a hysteretic phenomenon. This type of instability is extremely undesirable because as the flutter speed is reached, the amplitude increases suddenly and significantly, as the the speed drops below the flutter point, the LCO will persist.

The presence of nonlinearities, either structural or aerodynamic, poses additional challenges both in terms of complexity and computational resources, these requirements can be exacerbated by the need to quantify the uncertainty due to unknown or variable parameters. Hence, several efforts have been made to address both these issues.

Reduced order modelling is a technique widely utilised to ease the computational burden associated with high-fidelity unsteady simulations, required to capture nonlinear effects. Proper orthogonal decomposition (POD) is commonly used to compress high order data[8, 9] and has been implemented in a reliability-based design optimisation framework (RBDO) for aeroelastic problems[10]. Volterra series can be used to model nonlinear responses with historic consideration, hence suitable for transient problems[11]. Recently, recurrent artificial neural networks (ANN), were applied to replicate an input-output relationship and can be used for nonlinear problems, such as LCOs[12], provided the model is sufficiently trained. System identification techniques using describing functions are another alternative to capture unsteady aerodynamic effects in dynamic aeroelastic problems [13, 14]. The common limitation of the methods mentioned above is the sacrifice of physical accuracy and parameter space associated with the reduction process, rendering the ROM unreliable outside the limits of the original data. The application of ROMs to uncertainty quantification (UQ) problems is in principle possible, however, the associated increase in the parameter space would require additional computational resources to generate suitable ROMs.

Two promising approaches which do not compromise the underlying physics of the oscillatory behaviour and have been applied to LCOs are: model reduction techniques based on the centre manifold theorem[15] and frequency-based techniques (finite-difference cyclic methods[16], spectral elements in time[17] and Harmonic Balance (HB) methods[6, 18, 19]). Although the HB method employs global basis functions resulting in system matrices with no sparsity, it offers better temporal convergence than spectral element and

cyclic methods[20]. Additionally, convergence problems can occur for the spectral element method during the transition between unstable and stable branches of a subcritical LCO[7], the HB method does not encounter this problem. An overview of different variations of the Harmonic Balance method, such as high-dimensional, incremental, or elliptic HB methods is given by Dimitriadis[21].

The growth in complexity associated with classical HB method for higher order nonlinear terms render it inefficient for most practical problems[18]. The High-Dimensional Harmonic Balance (HDHB) method can simplify the treatment of nonlinearities thus making it scalable for more complex problems and can subsequently offer over one order of magnitude reduction in cost[22]. The benefits of the Harmonic Balance approach deteriorate as the number of harmonics retained to solve the problem increase[23].

As for flutter, LCOs are sensitive to parametric variability, which makes the use of stochastic tools attractive to this problem. Beran *et al*[24] applied several UQ techniques to an aerofoil LCO problem, where variability was propagated using time domain and cyclic methods. To overcome the difficulties with applying stochastic methods such as Probabilistic Collocation to long time integration problem, Witteveen *et al*[25], re-cast LCO time domain results as a function of the resultant frequency. More recently, Le Meitour *et al*[26] used a non-intrusive, adaptive formulation of a generalised Polynomial Chaos Expansion (PCE) approach to 2-dimensional LCO problems, the adaptive formulation allowed for the PCE method to give reliable answers in the presence of discontinuities such as supercritical bifurcations.

In this work, an HDHB formulation is exploited to determine the LCO conditions without incurring the costs of time-accurate simulations; the paper then investigates the practicality of using the HDHB approach to propagate parametric variability using a *Non-Intrusive Polynomial Chaos* (NIPC) approach. The paper will first summarize the HDHB formulation, this is followed by the description of the probabilistic approach based on non-intrusive PCE. The impact of variability on the responses amplitudes and motion frequency is assessed and compared against Monte Carlo (MC) results (using both time domain and HDHB methods).

2. Harmonic Balance Formulation

The HB formulation used in this work was proposed by Hall *et al*[22] for time-periodic flow problems, this methodology was adapted to nonlin-

ear dynamical systems by Liu *et al*[27] and is summarised next. Consider a dynamic system with a nonlinearity in stiffness whose behaviour can be described using a simple equation of motion given by:

$$\mathbf{M}\ddot{x} + \mathbf{C}\dot{x} + \mathbf{K}x + \mathbf{K}_{nl}(x) = \mathbf{F}(x, \dot{x}, \ddot{x}, t) \quad (1)$$

Matrices \mathbf{M} , \mathbf{C} and \mathbf{K} describe the mass, damping and linear stiffness properties of the system respectively and $\mathbf{K}_{nl}(x)$ is the nonlinear component of the stiffness restoring force. The external force, \mathbf{F} can be a function of the motion of the system and/or time. Here consider the external force to be, $\mathbf{F} = \sin(\omega t)$. The solution of eq. (1) can be approximated to be a truncated Fourier series of N_H harmonics with a fundamental frequency ω .

$$x(t) \approx \hat{x}_0 + \sum_{n=1}^{N_H} (\hat{x}_{2n-1} \cos(n\omega t) + \hat{x}_{2n} \sin(n\omega t)) \quad (2)$$

The first and second derivatives of $x(t)$ with respect to time can be found to be:

$$\dot{x}(t) \approx \sum_{n=1}^{N_H} (-n\omega \hat{x}_{2n-1} \sin(n\omega t) + n\omega \hat{x}_{2n} \cos(n\omega t)) \quad (3)$$

$$\ddot{x}(t) \approx \sum_{n=1}^{N_H} (-(n\omega)^2 \hat{x}_{2n-1} \cos(n\omega t) - (n\omega)^2 \hat{x}_{2n} \sin(n\omega t)) \quad (4)$$

By substituting the Fourier series back into eq. (1) and collecting terms associated with each harmonic, a system of equations can be assembled that relate the system's dynamic properties with the Fourier coefficients. This algebraic system consists of $2N_H+1$ equations which can be conveniently displayed in vector form:

$$(\mathbf{M}\omega^2 \mathbf{A}^2 + \mathbf{C}\omega \mathbf{A} + \mathbf{K}\mathbf{I})\hat{\mathbf{Q}} + \hat{\mathbf{Q}}_{nl} - \mathbf{F}\hat{\mathbf{H}} = 0 \quad (5)$$

where:

$$\hat{\mathbf{Q}} = \begin{Bmatrix} \hat{x}_0 \\ \hat{x}_1 \\ \hat{x}_2 \\ \hat{x}_3 \\ \vdots \\ \hat{x}_{2N_H} \end{Bmatrix}_{2N_H+1}, \quad \hat{\mathbf{Q}}_{nl} = \begin{Bmatrix} \hat{K}_{nl0} \\ \hat{K}_{nl1} \\ \hat{K}_{nl2} \\ \hat{K}_{nl3} \\ \vdots \\ \hat{K}_{nl2N_H} \end{Bmatrix}_{2N_H+1} \quad \text{and} \quad \hat{\mathbf{H}} = \begin{Bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ \vdots \\ 0 \end{Bmatrix}_{2N_H+1}$$

Matrix \mathbf{A} reconstructs the Fourier series from the harmonic balancing and is shown in Appendix A. The nonlinear term Fourier coefficients, $\hat{\mathbf{K}}_{nl}$ are computed using discrete Fourier transforms (DFT). Computing these terms analytically can be cumbersome for certain types of nonlinearities such as high order polynomial terms or fluxes in CFD problems[22]. The HDHB method overcomes these issues by casting the problem in the time domain where the Fourier coefficients are related to $2N_H + 1$ equally spaced sub-time levels throughout one temporal period using a constant transformation matrix which yields:

$$\hat{\mathbf{Q}} = \mathbf{E}\tilde{\mathbf{Q}}, \quad \hat{\mathbf{Q}}_{nl} = \mathbf{E}\tilde{\mathbf{Q}}_{nl} \quad \text{and} \quad \hat{\mathbf{H}} = \mathbf{E}\tilde{\mathbf{H}} \quad (6)$$

where:

$$\tilde{\mathbf{Q}} = \begin{Bmatrix} x(t_0) \\ x(t_1) \\ \vdots \\ x(t_{2N_H}) \end{Bmatrix}, \quad \tilde{\mathbf{Q}}_{nl} = \begin{Bmatrix} K_{nl}(x(t_0)) \\ K_{nl}(x(t_1)) \\ \vdots \\ K_{nl}(x(t_{2N_H})) \end{Bmatrix} \quad \text{and} \quad \tilde{\mathbf{H}} = \begin{Bmatrix} \sin t_0 \\ \sin t_1 \\ \vdots \\ \sin t_{2N_H} \end{Bmatrix}$$

and

$$t_i = \frac{i2\pi}{2N_H + 1} (i = 0, 1, \dots, 2N_H) \quad (7)$$

Expressions for the transformation matrix \mathbf{E} and its inverse \mathbf{E}^{-1} which can be used to relate the time domain variables back to the Fourier coefficients ie. $\hat{\mathbf{Q}} = \mathbf{E}^{-1}\tilde{\mathbf{Q}}$ are shown in Appendix A. Using these transformation matrices, the system in eq. (5) can be cast in the time domain as:

$$(\mathbf{M}\omega^2\mathbf{D}^2 + \mathbf{C}\omega\mathbf{D} + \mathbf{K}\mathbf{I})\tilde{\mathbf{Q}} + \tilde{\mathbf{Q}}_{nl} - \mathbf{F}\tilde{\mathbf{H}} = \mathbf{0} = \mathbf{R} \quad (8)$$

where $\mathbf{D} = \mathbf{E}^{-1}\mathbf{A}\mathbf{E}$. Equation (8) represents the HDHB system and can be solved using either pseudo-time marching or Newton-Raphson approaches. Here, the latter is employed:

$$\mathbf{S}^{n+1} = \mathbf{S}^n - \lambda\mathbf{J}^{-1}\mathbf{R}^n \quad (9)$$

where \mathbf{S}^n is the solution vector at iteration n , λ is a relaxation parameter for increased stability. The inverse Jacobian of the system, \mathbf{J}^{-1} , is numerically approximated using finite-differences[28] and \mathbf{R}^n is the residual of eq. (8) at

iteration n , ie.

$$\mathbf{S}^n = \left\{ \begin{array}{c} \hat{x}_0 \\ \hat{x}_1 \\ \vdots \\ \hat{x}_{2N_H} \end{array} \right\}^n, \quad \mathbf{R}^n = \left\{ \begin{array}{c} R_0 \\ R_1 \\ \vdots \\ R_{2N_H} \end{array} \right\}^n \quad \text{and} \quad \mathbf{J} = \begin{bmatrix} \frac{\partial R_0}{\partial \hat{x}_0} & \cdots & \frac{\partial R_0}{\partial \hat{x}_{2N_H}} \\ \vdots & \ddots & \vdots \\ \frac{\partial R_{2N_H}}{\partial \hat{x}_0} & \cdots & \frac{\partial R_{2N_H}}{\partial \hat{x}_{2N_H}} \end{bmatrix}$$

3. Stochastic Modelling

The system of equations shown in eq. (8) can be used to describe nonlinear time periodic dynamical systems and quantities such as frequency and amplitude are easily extracted. This enables the HDHB method to be an efficient way of propagating uncertainties in time periodic, nonlinear systems. The approach used in this paper is based on a non-intrusive polynomial chaos method, where sampled points from the parameter space are used to reconstruct a ‘‘polynomial expansion’’. Consider a generic system of equations with random input parameters given by:

$$\mathcal{L}(x, t, \theta; u) = f(x, t, \theta) \quad (10)$$

where $u = u(x, t, \theta)$ is the solution and $f(x, t, \theta)$ is the source term. \mathcal{L} is a general differential operator that may contain spatial, temporal, linear or nonlinear terms. The θ denotes a random event which may describe a system parameter, an initial or boundary condition, etc. In general $\theta \in \Theta$, the set containing all possible outcomes. Therefore, θ can represent M independent, continuous, uncertain parameters, in the cases reported here $\Theta = [0, 1]^M$, where θ has mean values of 1/2 and is uniformly distributed over Θ . The solution is now a random process which can be represented as a truncated series of orthogonal polynomials, referred to as Polynomial Chaos Expansions[29]:

$$u(x, t, \theta) = a_0 \Gamma_0 + \sum_{i_1=1}^P a_{i_1} \Gamma_1(\varphi_{i_1}(\theta)) + \sum_{i_1=1}^P \sum_{i_2=1}^{i_1} a_{i_1 i_2} \Gamma_2(\varphi_{i_1}(\theta), \varphi_{i_2}(\theta)) + \sum_{i_1=1}^P \sum_{i_2=1}^{i_1} \sum_{i_3=1}^{i_2} a_{i_1 i_2 i_3} \Gamma_3(\varphi_{i_1}(\theta), \varphi_{i_2}(\theta), \varphi_{i_3}(\theta)) + \dots \quad (11)$$

where a_i are polynomial coefficients, Γ_p represents basis functions, which are in fact orthogonal polynomials of order p , based on the random variable $\varphi_{i_p} = \{\varphi_{i_1}(\theta), \varphi_{i_2}(\theta), \dots, \varphi_{i_p}(\theta)\}$. Equation (11) is usually written as:

$$u(x, t, \theta) = \sum_{j=0}^{n_b} a_j \Psi_j(\varphi(\theta)) \quad (12)$$

The order-based indices correspond to each term j in the new summation. There are several possible ways to obtain solutions to eq. (12), namely *Galerkin Projection*, *Probabilistic Collocation*, *Point Collocation* among others. Le Maître and Knio[30] provide a detailed review of techniques available. In this work, a regression based Point Collocation method is used, which requires sampling $u(x, t, \theta)$ for specific values of θ and forming the following system of equations:

$$\underbrace{\begin{bmatrix} \Psi_0(\varphi_0) & \Psi_1(\varphi_0) & \cdots & \Psi_P(\varphi_0) \\ \Psi_0(\varphi_1) & \Psi_1(\varphi_1) & \cdots & \Psi_P(\varphi_1) \\ \vdots & \vdots & \ddots & \vdots \\ \Psi_0(\varphi_P) & \Psi_1(\varphi_P) & \cdots & \Psi_P(\varphi_P) \end{bmatrix}}_{\Psi} \underbrace{\begin{bmatrix} a_0 \\ a_1 \\ \vdots \\ a_P \end{bmatrix}}_{\mathbf{a}} = \underbrace{\begin{bmatrix} u_0(\theta) \\ u_1(\theta) \\ \vdots \\ u_P(\theta) \end{bmatrix}}_{\mathbf{u}} \quad (13)$$

The solution of eq. (13) is given by:

$$\mathbf{a} = (\Psi^T \Psi)^{-1} \Psi^T \mathbf{u} \quad (14)$$

For a specified order of the polynomial, P , a set of $P + 1$ vectors φ_i for $i = 0, 1, 2, \dots, P$ are used in the approximation. The response values, \mathbf{u} , which can describe quantities such as amplitude or frequency, are obtained from sampling the probabilistic space used to define θ , Hosder *et al*[31] suggest Latin hypercube sampling, but any sampling or design of experiments technique can be used. Oversampling is usually required, resulting in an overdetermined system and a least-squares minimization problem.

The orthogonal polynomials used to define the basis functions, Ψ , depend on type of the random variables, for example in the case of normal distributions, Hermite polynomials are typically used, whereas for uniformly distributed inputs Legendre polynomials are chosen[32]. With the regression model built, Monte Carlo analysis can be used with the regression model to obtain the statistic quantities of interest, usually $10^4 - 10^6$ samples suffice to converge the mean and standard deviation to engineering accuracy.

4. Results

In this study, the effects of uncertainties in initial conditions and structural parameters of various models exhibiting periodic oscillations is investigated:- a one degree of freedom (*dof*) Duffing oscillator, a two *dof* aerofoil and a wing configuration.

4.1. Duffing Oscillator

The problem defined in Liu *et al*[27] based on the *Duffing oscillator* serves as an initial test case to validate the current HDHB implementation. It contains one nonlinear parameter, a cubic stiffness variation. Following eq. (1), the terms are:

$$\mathbf{M} = m, \mathbf{C} = 2\zeta\sqrt{km}, \mathbf{K} = k, \mathbf{K}_{nl}(x) = \beta x^3 \text{ and } \mathbf{F} = F \sin(\omega t) \quad (15)$$

where β and ζ are the cubic stiffness and damping coefficients respectively. This system is solved using an ordinary differential equation solver in MatLab (ODE45) and provides the reference time domain results used to assess the HDHB method. The application of the HDHB method yields the following system:

$$(m\omega^2\mathbf{D}^2 + 2\zeta\sqrt{km}\omega\mathbf{D} + k\mathbf{I})\tilde{\mathbf{Q}}_x + \beta\tilde{\mathbf{Q}}_x^3 - F\tilde{\mathbf{H}} = 0 \quad (16)$$

where $\tilde{\mathbf{Q}}_x$ and $\tilde{\mathbf{H}}$ are the solutions of displacement and the external force respectively at each time level. As before, $\mathbf{D} = \mathbf{E}^{-1}\mathbf{A}\mathbf{E}$ with matrices \mathbf{A} and \mathbf{E} shown in Appendix A. Equation (16) is solved using the Newton-Raphson scheme shown in section 2.

The impact of the number of harmonics employed by the HDHB method is demonstrated by the deterministic simulation of a Duffing oscillator as shown in Figure 1. It is clear that the HDHB solution will converge to the time domain result as the number of harmonics is increased and seven harmonics are sufficient in this case.

In the stochastic analysis of the Duffing oscillator two uncertain parameters are of interest, the magnitude and frequency of the external force. The additional structural parameters used here are: mass, $m = 1\text{kg}$, linear and cubic stiffness coefficients, $k = \beta = 1$ and damping ratio, $\zeta = 0.1$. The non-dimensional force magnitude, F and frequency, ω , were assigned mean values of 1.25 and 0.6 respectively and given a variation of $\pm 10\%$ using a uniform distribution.

Table 1 shows the convergence rate of the MC simulation, using the HDHB solver and the motion's the peak-to-peak amplitude as the output measure; the samples were obtained using Latin hypercube sampling (LHS), 10^4 samples give results of acceptable accuracy for this work and will be employed throughout this work.

The described PCE model was compared with the MC analysis using both time domain and HDHB approaches. A 5th order polynomial expansion was

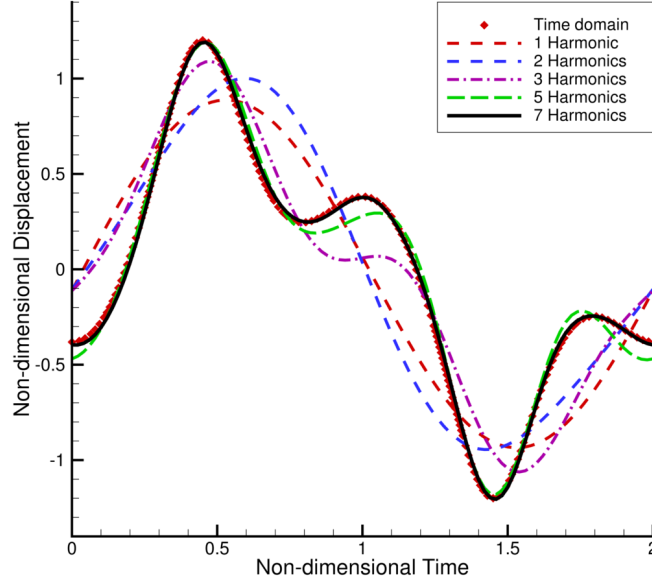


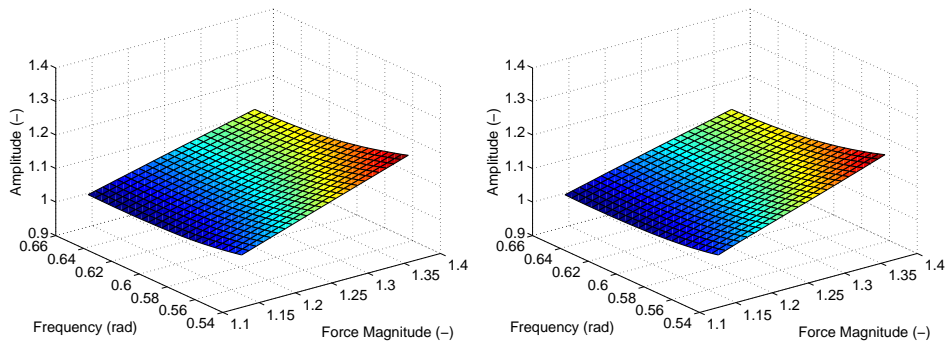
Figure 1: Number of harmonics convergence, $\omega = 0.5$ and $F = 1.25$

implemented requiring 44 samples. Figure 2 compares the response surface generated from the time accurate MC results with the HDHB-PCE. It can be seen that the amplitude of the response is affected by both the magnitude and frequency; it appears an increase in frequency, attenuates the impact of increases in the force magnitude. The histograms in Figure 2(c) show the frequencies of the amplitude and highlights the level of agreement between time domain MC and HDHB-PCE methods.

Table 2 shows the first two statistical moments for the motion's amplitude

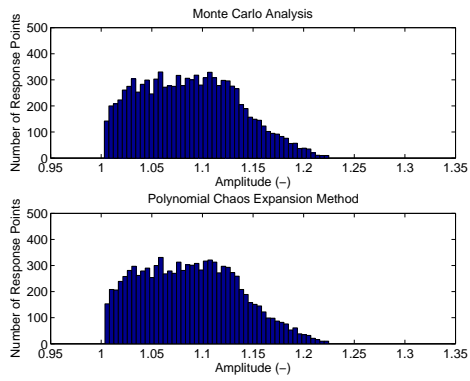
Table 1: Amplitude mean and standard deviation for Duffing oscillator - Monte Carlo sample convergence

No. of Samples	Mean	Std Deviation
100	1.088160	4.835522×10^{-2}
1,000	1.087853	4.631601×10^{-2}
10,000	1.088065	4.701828×10^{-2}
100,000	1.088070	4.702010×10^{-2}



(a) MC Response Surface

(b) HDHB PCE Response Surface



(c) Histograms of response solutions

Figure 2: Comparison of time domain MC analysis (MatLab ODE45) with HDHB PCE

Table 2: Amplitude mean and standard deviation for Duffing oscillator

	Time domain	HDHB method
MC mean	1.088173	1.088065
PCE mean	1.088032	1.088066
MC std deviation	4.701390×10^{-2}	4.701828×10^{-2}
PCE std deviation	4.703094×10^{-2}	4.707843×10^{-2}

obtained by the different methods, confirming the ability of the HDHB-PCE approach to capture the uncertainty in this system. Table 3 shows the computational cost of the problem.

4.2. Pitch-Plunge Aerofoil

In this section a typical aerofoil section restricted to pitching and plunging motions is analysed. The equations of motion for a pitch/plunge aerofoil with nonlinear restoring forces are shown in reference [33]. They can be displayed in the form of eq. (1), the terms are given as:

$$\mathbf{M} = \begin{bmatrix} x_\alpha & 1 \\ 1 & \frac{x_\alpha}{r_\alpha^2} \end{bmatrix}, \quad \mathbf{C} = \begin{bmatrix} 0 & \frac{2\zeta_\xi \bar{\omega}}{V^*} \\ \frac{2\zeta_\alpha}{V^*} \dot{\alpha} & 0 \end{bmatrix}, \quad \mathbf{K} = \begin{bmatrix} 0 & \frac{k_\xi \bar{\omega}^2}{V^{*2}} \\ \frac{k_\alpha}{V^{*2}} & 0 \end{bmatrix},$$

$$x = \begin{Bmatrix} \alpha \\ \xi \end{Bmatrix}, \quad \mathbf{K}_{nl} = \begin{bmatrix} 0 & \frac{\beta_\xi \bar{\omega}^2}{V^{*2}} \\ \frac{\beta_\alpha}{V^{*2}} & 0 \end{bmatrix} \begin{Bmatrix} \alpha^3 \\ \xi^3 \end{Bmatrix} + \begin{bmatrix} 0 & \frac{\gamma_\xi \bar{\omega}^2}{V^{*2}} \\ \frac{\gamma_\alpha}{V^{*2}} & 0 \end{bmatrix} \begin{Bmatrix} \alpha^5 \\ \xi^5 \end{Bmatrix},$$

$$\mathbf{F} = \begin{Bmatrix} -\frac{C_L(\tau)}{\pi\mu} + \frac{bP(\tau)}{mV^2} \\ \frac{2C_M(\tau)}{\pi\mu r_\alpha^2} + \frac{Q(\tau)}{mV^2 r_\alpha^2} \end{Bmatrix}$$

where ξ is the non-dimensional plunge displacement of the elastic axis, α is the pitch, C_L and C_M correspond to the lift and pitching moment coefficients respectively, $P(\tau)$ and $Q(\tau)$ are external forces and moments respectively. After the introduction of four new variables, w_1, w_2, w_3, w_4 which partially

describe the aerodynamic and external forces characterised by \mathbf{F} , the equations of motion can be written as:

$$c_0\xi'' + c_1\alpha'' + c_2\xi' + c_3\alpha' + c_4\xi + c_{5_\beta}\xi^3 + c_{5_\gamma}\xi^5 + c_6\alpha + c_7w_1 + c_8w_2 + c_9w_3 + c_{10}w_4 = f(t^*) \quad (17)$$

$$d_0\xi'' + d_1\alpha'' + d_2\alpha' + d_3\alpha + d_{4_\beta}\alpha^3 + d_{4_\gamma}\alpha^5 + d_5\xi' + d_6\xi + d_7w_1 + d_8w_2 + d_9w_3 + d_{10}w_4 = g(t^*) \quad (18)$$

where $f(t^*)$ and $g(t^*)$ represent the remainder of the generalised aerodynamic forces and damp out with time hence are not part of the periodic solution. The time domain solutions are obtained by an explicit, fourth-order Runge-Kutta scheme[34, 35, 24, 36]. The nonlinearity is considered only in the pitch *dof* ($c_{5_\beta} = c_{5_\gamma} = 0$). Expressions for the of the remainder coefficients can be found in [34]. Implementing the HDHB approach to eqs. (17) and (18), a system in the frequency domain can be created:

$$\begin{cases} (c_0\omega^2\mathbf{A}^2 + c_2\omega\mathbf{A} + c_4\mathbf{I})\hat{\mathbf{Q}}_\xi + (c_1\omega^2\mathbf{A}^2 + c_3\omega\mathbf{A} + c_6\mathbf{I})\hat{\mathbf{Q}}_\alpha + c_7\hat{\mathbf{Q}}_{w_1} + \\ + c_8\hat{\mathbf{Q}}_{w_2} + c_9\hat{\mathbf{Q}}_{w_3} + c_{10}\hat{\mathbf{Q}}_{w_4} = 0 \\ (d_0\omega^2\mathbf{A}^2 + d_5\omega\mathbf{A} + d_6\mathbf{I})\hat{\mathbf{Q}}_\xi + (d_1\omega^2\mathbf{A}^2 + d_2\omega\mathbf{A} + d_3\mathbf{I})\hat{\mathbf{Q}}_\alpha + d_7\hat{\mathbf{Q}}_{w_1} + \\ + d_8\hat{\mathbf{Q}}_{w_2} + d_9\hat{\mathbf{Q}}_{w_3} + d_{10}\hat{\mathbf{Q}}_{w_4} + d_{4_\beta}\hat{\mathbf{Q}}_{\beta_\alpha} + d_{4_\gamma}\hat{\mathbf{Q}}_{\gamma_\alpha} = 0 \\ (\omega\mathbf{A} + \epsilon_1\mathbf{I})\hat{\mathbf{Q}}_{w_1} - \hat{\mathbf{Q}}_\alpha = 0 \\ (\omega\mathbf{A} + \epsilon_2\mathbf{I})\hat{\mathbf{Q}}_{w_2} - \hat{\mathbf{Q}}_\alpha = 0 \\ (\omega\mathbf{A} + \epsilon_1\mathbf{I})\hat{\mathbf{Q}}_{w_3} - \hat{\mathbf{Q}}_\xi = 0 \\ (\omega\mathbf{A} + \epsilon_2\mathbf{I})\hat{\mathbf{Q}}_{w_4} - \hat{\mathbf{Q}}_\xi = 0 \end{cases} \quad (19)$$

By substituting the last 4 equations of system 19 into the first 2 and replacing $\hat{\mathbf{Q}}_{\beta_\alpha}$ with $\mathbf{E}(\mathbf{E}^{-1}\hat{\mathbf{Q}}_\alpha)^3$ and $\hat{\mathbf{Q}}_{\gamma_\alpha}$ with $\mathbf{E}(\mathbf{E}^{-1}\hat{\mathbf{Q}}_\alpha)^5$ the system can be further reduced to[27]:

$$(\mathbf{A}_2 - \mathbf{B}_2\mathbf{B}_1^{-1}\mathbf{A}_1)\hat{\mathbf{Q}}_\alpha + d_{4_\beta}\mathbf{E}(\mathbf{E}^{-1}\hat{\mathbf{Q}}_\alpha)^3 + d_{4_\gamma}\mathbf{E}(\mathbf{E}^{-1}\hat{\mathbf{Q}}_\alpha)^5 = 0 \quad (20)$$

where the matrices \mathbf{A}_\bullet and \mathbf{B}_\bullet are given by eqs. A.1-A.4.

4.2.1. Supercritical Bifurcations

Unlike the Duffing oscillator, the frequency of the response is not constrained, hence it must be treated as a variable in conjunction with the amplitude properties in order to capture the behaviour of the system. This is achieved by setting $\hat{\alpha}_1 = 0$ which will affect only the phase of the solution

thus creating a system of $2N_H + 1$ equations with $2N_H + 1$ unknowns. The frequency can then be simultaneously solved along with the Fourier coefficients using the Newton-Raphson scheme. The solution and residual vectors are now given by:

$$\mathbf{S}^n = \begin{pmatrix} \omega \\ \hat{\alpha}_0 \\ \hat{\alpha}_2 \\ \vdots \\ \hat{\alpha}_{2N_H} \end{pmatrix}^n, \quad \mathbf{R}^n = \begin{pmatrix} R_1 \\ R_0 \\ R_2 \\ \vdots \\ R_{2N_H} \end{pmatrix}^n$$

The system parameters used for this case are $\bar{\omega} = 0.2$, $\mu = 100$, $a_h = 0.5$, $x_\alpha = 0.25$, $r_\alpha = 0.5$, $\zeta_\alpha = \zeta_\xi = 0$ and $\gamma_\alpha = 0$. A $\pm 10\%$ variation following a uniform distribution was imposed on the linear and cubic stiffness coefficients, with nominal values of 1.0 and 3.0 respectively. This nominal case was simulated over a range of velocities for different lengths of time, to determine convergence of the time domain solver as shown in Figure 3. As the velocity increases towards the bifurcation point, the time domain solver requires increasingly longer time integration periods to damp out residual oscillations. For conditions beyond the bifurcation point, 2500 seconds suffice to achieve the final periodic orbit, hence this value was used for the non-deterministic calculations. Note that for the HDHB method, one harmonic is shown to be adequate for this investigation.

For a given velocity the system undergoes a supercritical Hopf-bifurcation, this is shown in Figure 4. The time domain and HDHB method show good agreement with exception to the bifurcation region due to the large cost associated with achieving a well-defined discontinuity. The presence of the bifurcation point requires a higher order polynomial capable of capturing the abrupt change in behaviour adequately. The effects of PCE order near the bifurcation point is shown by Figure 5, hence, an 11th order PCE requiring 194 samples was employed in the aerofoil investigation. The response frequency is shown in Figure 4. Note that there is a linear relationship between the linear stiffness coefficient and frequency for low values of linear stiffness, where LCOs exist. When no LCO exists, ie. amplitude is zero, frequencies with no physical meaning are generated which can have an adverse affect on the PCE performance. The histograms in Figure 6 reflect this limitation by the PCE when discontinuities are present.

Figure 7(a) shows the reference time domain response with respect to the

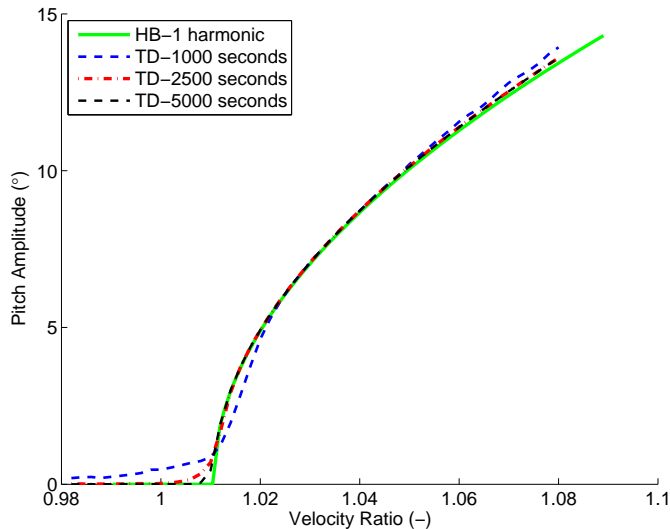


Figure 3: Convergence of time domain solver

deterministic case computed by a velocity sweep. It is evident that there is more variation present at lower velocities, this is due to increased sensitivity of the system close to the flutter speed (represented by the region of highest gradient). In this region, the linear stiffness has a larger effect on the stability of the system. The cubic stiffness impacts the amplitude as velocity increases because of the cubic relationship with displacement, but in this case the linear stiffness is the dominant factor. The HDHB method shows variations at all the velocities which are very similar to the time domain results. The PCE is shown to perform better at the higher velocities where only smooth behaviour is exhibited. The mean values extracted from the PCE analysis agree well with the MC time domain samples. The computational times for the aerofoil are shown in Table 3.

4.2.2. Subcritical Bifurcations

The subcritical case investigated here is similar to that used by Millman *et al*[37]. The desired subcritical behaviour is exhibited when the nonlinear term consists of a hardening pentic term, (+) and a softening cubic term, (-). The uncertain variables are the pentic stiffness coefficient, γ_α , and the initial pitch amplitude, α_0 , with nominal values of 20 and 15° respectively. A $\pm 10\%$ variation from a uniform distribution was assigned to the pentic stiffness coefficient, γ_α , and a $\pm 50\%$ variability of initial pitch amplitude, α_0 , was

also added using a uniform distribution. The cubic stiffness coefficient was now softening, ie. $\beta_\alpha = -3$. PCE was not employed in the subcritical case as the hysteresis provides three disconnected response surfaces which cannot be sufficiently modelled without the partitioning of the random space[26]. Only the HDHB method was employed here as the time integration scheme that was implemented was unable to converge to the unstable branch of the subcritical LCO. Results are shown in Figure 8. The distribution of samples coincides with the different branches of the deterministic case, a large proportion of samples exhibit LCO behaviour below the bifurcation point. The variability in the chosen uncertain parameters has a more limited impact on the LCO amplitude than in the supercritical case, as shown by Figure 8. For a velocity ratio of 0.96, Figure 9(a) shows how lower values for the pentic stiffness coefficient lead to a wider range of initial pitch values

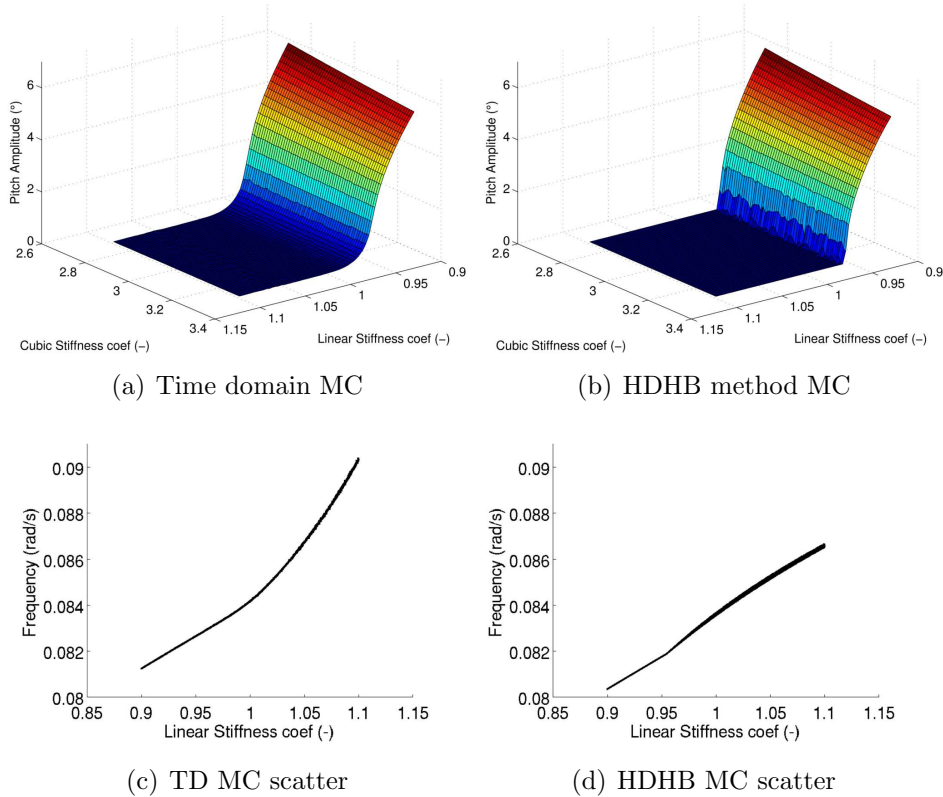


Figure 4: Supercritical Bifurcation at Linear Flutter Speed

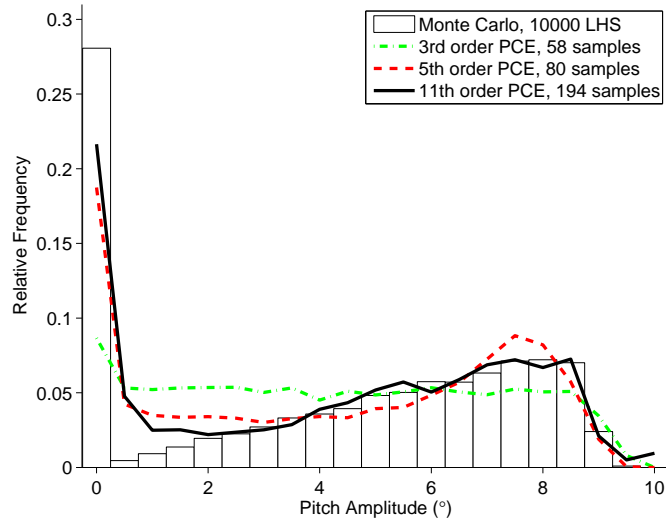


Figure 5: Histogram for Monte-Carlo and PCE, Supercritical Bifurcation at $Velocity Ratio = 1.02$

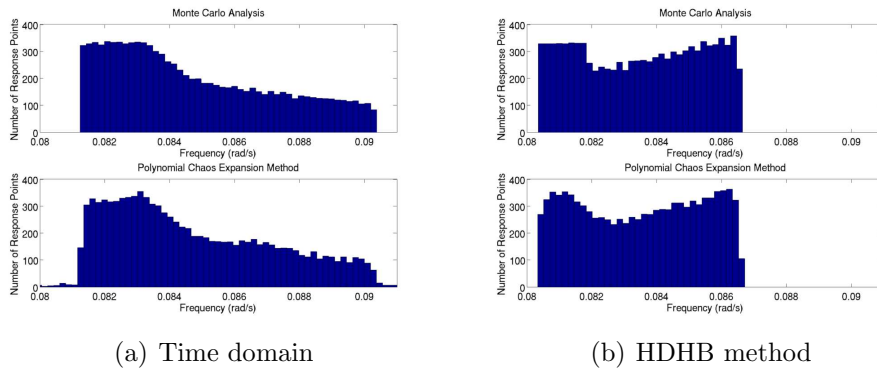


Figure 6: Frequency Variation - Supercritical Bifurcation at Linear Flutter Speed

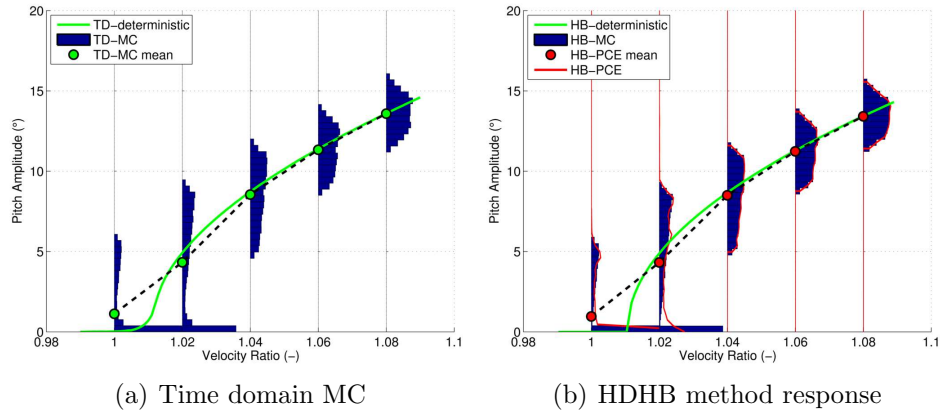


Figure 7: Supercritical Bifurcation Response

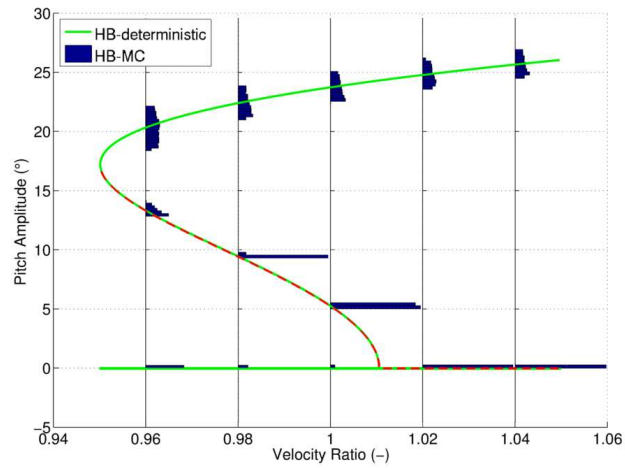


Figure 8: Subcritical Bifurcation, Monte-Carlo from HDHB

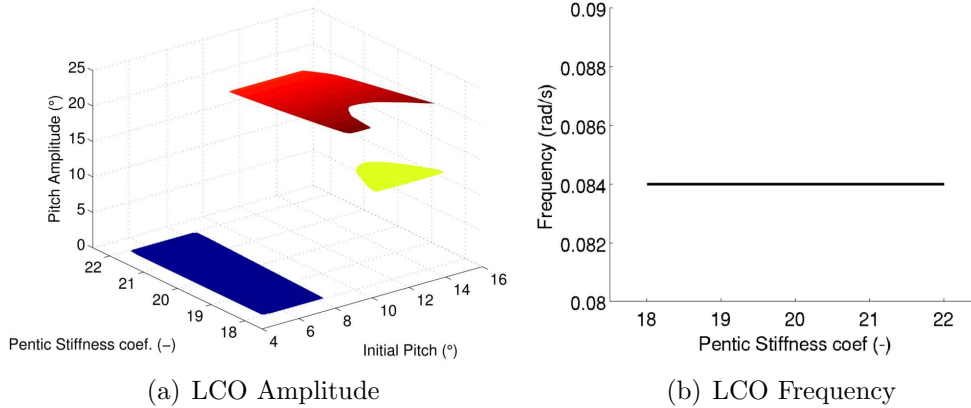


Figure 9: Amplitude and Frequency Response, *Velocity Ratio* = 0.96

to converge to the unstable branch, this subcritical behaviour is observed in the vicinity of the nominal initial pitch value. Figure 9(b) shows the LCO frequency response of the aerofoil where the two LCO branches are characterised by the same frequency. Contrary to secondary bifurcations where two stable LCOs exist with different frequencies[19], the subcritical branch is unstable and is not a true physical solution, hence any point on this branch subsequently jumps to the stable upper branch.

4.3. Golland wing

The Golland wing provides a relatively simple 3D model exhibiting several complex aeroelastic phenomenon that are challenging to engineering prediction methods. The wing has a rectangular plan-form with a span of $20ft$ and $6ft$ chord. The finite element model of the heavy version of the Golland wing is described in [38] and is shown in Figure 10(a). The structural model used in this work includes localised nonlinearities between the tip store attachment stiffness and the wing. The nonlinearities are in the form of polynomial laws for spring elements in the translational z -direction (K_z), and the rotational y -direction (K_{ry}) degrees of freedom which were shown to be the most sensitive by reference[15]. The equations of motion for the Golland wing take the same form as eq. (1). The external forces, \mathbf{F} acting on the wing are aerodynamic in nature. NASTRAN computes these forces in the modal domain using Doublet-Lattice method. Thus the wing is analysed in the modal domain, this also significantly reduces the complexity of the problem[39].

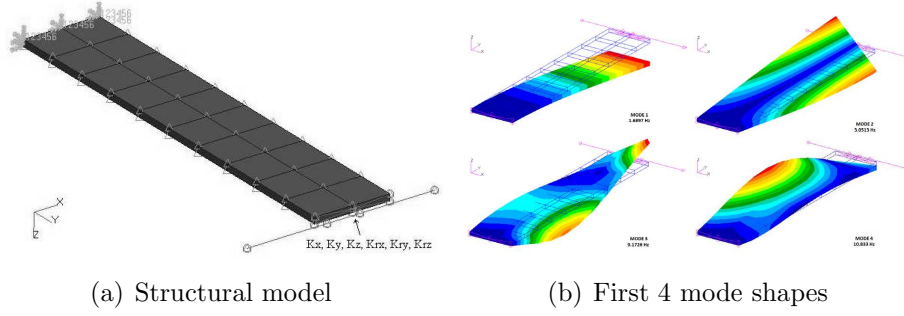


Figure 10: Goland wing

The transformation between the physical and modal space[40] is given as $\{x\} = [\Phi] \{\mathbf{q}\}$, where Φ is the truncated matrix of eigenvectors, (n_m modes, extracted from NASTRAN) and \mathbf{q} is a vector of n_m modal coordinates.

The aerodynamic data is only computed for a range of discrete reduced frequencies so it is represented as a rational function to maintain validity for all values within this range[41]. For this investigation only four structural modes are considered and are shown in Figure 10(b). The system in the modal domain with modal coordinates, \mathbf{q} is given as[15, 19]:

$$\tilde{\mathbf{M}}_\phi \ddot{\mathbf{q}} + \tilde{\mathbf{C}}_\phi \dot{\mathbf{q}} + \tilde{\mathbf{K}}_\phi \mathbf{q} + \mathbf{K}_{nl}(\mathbf{q}) = \frac{\rho V^2}{2} \sum_{i=1}^{n_i} [\mathbf{A}_{i+2}] \dot{\mathbf{q}}_{a_i} \quad (21)$$

where $\tilde{\mathbf{M}}_\phi$, $\tilde{\mathbf{C}}_\phi$ and $\tilde{\mathbf{K}}_\phi$ are the aeroelastic system mass, damping and linear stiffness matrices, given by eq. B.1-B.3. $\mathbf{K}_{nl}(\mathbf{q})$ is the nonlinear force given by eq. B.4, \mathbf{A}_\bullet represents the rationally approximated components of the generalised aerodynamic matrix extracted from NASTRAN. $\dot{\mathbf{q}}_{a_i}$ are augmented terms arising from the Laplace domain treatment of the generalised aerodynamic matrix and have the relationship:

$$\ddot{\mathbf{q}}_{a_i} = \dot{\mathbf{q}} - \frac{V}{b} \eta_i \dot{\mathbf{q}}_{a_i} \quad (22)$$

The state space equation which is solved in the time domain is constructed by combining eqs. (21) and (22), leading to:

$$\dot{\mathbf{w}} + \mathbf{A}_s \mathbf{w} + \mathbf{u} = \mathbf{0} = \mathbf{R} \quad (23)$$

where

$$\mathbf{w} = \begin{pmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \\ -\mathbf{A}_3 \dot{\mathbf{q}}_{a_1} \\ -\mathbf{A}_4 \dot{\mathbf{q}}_{a_2} \\ \vdots \\ -\mathbf{A}_{n_l+2} \dot{\mathbf{q}}_{a_{n_l}} \end{pmatrix}, \quad \mathbf{u} = \begin{pmatrix} \mathbf{0} \\ \tilde{\mathbf{M}}_\phi^{-1} \Phi^T \mathbf{K}_{nl}(\mathbf{q}) \\ \mathbf{0} \\ \mathbf{0} \\ \vdots \\ \mathbf{0} \end{pmatrix}$$

and

$$\mathbf{A}_s = \begin{bmatrix} \mathbf{0} & -\mathbf{I} & \mathbf{0} & \dots & \dots & \mathbf{0} \\ \tilde{\mathbf{M}}_\phi^{-1} \tilde{\mathbf{K}}_\phi & \tilde{\mathbf{M}}_\phi^{-1} \tilde{\mathbf{C}}_\phi & \tilde{\mathbf{M}}_\phi^{-1} \frac{\rho V^2}{2} \mathbf{I} & \dots & \dots & \tilde{\mathbf{M}}_\phi^{-1} \frac{\rho V^2}{2} \mathbf{I} \\ \mathbf{0} & \mathbf{A}_3 & \frac{V}{b} \eta_1 \mathbf{I} & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_4 & \mathbf{0} & \frac{V}{b} \eta_2 \mathbf{I} & \ddots & \vdots \\ \vdots & \vdots & \vdots & \ddots & \ddots & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_{n_l+2} & \mathbf{0} & \dots & \mathbf{0} & \frac{V}{b} \eta_{n_l} \mathbf{I} \end{bmatrix}$$

Applying the HDHB method to eq. (21) yields the system:

$$\left[\tilde{\mathbf{M}}_\phi \mathbf{E}_{acc}^{-1} + \tilde{\mathbf{C}}_\phi \mathbf{E}_{vel}^{-1} + \tilde{\mathbf{K}}_\phi \mathbf{E}_{def}^{-1} \right] \hat{\mathbf{Q}}_\phi + \mathbf{E}_{def}^{-1} \hat{\mathbf{K}}_{nl} - \frac{\rho V^2}{2} \sum_{i=1}^{n_l} [\mathbf{A}_{i+2}] \mathbf{E}_{def}^{-1} \hat{\mathbf{Q}}_{a_i} = 0 \quad (24)$$

\mathbf{E}_{acc}^{-1} , \mathbf{E}_{vel}^{-1} and \mathbf{E}_{def}^{-1} are transformation matrices shown in Appendix B. The complexity of both the nonlinear stiffness force, $\{\hat{\mathbf{K}}_{nl}\}$ and the decomposed generalised aerodynamic vectors, $\{\hat{\mathbf{Q}}_{a_i}\}$ prevent the straightforward representation of these terms in the frequency domain. Subsequently system (24) is a time domain representation of the problem, where the nonlinear terms are represented as reconstructed Fourier series, the Fourier coefficients are formed using discrete Fourier transforms (DFT), computed numerically from the expressions shown in eqs. B.9-B.14. Equation (24) is solved simultaneously for $2N_H + 1$ equally spaced time steps across one period with $t_i = \frac{i2\pi}{2n_H+1}$, ($i = 0, 1, \dots, 2N_H$) to maintain temporal accuracy. A Newton-Raphson scheme is employed and as in the previous cases; the response frequency is maintained as a variable by locking the *cosine* Fourier coefficient of the first harmonic of the first mode to zero.

4.3.1. Supercritical Bifurcations

Although global properties of the structure remain within a reasonably small tolerance, localised structural properties between different units can

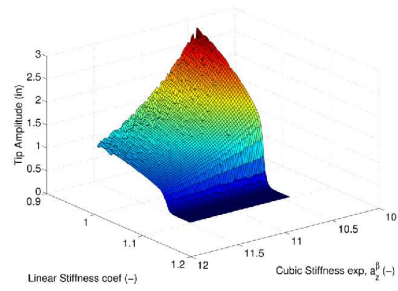
vary substantially[42]. The cubic stiffness nonlinearity is varied to represent this variability and is consistent with reference[15] where values over a range of orders of magnitude are chosen.

For this case the linear stiffness matrix, $\tilde{\mathbf{K}}_\phi$ is multiplied by a scalar linear stiffness coefficient given a value of $1 \pm 10\%$, the cubic stiffness coefficient in the rotational *dof* about the y axis was given a value of 10^{10} . The cubic stiffness in the z direction, β_z is defined by the expression, $10^{a_z^\beta}$, where the exponent, a_z^β was the second uncertain parameter with a uniform distribution resulting in a variation of $10.95 \pm 5\%$. The damping matrix, $\tilde{\mathbf{C}}_\phi$ is given a damping coefficient of 0.1. The response surfaces defined by these uncertainties are displayed in Figure 11. As in the aerofoil case, the time domain method does not reach a fully periodic state within the allowed computational time, shown by the scatter of points in the response surface. Despite this, there is good agreement between the time domain and the HDHB method. It should be mentioned that, similar to the aerofoil case, the cubic stiffness nonlinearity has no impact on the frequency behaviour of the LCO.

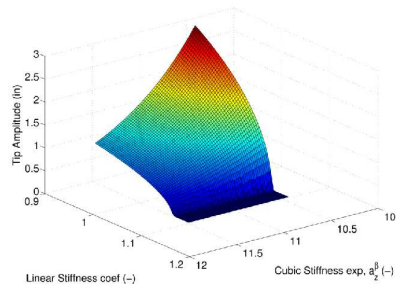
Figure 12 shows the response of the Goland wing with respect to the corresponding deterministic case. One harmonic was used in the HDHB method for speed although fractionally smaller amplitudes are observed. In this case a 5th order PCE was used, requiring 74 samples. Figure 12(b) shows the HDHB-PCE agreeing with the MC results based on the time-integration formulation. As before the mean values of the response are accurately predicted. The simulations are ran for 100 seconds which is sufficient capture the important, high amplitude points. Results near the bifurcation point are slightly degraded, where the number of stable points is not well captured. The range of cubic stiffness values has resulted in a distribution of amplitudes which is skewed due to the concentration of stable points. It is also noted that the amplitude mode value remains almost constant, not necessarily following the increase in mean and deterministic results. Computational times for the Goland wing are shown in Table 3.

4.3.2. Subcritical Bifurcations

The subcritical behaviour is obtained by including a pentic stiffness term in the nonlinear restoring force vector as shown in eq. B.5. Note the cubic terms are now also softening terms as in the aerofoil case. In this case the pentic stiffness is given as: $\gamma_z = 10^{a_z^\gamma}$ with a variation of $a_z^\gamma = 16.5 \pm 5\%$. The initial tip deflection, x_0 is also varied, ie. $x_0 = 0.75\text{in} \pm 100\%$. The other

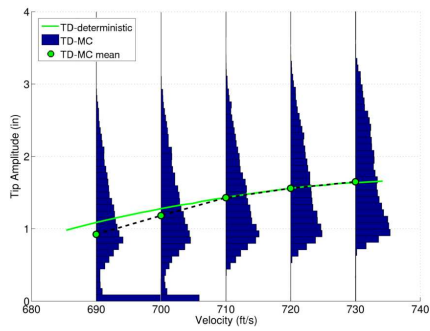


(a) Time domain MC

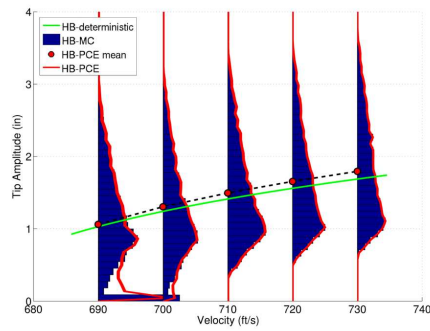


(b) HDHB method MC

Figure 11: Goland wing response at 690fts^{-1}



(a) Time domain MC



(b) HDHB

Figure 12: Goland Wing Supercritical LCO

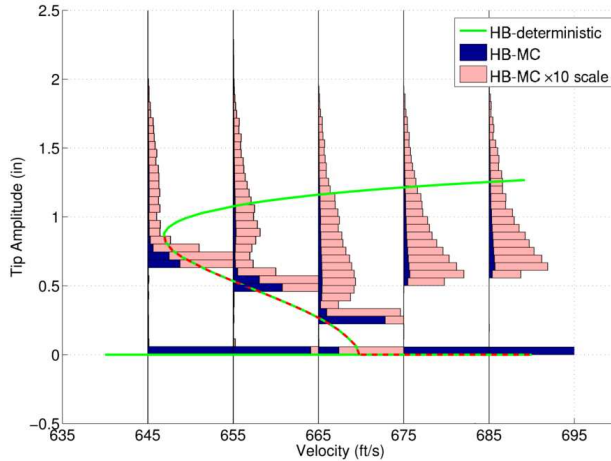


Figure 13: Goland Wing Subcritical LCO Amplitude, HDHB-MC

nonlinear stiffness coefficients are defined as: $\beta_z = 10^{11.5}$, $\beta_{ry} = 10^{10}$ and $\gamma_{ry} = 10^{16.5}$. As in previous cases the variability is obtained from uniform distributions.

The MC response of the subcritical Goland wing is shown in Figure 13. The dashed line represents the unstable branches of the response. The light colour bars show the response magnified by a factor of 10, to help clarify the upper branch. Note that finite amplitude LCOs can still be encountered at lower velocities than possible in the deterministic case, furthermore it is at this velocity that the maximum amplitude is found, highlighting the impact of variability on the LCO subcritical behaviour. In some ways the subcritical behaviour of the wing is analogous to the aerofoil: as the pentic stiffness reduces, samples converge to the unstable branch, as shown by Figure 14. The samples that converge to the stable branch are localised within a small vicinity of the nominal value of the pentic stiffness. These samples are responsible for the largest variations in amplitude, emphasising the sensitivity of the LCO to this parameter.

5. Conclusions

The influence of uncertainties in three nonlinear dynamical systems was investigated, a one *dof* Duffing oscillator, a two *dof* aerofoil and a multiple

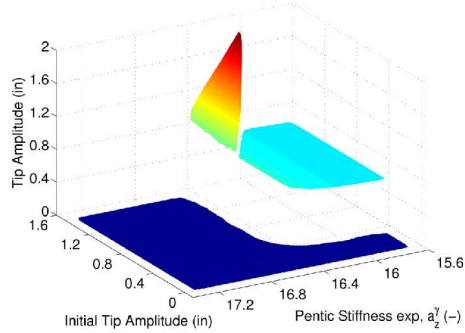


Figure 14: Goland Wing Subcritical LCO response at 645fts^{-1}

dof 3D wing. Each system was simulated using time domain and High-Dimensional Harmonic Balance methods where a non-intrusive polynomial chaos method was implemented and compared with Monte Carlo results. The HDHB method showed strong potential by modelling the system at a small fraction of the cost associated with time domain methods. The PCE method proved extremely effective for smooth response surfaces and showed significant reductions in cost in comparison with the Monte Carlo simulation. The limitations of PCE were highlighted when discontinuous behaviour was encountered as reproducing the bifurcation feature proved difficult, stability issues were encountered at the variable space boundaries. The subcritical behaviour of the aerofoil and Goland wing was investigated using the HDHB method which could reproduce the hysteretic unstable LCO branch. The unstable branch was characterised by lower values of the pentic stiffness and the same frequency as the stable upper branch as it is not a true physical solution. The variability of pentic stiffness can create the undesirable behaviour whereby large amplitude oscillations are found at velocities below

Table 3: Computational times

Case	Wall Clock (s)					
	Duffing		Aerofoil		Goland wing	
Method	MC	PCE	MC	PCE	MC	PCE
Time domain	9984	272	8042	142	83410	621
HDHB, NR	123	5	136	9	27511	206

the bifurcation point.

6. Acknowledgments

The first author would like to thank the Department for Employment and Learning for Northern Ireland for funding his research.

Appendix A. Aerofoil Formulation

The \mathbf{A} matrix used in eqs. (5) and (19) is given as:

$$\mathbf{A} = \begin{bmatrix} 0 & & & & \\ & \mathbf{N}_1 & & & \\ & & \mathbf{N}_2 & & \\ & & & \ddots & \\ & & & & \mathbf{N}_{N_H} \end{bmatrix}_{(2N_H+1) \times (2N_H+1)}, \quad \mathbf{N}_n = n \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, \quad n = 1, 2, \dots, N_H$$

The \mathbf{E} and \mathbf{E}^{-1} transformation matrices used in eqs. (6) and (20) are:

$$\mathbf{E} = \frac{2}{2N_{H+1}} \begin{bmatrix} 1/2 & 1/2 & \dots & 1/2 \\ \cos t_0 & \cos t_1 & \dots & \cos t_{2N_H} \\ \sin t_0 & \sin t_1 & \dots & \sin t_{2N_H} \\ \cos 2t_0 & \cos 2t_1 & \dots & \cos 2t_{2N_H} \\ \sin 2t_0 & \sin 2t_1 & \dots & \sin 2t_{2N_H} \\ \vdots & \vdots & & \vdots \\ \cos N_H t_0 & \cos N_H t_1 & \dots & \cos N_H t_{2N_H} \\ \sin N_H t_0 & \sin N_H t_1 & \dots & \sin N_H t_{2N_H} \end{bmatrix}$$

and

$$\mathbf{E}^{-1} = \begin{bmatrix} 1 & \cos t_0 & \sin t_0 & \dots & \cos N_H t_0 & \sin N_H t_0 \\ 1 & \cos t_1 & \sin t_1 & \dots & \cos N_H t_1 & \sin N_H t_1 \\ \vdots & \vdots & \vdots & & \vdots & \vdots \\ 1 & \cos t_{2N_H} & \sin t_{2N_H} & \dots & \cos N_H t_{2N_H} & \sin N_H t_{2N_H} \end{bmatrix}$$

$\hat{\mathbf{Q}}_{w_i}$, $i = (1, 2, 3, 4)$ denote the Fourier coefficients of the aerodynamic force generalising variables from system (19) where:

$$\hat{\mathbf{Q}}_{w_i} = \left\{ \begin{array}{c} \hat{w}_0^i \\ \hat{w}_1^i \\ \hat{w}_2^i \\ \vdots \\ \hat{w}_{2N_H}^i \end{array} \right\} \text{ and } \begin{array}{l} w_1 = \int_0^{t^*} e^{-\epsilon_1(t^*-\sigma)} \alpha(\sigma) d\sigma \\ w_2 = \int_0^{t^*} e^{-\epsilon_2(t^*-\sigma)} \alpha(\sigma) d\sigma \\ w_3 = \int_0^{t^*} e^{-\epsilon_1(t^*-\sigma)} \xi(\sigma) d\sigma \\ w_4 = \int_0^{t^*} e^{-\epsilon_2(t^*-\sigma)} \xi(\sigma) d\sigma \end{array}$$

where $\epsilon_1 = 0.0455$ and $\epsilon_2 = 0.3$, also $\psi_1 = 0.165$ and $\psi_2 = 0.335$. The matrices \mathbf{A}_1 , \mathbf{B}_1 , \mathbf{A}_2 and \mathbf{B}_2 from system (20) are given as:

$$\mathbf{A}_1 = c_1\omega^2\mathbf{A}^2 + c_3\omega\mathbf{A} + c_6\mathbf{I} + c_8(\omega\mathbf{A} + \epsilon_1\mathbf{I})^{-1} + c_9(\omega\mathbf{A} + \epsilon_2\mathbf{I})^{-1} \quad (\text{A.1})$$

$$\mathbf{B}_1 = c_0\omega^2\mathbf{A}^2 + c_2\omega\mathbf{A} + c_4\mathbf{I} + c_{10}(\omega\mathbf{A} + \epsilon_1\mathbf{I})^{-1} + c_{11}(\omega\mathbf{A} + \epsilon_2\mathbf{I})^{-1} \quad (\text{A.2})$$

$$\mathbf{A}_2 = d_1\omega^2\mathbf{A}^2 + d_2\omega\mathbf{A} + d_3\mathbf{I} + d_7(\omega\mathbf{A} + \epsilon_1\mathbf{I})^{-1} + d_8(\omega\mathbf{A} + \epsilon_2\mathbf{I})^{-1} \quad (\text{A.3})$$

$$\mathbf{B}_2 = d_0\omega^2\mathbf{A}^2 + d_5\omega\mathbf{A} + d_6\mathbf{I} + d_9(\omega\mathbf{A} + \epsilon_1\mathbf{I})^{-1} + d_{10}(\omega\mathbf{A} + \epsilon_2\mathbf{I})^{-1} \quad (\text{A.4})$$

Appendix B. Modal Models

The aeroelastic mass, damping and stiffness matrices are given as:

$$[\tilde{\mathbf{M}}_\phi] = \left[\mathbf{M}_\phi - \frac{\rho V^2}{2} \left(\frac{b}{V} \right)^2 \mathbf{A}_2 \right] \quad (\text{B.1})$$

$$[\tilde{\mathbf{C}}_\phi] = \left[\mathbf{C}_\phi - \frac{\rho V^2}{2} \frac{b}{V} \mathbf{A}_1 \right] \quad (\text{B.2})$$

$$[\tilde{\mathbf{K}}_\phi] = \left[\mathbf{K}_\phi - \frac{\rho V^2}{2} \mathbf{A}_0 \right] \quad (\text{B.3})$$

The nonlinear restoring force in the spatial domain for the supercritical and subcritical cases respectively are given as:

$$\mathbf{K}_{nl}(\mathbf{q}) = \left\{ \begin{array}{c} 0 \\ \vdots \\ 0 \\ -\beta_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^3 \\ -\beta_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^3 \\ 0 \\ \vdots \\ 0 \\ \beta_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^3 \\ \beta_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^3 \\ 0 \\ \vdots \\ 0 \end{array} \right\} \quad (\text{B.4})$$

and

$$\mathbf{K}_{nl}(\mathbf{q}) = \left(\begin{array}{c} 0 \\ \vdots \\ 0 \\ -\gamma_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^5 + \beta_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^3 \\ -\gamma_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^5 + \beta_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^3 \\ 0 \\ \vdots \\ 0 \\ \gamma_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^5 - \beta_z([\Phi(q_1, :)] \{\mathbf{q}\} - [\Phi(q_2, :)] \{\mathbf{q}\})^3 \\ \gamma_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^5 - \beta_{ry}([\Phi(q_3, :)] \{\mathbf{q}\} - [\Phi(q_4, :)] \{\mathbf{q}\})^3 \\ 0 \\ \vdots \\ 0 \end{array} \right) \quad (\text{B.5})$$

The transformation matrices used in eq. (24) are given as:

$$\mathbf{E}_{def}^{-1} = \begin{bmatrix} [\mathbf{e}_{def}]_1 & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & [\mathbf{e}_{def}]_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \mathbf{0} \\ \mathbf{0} & \dots & \mathbf{0} & [\mathbf{e}_{def}]_{n_m} \end{bmatrix}, [\mathbf{e}_{def}] = [1 \ \cos \omega t \ \dots \ \sin N_H \omega t]$$

$$\mathbf{E}_{vel}^{-1} = \begin{bmatrix} [\mathbf{e}_{vel}]_1 & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & [\mathbf{e}_{vel}]_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \mathbf{0} \\ \mathbf{0} & \dots & \mathbf{0} & [\mathbf{e}_{vel}]_{n_m} \end{bmatrix}, [\mathbf{e}_{vel}] = [0 \ -\omega \sin \omega t \ \dots \ \omega N_H \cos N_H \omega t]$$

$$\mathbf{E}_{acc}^{-1} = \begin{bmatrix} [\mathbf{e}_{acc}]_1 & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{0} & [\mathbf{e}_{acc}]_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \mathbf{0} \\ \mathbf{0} & \dots & \mathbf{0} & [\mathbf{e}_{acc}]_{n_m} \end{bmatrix}, [\mathbf{e}_{vel}] = [0 \ -\omega^2 \cos \omega t \ \dots \ -(\omega N_H)^2 \sin N_H \omega t]$$

The convolution integral of the inverse Laplace transform of the generalised aerodynamic matrix yields:

$$\dot{\mathbf{q}}_{a_i} = \int_0^t \dot{\mathbf{q}} e^{-\frac{V}{b}\eta_i(t-t^*)} dt^*, \quad i = 1, \dots, n_l \quad (\text{B.6})$$

Evaluating the integral gives

$$\dot{\mathbf{q}}_{a_i} = \dot{\mathbf{q}} \frac{b}{V\eta_i} \left(1 - e^{-\frac{V}{b}\eta_i t} \right) \quad (\text{B.7})$$

Here we are interested in the periodic solution only so the exponential term is damped out which yields:

$$\dot{\mathbf{q}}_{a_i} = \dot{\mathbf{q}} \frac{b}{V\eta_i}, \quad i = 1, \dots, n_l \quad (\text{B.8})$$

The discrete Fourier transforms used in eq. (24) for the j th mode can be given as:

$$\hat{q}_0^{a_i,j} = \frac{1}{2\pi} \int_0^{2\pi} \frac{b}{V\eta_i} \left(\sum_{n=1}^{N_H} (-\omega n \hat{q}_{2n-1}^j \sin \omega n t + \omega n \hat{q}_{2n}^j \cos \omega n t) \right) dt \quad (\text{B.9})$$

$$\hat{q}_{2m-1}^{a_i,j} = \frac{1}{\pi} \int_0^{2\pi} \frac{b}{V\eta_i} \left(\sum_{n=1}^{N_H} (-\omega n \hat{q}_{2n-1}^j \sin \omega n t + \omega n \hat{q}_{2n}^j \cos \omega n t) \right) \cos m t dt \quad (\text{B.10})$$

$$\hat{q}_{2m}^{a_i,j} = \frac{1}{\pi} \int_0^{2\pi} \frac{b}{V\eta_i} \left(\sum_{n=1}^{N_H} (-\omega n \hat{q}_{2n-1}^j \sin \omega n t + \omega n \hat{q}_{2n}^j \cos \omega n t) \right) \sin m t dt \quad (\text{B.11})$$

$$\hat{f}_0^j = \frac{1}{2\pi} \int_0^{2\pi} [\Phi]^T \mathbf{K}_{nl}(\mathbf{q}) dt \quad (\text{B.12})$$

$$\hat{f}_{2m-1}^j = \frac{1}{\pi} \int_0^{2\pi} [\Phi]^T \mathbf{K}_{nl}(\mathbf{q}) \cos m t dt \quad (\text{B.13})$$

$$\hat{f}_{2m}^j = \frac{1}{\pi} \int_0^{2\pi} [\Phi]^T \mathbf{K}_{nl}(\mathbf{q}) \sin m t dt \quad (\text{B.14})$$

for $m = 1, \dots, N_H$, $\{\hat{\mathbf{f}}_j\} = [\hat{f}_0^j \hat{f}_1^j \dots \hat{f}_{2N_H+1}^j]^T$ and $\hat{\mathbf{K}}_{nl} = [\hat{\mathbf{f}}_1 \hat{\mathbf{f}}_2 \dots \hat{\mathbf{f}}_{n_m}]^T$. The DFTs are computed numerically due to their complexity using a trapezoidal rule[43].

Appendix C. Nomenclature

Appendix C.1. Roman Symbols

- a polynomial coefficients for polynomial chaos expansions
- b semi-chord
- \mathbf{C} structural damping matrix
- C_L lift coefficient
- C_M pitching moment coefficient
- \mathbf{E} time/frequency domain transformation matrix
- \mathbf{F} generalised external force matrix
- \mathbf{J} Newton-Raphson system Jacobian
- k linear stiffness coefficient
- \mathbf{K} structural linear stiffness matrix
- m structural mass
- M number of independent continuous uncertain parameters
- \mathbf{M} structural mass matrix
- n_l Goland wing, number of lag variables in rational approximation
- N_H number of harmonics
- \mathbf{q} vector of modal deflections
- \mathbf{q}_{a_i} decomposed generalised aerodynamic vectors, $i = 1, \dots, n_l$
- \mathbf{Q} solution vector
- r_α radius of gyration
- \mathbf{R}^n Newton-Raphson system residual vector at iteration n
- \mathbf{S}^n Newton-Raphson solution vector at iteration n

t time
 V freestream velocity
 w_i Wagner variables, $i = 1, 2, 3, 4$
 x solution
 x_α distance between mass centre and elastic axis
 \hat{x}_i Fourier coefficient of displacement, $i = 1, \dots, N_H$

Appendix C.2. Greek Symbols

α aerofoil pitch displacement, angle-of-attack
 β cubic stiffness coefficient
 γ pentic stiffness coefficient
 Γ polynomial chaos basis functions
 ϵ_i constants in Wagner's function, $i = 1, 2$
 φ polynomial chaos random variable
 ζ damping ratio
 η Goland wing, term from rational approximation of generalised aerodynamic forces, $i = 1, \dots, n_l$
 λ Newton-Raphson relaxation parameter
 μ aerofoil air mass ratio
 ξ aerofoil non-dimensionalised plunge displacement
 ρ air density
 Φ truncated matrix of eigenvectors
 θ uncertain parameters
 ω fundamental solution frequency
 $\bar{\omega}$ aerofoil, frequency ratio, $\bar{\omega} = \omega_\xi / \omega_\alpha$

Appendix C.3. Subscripts, Superscripts and Oversets

- $()_{a_i}$ decomposed generalised aerodynamic vectors
- $()_L$ coefficient of lift
- $()_M$ coefficient of pitching moment
- $()_{nl}$ nonlinear force
- $()_{ry}$ rotation about y axis *dof*
- $()_{w_i}$ Wagner function representative aerodynamic variables
- $()_x$ Duffing oscillator displacement
- $()_z$ translation about z axis *dof*
- $()_\alpha$ aerofoil pitch *dof*
- $()_\xi$ aerofoil plunge *dof*
- $()_\phi$ quantity in modal domain
- $()_0$ initial condition (when specified)
- $()^*$ non-dimensionalised quantity
- $\hat{()}$ Fourier coefficient
- $\tilde{()}$ equally spaced time domain solution

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