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## Effect of pre-treatment and calcination temperature on Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> supported Ni-Co catalysts for dry reforming of methane

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#### Abstract

In this paper, the effect of pre-treatment and calcination temperature on a series of 5%Co/Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>, 5%Ni/Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> and 2.5%Co-2.5%Ni/Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts for dry reforming of methane was investigated. Main focus of our research was to improve the catalyst stability by proper pre-treatment and reaction conditions. The first approach aimed at the catalyst pre-treatment by using bimetallic systems and the second strategy at the *in* situ suppression of coke. The catalytic activity of bimetallic system was indeed higher compared to the monometallic in the temperature range of 500-800 °C (space velocity 18000 ml·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>, CH<sub>4</sub>/CO<sub>2</sub> = 1). The bimetallic catalyst calcined at 800 °C showed highest  $CH_4$  conversion without deactivation and gave a  $H_2/CO$  ratio of 91% and 0.96, respectively, and good stability with less coke deposition over 28 h at 800 °C reaction temperature. This improvement is assigned to the synergism between Co and Ni, their high dispersion according to interaction with support. It has been shown in our work that pretreatment temperatures and atmospheres have strong impact on stability of the catalyst. TEM, XRD and TPO investigations confirmed that the slight catalyst deactivation was related to the formation of multiwall carbon nanotubes with hollow inner tube structure. The addition of small amounts of steam or oxygen during DRM improved both the catalyst activity and stability as the bimetallic catalyst lost around 9.4% conversion in DRM, 5.4% in presence of water and only 3.2% in presence of O<sub>2</sub>.

*Keywords*: Bimetallic catalyst, Dry reforming, Methane, Stability, Deactivation, Regeneration

## Introduction

In recent years industrial processes have been established to convert methane into syngas  $(H_2, CO)$ . Some of these industrial processes comprise steam reforming and partial oxidation while lab-scale studies are also in progress on dry reforming of methane (DRM) and/or a combination of above mentioned processes [1]. The respective equations (Eqs. 1-3) are stated below. Dry reforming of methane would be attractive as it simultaneously converts main greenhouse gases  $CH_4$  and  $CO_2$  [2-7]. The produced syngas can be directly used for reactions like hydroformylation or the  $H_2/CO$  ratio can be adjusted for Fischer–Tropsch, dimethyl ether and methanol processes, which require higher  $H_2/CO$  ratios. DRM is usually associated with the reverse water–gas shift reaction Eq. (4).

$$CH_4 + H_2 O \rightarrow 3H_2 + CO \Delta H^\circ = 206 \text{ kJ/mol}$$
 Steam reforming (1)

$$CH_4 + \frac{1}{2}O_2 \rightarrow 2H_2 + CO \quad \Delta H^\circ = -38 \text{ kJ/mol}$$
 Partial oxidation (2)

$$CH_4 + CO_2 \rightarrow 2H_2 + 2CO \Delta H^\circ = 247 \text{ kJ/mol}$$
 Dry reforming (3)

 $CO_2 + H_2 \rightarrow CO + H_2O$   $\Delta H^\circ = 37.6 \text{ kJ/mol}$  reverse water-gas shift (4)

Noble metals display superior performance in this reaction but are generally too expensive [8]. Various emerging catalyst technologies for different applications were also recently reported in the literature [9-17]. Transition metals, for instance Ni and Co, are universally considered as suited catalysts for DRM due to their low costs. On the other hand, they were still not commercialized for DRM because they are prone to rapid deactivation as a consequence of carbon deposition. The following reactions are considered as the main source of coke formation in dry reforming of methane:

$$CH_4 \rightarrow 2H_2 + C$$
  $\Delta H^\circ = 75 \text{ kJ/mol}$  Methane decomposition (5)

$$2CO \rightarrow CO_2 + C$$
  $\Delta H^\circ = -172 \text{ kJ/mol}$  Boudouard reaction (6)

Both these reactions are limited by thermodynamic equilibrium. At high temperature, Boduouard reaction (Eq. 6) is not significant for coke formation, while methane decomposition (Eq. 5) is favoured.

To tackle the issue of carbon formation, several researchers investigated in depth the nature of the constituents of the catalysts and the operating conditions in order to improve their activity and stability in the process. This was done by supporting the active metals on materials such as alumina [18-22] which has advantages including low cost, great mechanical strength and high surface area. However, the phase transformations and interaction with metals during temperature variation affect and limit its applicability [20]. To solve this issue, alumina can be mixed with other supports to promote the catalyst activity and in general mixed oxide catalysts have better catalytic properties than pure oxides [23-27]. For instance, Bellido et al. [27] tested the effect of mixing ZrO<sub>2</sub> and CaO on the activity of nickel-based catalyst in DRM. They found that the electrical properties, such as particle conductivity as a function of anionic vacancies of the support, have a proportional influence on catalytic activity. The other two approaches to avoid carbon deposition during the reforming of hydrocarbons are to use a high oxygen mobility support or to add basic oxide such as  $ZrO_2$  to stabilize the alumina, which facilitates gasification of the carbon simultaneously [5]. Also, Perez-Camacho et al. [5] studied the effect of adding different high oxygen mobility dopants such as CeO<sub>2</sub>, ZrO<sub>2</sub>, or yttrium-stabilised zirconia (YSZ) on a Ni perovskite catalyst ( $Na_{0.5}La_{0.5}Ni_{0.3}Al_{0.7}O_{2.5}$ ). They found that the perovskite doped with 80.9% ZrO<sub>2</sub> and 15.2% CeO<sub>2</sub> gave the lowest amount of carbon deposits.

The pre-treatment conditions of the catalysts play a significant role for the final performance. It has been reported that the activity of supported metal catalysts strongly depends on the thermal treatment (either ex situ or in situ) before reaction, i.e., calcination and reduction temperatures [28, 29]. Calcination temperature has a substantial effect on dispersion of the active metal particles and the metal-support interaction and therefore influences the rate of carbon formation on the catalyst surface [30]. Wang and Ruckenstein [31] tested the effect of calcination temperature on Co-supported catalysts and found that degree of catalyst reduction and structural properties varied with calcination temperatures, which then altered the catalytic performance. Similarly, the investigation by Sun et al. [32] emphasized the significance of calcination temperature for the development of surface textural properties and phase structure. Our group [33] investigated the effect of combining Ni and Co metal catalysts and found that the interaction of Ni and Co gave less carbon formation with higher activity. The importance of calcination temperature on Ni/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts was also studied [28] as well as the effect of reduction temperature on the catalysts using hydrogen. Calcination temperature enhanced the activity while the reduction temperature increased basicity and therefore increased the CO<sub>2</sub> adsorption. The enhancement of CO<sub>2</sub> adsorption provided more oxygen species on the surface of the catalysts, which increase the gasification of the formed carbon (Eq. 6, back reaction) and prevent carbon deposition.

This paper presents the catalytic performance of a series of Co, Ni and Ni-Co-based catalysts supported on Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>. The effect of calcination temperature and of different

catalyst reduction protocols will be discussed. Moreover, the long-term stability of the bimetallic catalyst was examined, and the best-performing catalyst was also tested in presence of small amounts of steam or oxygen to study the impact of feed composition on stability.

#### Experimental

## Materials

The chemicals used include cobalt acetate tetrahydrate  $[(CH_3COO)_2Co]$ , nickel acetate tetrahydrate  $[(CH_3COO)_2Ni]$ , zirconium butoxide/butylate  $[(OC_4H_9)_4Zr]$  solution (80 wt.% in 1-butanol) and aluminium sec-butoxide/butylate  $[(C_{12}H_{27}O_3)Al]$  and all were of analytical grade. These chemicals were supplied by Aldrich, UK and Merck.

## **Catalyst preparation**

In order to get the crystal water-free salts, all the metal precursors were oven dried at 100  $^{\circ}$ C for 24 h. The weight loss was similar to the water content and therefore no decomposition took place. Prior to use, the salts were ground and sieved below 100  $\mu$ m in order to dissolve and react easily with Al-butylate. These salts were the source for cobalt and nickel. 48 g of Zr-butylate and 25 g of Al-sec-butoxide were mixed in a 250 ml three-neck round-bottom glass flask equipped with a reflux cooler and magnetic stirrer. The mixture was subjected to heating under stirring up to 130 °C followed by addition of 2.59 g of the dried cobalt acetate. After keeping the mixture under magnetic stirring for 2 h at 130 °C, the contents in the round-bottom flask were transferred into a 500 ml beaker containing 75 g of iso-propanol. The residues (butylates) from round-bottom flask were

poured into another beaker containing 75 g of iso-propanol. Finally, clear solutions with slightly pink and green colour were obtained for cobalt and nickel, respectively. These solutions were subjected to reflux for 1 h after addition of 27 g of distilled water within 1 min under intensive stirring. In order to avoid loss of iso-propanol, a water-containing round-bottom flask was used to cover the beaker. Finally, a glass frit was used to separate precipitate from the liquid after cooling the solution down to room temperature. No washing was necessary. Based on this recipe, three precursors were prepared with 5 wt% Ni, 5 wt% Co and 2.5 wt% Ni + 2.5 wt% Co on the ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> support. With each of these precursors, four different pre-treatment protocols were applied (groups 1-4, Table 1). After drying the as-prepared precursor overnight at room temperature, part of the solid was reduced *in situ* in the DRM reactor with H<sub>2</sub> at 800 °C without preceding calcination (group 1). Another part also was not calcined but reduced *ex situ* with H<sub>2</sub> at 800  $^{\circ}$ C, transferred to the reactor and reduced *in situ* with H<sub>2</sub> at 800 °C (group 2). A third part of the sample was heated with 2K/min and calcined ex situ under air at 550 °C for 6 h, transferred to the reactor and reduced with H<sub>2</sub> at 800 °C (group 3). The last part was heated with 2 K/min and calcined *ex situ* at 800 °C for 6 h and subsequently reduced in the reactor with  $H_2$  at  $800 \,^{\circ}C$  (group 4). The catalysts were named after the active metals and the respective pretreatment group (Table 1).

Table 1: Overview on pre-treatment protocols and catalyst names. All samples were dried at ambient conditions overnight before pre-treatment

Group	Pre-treatment	Catalyst	Name
1		5%Co/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Co-1
	- not calcined - reduced in situ (H <sub>2</sub> flow, 800 °C, 1.5 h)	5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Ni-1
		2.5%Co+2.5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	CoNi-1
2	- not calcined	5%Co/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Co-2
	- reduced ex situ (H <sub>2</sub> flow, 800 °C)	5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Ni-2

	- reduced in situ (H <sub>2</sub> flow, 800 °C, 1.5 h)	2.5%Co+2.5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	CoNi-2
3		5%Co/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Co-3
	- calcined (air flow, 550 °C, 6 h) - reduced in situ (H <sub>2</sub> flow, 800 °C, 1.5 h)	5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Ni-3
		2.5%Co+2.5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	CoNi-3
4	<ul> <li>calcined (air flow, 800 °C, 6 h)</li> <li>reduced in situ (H<sub>2</sub> flow, 800 °C, 1.5 h)</li> </ul>	5%Co/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Co-4
		5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Ni-4
		2.5%Co+2.5%Ni/ZrO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	CoNi-4

#### **Characterization of catalyst**

Micromeritics Tristar II 3020 surface area and porosity analyser was used to evaluate the Brunauer–Emmett–Teller (BET) specific surface area of the catalysts prior to reaction. 0.2 g of each sample was used for every analysis. Prior to analysis, moisture and other adsorbed gases on the catalysts surface were removed by degassing the samples at 250 °C for 3 h. Barrett-Joyner-Halenda (BJH) method was adopted to determine the pore size distribution using the corresponding nitrogen adsorption-desorption isotherm.

Temperature-programmed reduction using hydrogen (H<sub>2</sub>-TPR) and oxidation (O<sub>2</sub>-TPO) experiments were carried out using Micromeritics AutoChem II apparatus. For each analysis, 70 mg of the sample were pre-treated with Argon (30 ml/min) for H<sub>2</sub>-TPR and with Helium (30 ml/min) for O<sub>2</sub>-TPO at 150 °C for 30 min. The samples were cooled to ambient temperature before starting the analysis. For H<sub>2</sub>-TPR, the sample temperature was raised from ambient to 1000 °C in an automatic furnace under atmospheric pressure. During temperature ramping, H<sub>2</sub>/Ar mixture with a volume ratio 10/90 was flowing at 40 ml/min while heating rate was kept constant at 10 K/min. In O<sub>2</sub>-TPO, used for determining the nature of carbon deposits on the spent catalysts, a mixture of O<sub>2</sub> and He was flowing at 30 ml/min at same rate as in H<sub>2</sub>-TPR. The outlet gases were monitored by a thermal conductivity detector (TCD) to analyse the hydrogen and oxygen consumption with respect

to temperature in H<sub>2</sub>-TPR and O<sub>2</sub>-TPO respectively. The amount of carbon deposited during reaction was quantified using Shimadzu thermo-gravimetric analyser. Each spent catalyst with 10-15 mg was subjected to thermal treatment under air from 35 to 1000  $^{\circ}$ C (ramp rate of 20 K/min) and carbon contents were calculated.

The crystallinity of catalysts before and after reaction was measured by X-ray powder diffraction (XRD). STADI P automated transmission diffractometer (STOE, Darmstadt) equipped with Ge monochromator and CuK $\alpha$ 1 radiation was used. The patterns were recorded by a STOE position sensitive detector in the 2 $\theta$  range of 5 to 70°. The step widths of 0.5 and 100 s per step were used. Flat plates were used to prepared samples.

The morphology of nano-structured carbon deposited over the catalyst surface was analysed by JEOL JEM-1400 transmission electron microscope (TEM). TEM images were recorded at 120 kV accelerating voltage. Prior to analysis, ultrasonic dispersion of catalyst samples was carried out in ethanol at room temperature. A few drops of the suspension containing catalyst sample were placed on a carbon-coated copper grid. The copper grid was then used for imaging for each sample. The actual amounts of each metal, i.e., Co, Ni, Zr and Al were determined using inductively coupled plasma atomic emission spectroscopy (ICP-AES). The results are shown in Table (2).

**Table 2**: ICP-AES of the prepared catalyst

Sample name	Elements	Theoretical value	ICP values
		%	%
5% Co/Zr-Al	Zr	52	48.6
	Al	15	14.2
	Co	5	4.5
2.5%Co+2.5%Ni/Zr-Al	Zr	52	44.8
	Al	15	13.6
	Co	2.5	2.8
	Ni	2.5	2.6
5%Ni/Zr-Al	Zr	52	45.6

Al	15	13.1
Ni	5	4.4

#### **Catalyst activity**

As-synthesized catalysts (each 0.15 g) were tested in a fixed-bed microactivity reactor at atmospheric pressure. The reactor was made up of stainless steel and had an I.D. of 9.4 mm and was 30 cm long. A thermocouple was placed in the core of catalyst bed to monitor the reaction temperature. Prior to the DRM test, the metal oxides were reduced to metals with hydrogen (40 ml/min) at 800 °C for 90 min followed by nitrogen purging to remove any residual hydrogen in the reactor. Then the reactor temperature was lowered under flowing nitrogen to set point temperature of 700 °C. The feed gas contained methane and carbon dioxide (17 ml/min each) and nitrogen (11 ml/min) was added as inert. The gas hourly space velocity (GHSV) was 18000 ml·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup> corresponding to a catalyst weight of 0.15 g and a feed flow rate of 45 ml/min. Reaction temperatures ranged from 500 to 800 °C. Shimadzu 2014 gas chromatograph (GC) was used to analyse gases on-line from the reactor outlet using a thermal conductivity detector (TCD). The GC was equipped with two columns, i.e., Molecular Sieve 5A and Porapak Q for product analysis.

## **Results and Discussion**

#### Catalyst characterization

The XRD patterns for the fresh catalysts are shown in Figure 1a for group 2 (uncalcined + reduced *ex situ*) and group 4 (calcined at 800 °C + reduced *in situ*), respectively. All the catalysts were treated *in situ* at least once at 800 °C and have similar patterns in which all the reflections appeared except the one at 45.2° which only appeared for group 2 catalysts. This reflection can be assigned to metallic Co or Ni according to JCPDS 01-089-7093 and

JCPDS 03-065-0380 references, respectively. This explains the role of calcination in the dispersion and distribution of the active metal on the support surface.

In group 2, Co and Ni do not interact with the support and so small reflexes appeared which could stem from Ni, Co and/or Co-Ni alloy, while in group 4 - covering the samples that were calcined at 800  $^{\circ}$ C – Co and Ni are strongly interacting with the support and so no Co and Ni reflexes were observed. The reflections at  $2\theta = 35.6$ , 50.9 and 60.5 are assigned to  $ZrO_2$  [34] while the signal at  $2\theta = 30.5^{\circ}$  is ascribed to  $Al_{0.52}Zr_{0.48}O_{1.74}$  according to JCPDS 00-053-0294. Essential changes were observed in the phase composition when the calcination temperature was set to 800 °C in group 4, as the reflexes of  $ZrO_2$  turned to be more intense due to the formation of tetragonal  $ZrO_2$  [35]. Moreover, the intensity of the reflexes of Al<sub>0.52</sub>Zr<sub>0.48</sub>O<sub>1.74</sub> phase increased due to the calcination at 800 °C. Figure 1b shows XRD patterns of the spent catalysts after 6 h on stream at 700 °C, illustrating graphite peaks in the spent catalysts as it is confirmed by TEM as well. These reflexes appear at 26° for CoNi-2, Ni-2, CoNi-4 and Co-4 and at 43° for CoNi-4 and Co-4. Moreover, the peak intensities for spent CoNi-2 and Ni-2 catalysts are relatively lower than for the fresh materials, indicating the higher dispersion (lower crystallite size) of the bimetallic sample, which can affect their reducibility as will be discussed later. The same behaviour was also found by others [36, 37].



patterns of a) fresh catalysts and b) spent catalysts after 6 h on stream at 700 °C, atmospheric pressure, CH<sub>4</sub>: CO<sub>2</sub> =1: 1 in the feed gas. Catalyst weight: 150 mg, WHSV: 18000 ml g<sup>-1</sup> h<sup>-1</sup>.

The diffraction pattern of the spent CoNi-4 catalyst after 28 h on stream at 800 °C is shown in Figure 2. The new reflection at  $2\theta = 26.1^{\circ}$  indicates the formation of graphite [38,39], whereas the reflexes at  $2\theta = 43$ , 44.5, 53, 62 and 77° can be assigned to graphite carbon [40].



**Fig. 2:** XRD patterns of spent CoNi-4 catalyst after 28 h on stream at 800 °C, atmospheric pressure,  $CH_4/CO_2 = 1:1$ . Catalyst was reduced in H<sub>2</sub> at 800 °C, catalyst weight = 150 mg, WHSV = 18000 ml·g<sup>-1</sup>·h<sup>-1</sup>.

Figures 3-6 display the nitrogen volumes adsorbed with relative pressure for all the catalysts. All the isotherms are categorized as type II, with hysteresis loop similar to H3 according to IUPAC [41], thus indicating the presence of macropores. Group 1 samples before calcination and/or reduction showed the highest surface area of 384-460 m<sup>2</sup>/g. The surface area of groups 2, 3, and 4 were in the range of 15-175, 211-216 and 104.7-129.4 m<sup>2</sup>/g, respectively. The effect of calcination temperature can be clearly seen on comparing group 3 and 4. As expected, increasing the calcination temperature of group 4 materials to 800 °C lead to a decrease in the surface area by 43-50%. This means that high calcination temperature triggers sintering and reduction of surface area and thus particle growth. The

effect of pretreatment atmosphere can be elucidated by comparing groups 2 and 4. The loss in surface area of group 4 in comparison with group 2 samples was not as high as compared with group 3 (32%). Calcination temperature has a much higher impact on the surface area compared to the nature of pre-treatment atmosphere. Furthermore, the higher surface area found for group 2 materials could be an explanation for the low crystallinity compared to group 4 as confirmed by XRD.



**Fig. 3:** Adsorption/desorption isotherms, BET pore volumes and pore diameters of group 1 catalysts.



**Fig. 4:** Adsorption/desorption isotherms, BET pore volumes and pore diameters of group 2 catalysts.



**Fig. 5:** Adsorption/desorption isotherms, BET pore volumes and pore diameters of group 3 catalysts.



**Fig. 6:** Adsorption/desorption isotherms, BET pore volumes and pore diameters of group 4 catalysts.

TPR analysis was carried out to determine the catalyst reducibility in respect to the metalsupport interaction. Figures 7-9 summarize the TPR plots of the prepared catalysts, which show only one main reduction peak for each catalyst. Nickel-based catalysts have the lowest reduction temperature as Ni is much easier to reduce than Co. The high reduction peak temperature for Co-3 and Co-4 catalysts is attributed to the strong interaction between Co and support. For Co-2 the reduction is different from Co-3 and 4. It possesses a peak near 350 °C which could be assigned to the transition from Co<sup>3+</sup> to Co<sup>2+</sup>, and another shoulder around 470 °C can be attributed to the reduction of Co<sup>2+</sup> to Co<sup>0</sup> [42]. Another small peak at 550 °C which is present in both Co-2 and Ni-2 is due to metal support interaction. The peak of Ni-based catalysts, addition of Ni to Co shifts the reduction peak to lower temperature. Low reduction temperature of the bimetallic catalyst is due to the high dispersion as it has been proved by XRD [37]. Setting the calcination temperature to 550 °C (group 3) and to 800 °C (group 4) shifts reduction temperatures to higher values, indicating strong metal-support interaction (Figures 8 and 9) [44, 45]. For instance, the reduction peaks for bimetallic CoNi-2 (not calcined), CoNi-3 (calcined at 550 °C) and CoNi-4 (calcined at 800 °C) occur at 300, 600 and 770 °C, respectively. The peaks for Ni-4, CoNi-4 and Co-4 catalysts are centred at 720, 760 and 920 °C, respectively.



Fig. 7: TPR plots for group 2 catalysts after *ex situ* reduction at 800 °C.



Fig. 8: TPR plots for group 3 catalysts ex situ calcined at 550 °C.



Fig. 9: TPR plots for group 4 catalysts ex situ calcined at 800 °C.

Table 3 shows the amount of carbon deposits on the surface of the spent catalysts after 6 h on stream at 700 °C. The carbon deposition on the bimetallic (CoNi-1 and CoNi-2) catalysts is higher than that on the monometallic catalysts.

Group	Catalyst	<b>Conv. CH</b> <sub>4</sub> (%)		<b>Conv. CO</b> <sub>2</sub> (%)		Avg.	D.F. <sup>d</sup>	Carbon
		Initial <sup>a</sup>	Final <sup>b</sup>	Initial <sup>a</sup>	Final <sup>b</sup>	H <sub>2</sub> /CO <sup>c</sup>	(%)	TGA <sup>e</sup>
1	Co-1	38.2	36.8	58.2	53.0	0.67	3.66	1.65
-	Ni-1	48.1	47.6	64.5	60.6	0.78	1.04	1.59
-	CoNi-1	56.6	53.5	71.3	66.3	0.82	5.50	3.97
2	Co-2	49.5	36.9	63.7	52.5	0.69	25.40	3.15
	Ni-2	67.6	63.0	74.2	69.8	0.80	6.80	6.27
	CoNi-2	71.4	68.1	77.5	75.8	0.93	4.62	19.36
	Co-3	44.1	45.2	65.1	60.2	0.74	-2.5	1.12
3								
	Ni-3	55.5	58.7	74.5	66.6	0.86	-5.8	3.51
	CoNi-3	51.4	51.0	65.2	64.0	0.79	0.78	1.95
4	Co-4	56.8	57.4	72.1	68.5	0.86	-1.1	19.75
	Ni-4	64.9	64.4	77.4	72.0	0.92	0.77	5.13
	CoNi-4	68.5	67.3	77.4	76.3	0.91	1.80	13.21

**Table 3**: Catalyst activity and amount of carbon deposits from TGA analysis

Reaction condition: 700 °C,  $CH_4 + CO_2 = 34$  ml/min,  $N_2 = 11$  ml/min, catalyst wt. = 0.3 g <sup>a)</sup> 20 min on stream.

<sup>b)</sup> Final on stream (360 min).

<sup>c)</sup> Average data during time-on-stream.

<sup>d)</sup> Deactivation Factor (D.F) = (final CH<sub>4</sub> conversion - initial conversion CH<sub>4</sub>)/(initial conversion of CH<sub>4</sub>)×100.

<sup>e)</sup> Carbon deposition obtained by TGA method (mg).

Figures 10 and 11 show the TGA profiles for the spent catalysts (CoNi-2 and CoNi-4, respectively) after 6 h on stream at 500, 600, 700 and 800 °C. The reaction temperature has a strong effect on the amount of carbon deposited. Both catalysts CoNi-2 and CoNi-4 have the lowest amount of coke deposited after operation at 800 °C.



**Fig. 10:** TGA curves for spent CoNi-2 catalysts from runs at different reaction temperatures, measured in air with heating rate 20 K/min.



**Fig. 11:** TGA curves for spent CoNi-4 catalysts from runs at different reaction temperatures, measured in air with heating rate of 20 K/min.

The TEM analysis of the spent CoNi-4 catalyst after reaction for 28 h at 800 °C is shown in Figure 12. The images evidence the formation of multiwall carbon nanotubes of different size together with amorphous carbon. Both ends of the nanotubes were open as seen in Figure 12 a-c. Figure 12 d shows a carbon nanotube with multiple graphitic layers around the hollow inner tube [38, 39].



**Fig. 12:** TEM analysis of the spent CoNi-4 catalyst after reaction for 28 h at 800 °C, atmospheric pressure,  $CH_4/CO_2 = 1:1$ . Catalyst was reduced in H<sub>2</sub> at 800 °C, catalyst weight = 150 mg, WHSV = 18000 ml·g<sup>-1</sup>·h<sup>-1</sup>.

Results from TPO study of the nature of carbon deposited on spent CoNi-4 catalysts after 28 h on stream at 800 °C and after 6 h on stream at 700 °C is shown in Figure 13. The TPO profile for CoNi-4 after 28 h showed one shoulder at 620 °C and another at higher temperature at 720 °C, while the sample after 6 h on stream shows one peak at 600 °C. This carbonaceous matter can be assigned to multiwall carbon nanotubes (low temperature) and graphite (high temperature).



**Fig. 13:** TPO plots of the spent CoNi-4 catalyst after 28 h on stream at 800 °C and after 6 h on stream at 700 °C.

#### Catalyst Activity

Table 3 displays the CO<sub>2</sub> and CH<sub>4</sub> conversions and H<sub>2</sub>/CO ratios in DRM at 700 °C for all catalysts. The CH<sub>4</sub> conversions were always lower than the corresponding CO<sub>2</sub> conversions and H<sub>2</sub>/CO ratios were always less than unity in all groups. This phenomenon can be explained by the occurrence of reversed water-gas shift reaction (RWGS, Eq. 2) in which CO<sub>2</sub> and H<sub>2</sub> are consumed to produce CO and H<sub>2</sub>O [43].

The table reveals that in all groups the monometallic nickel-based catalyst gives higher  $CO_2$  and  $CH_4$  conversion than monometallic cobalt-based catalysts. Similar results were found by Gonzalez-de la Cruz [44]. Also, the bimetallic catalysts provide higher  $CO_2$  and  $CH_4$  conversions than monometallic catalysts. The higher activity of these catalysts can be attributed to the synergistic effect between the Co and Ni metals [40]. Gonzalez-de la Cruz et al. [44] investigated the synergistic effect of Zr-supported bimetallic Ni-Co systems on

the DRM activity with *in-situ* X-ray absorption spectroscopy (XAS) and found that even though the monometallic cobalt system is inactive, the Ni-Co bimetallic systems have much higher activity and selectivity in DRM as both metals obviously protect each other from oxidation under reaction conditions. CH<sub>4</sub> conversions of 49.5, 67.6 and 71.4% were observed for Co-2, Ni-2 and CoNi-2 catalysts, respectively. This can be explained by the physical-chemical modification between Co and Ni (low crystallinity (XRD) and low reduction temperature (TPR)) which has an impact on their activity and stability. The higher the activity of the bimetallic catalysts, the higher the carbon deposition (Table 3). The catalysts CoNi-1, CoNi-2, CoNi-3 and CoNi-4 reached CH<sub>4</sub> conversions of 56.6, 71.4, 51.1 and 68.5% and the analysed carbon amounted to 3.97, 19.36, 1.95 and 13.21 mg, respectively. For the least active samples Co-1, Co-2, Co-3 and Co-4 the carbon deposits were measured as 1.65, 3.15, 1.12 and 19.75 mg, respectively. The highest amount of carbon deposition found by sample CoNi-2 could be due to low interaction with the support as it was found by XRD which revealed only small reflexes for Co, Ni or Co-Ni spinel. The carbon deposition can be attributed to both methane decomposition (Eq. 3) and Boudouard reaction (Eq. 4) [46]. Although the carbon deposition on the bimetallic catalysts is high, these catalysts show comparatively high stability in all four groups. This can be attributed to the large pore diameters that are beneficial for the long-term stability as complete pore plugging is hindered. Generally, one reason for the catalyst deactivation could be the carbon deposition within the pores of the catalyst [47, 48]. The initial conversions of  $CH_4$  in the catalysts of groups 4 and 3 are almost the same as the final conversions. However, both groups 1 and 3 showed deactivation and a loss of 5% in CH4 conversion (deactivation factors of -1.1, 0.77 and 2.5 % for Co-4, Ni-4 and CoNi-4,

respectively). This indicates that the catalyst pre-treatment has a significant effect on the textural properties and on catalytic activity and stability [28]. To get more information on the nature of carbon deposited on the CoNi-4 catalyst surface after 6 h on stream at 700 °C, TEM images were recorded. As shown in Figure 12, multiwall carbon nanotubes were formed with different diameter and orientation and with high degree of disorder which confirms the contribution of reverse Boudouard reaction (Eq. 4) in which CO<sub>2</sub> reacts with any type of deposited carbon [49]. This is in agreement with TPO results. The variation in reaction temperature has been studied over CoNi-2 and CoNi-4. Figures 14 and 15 show the effect of reaction temperature on  $CO_2$  and  $CH_4$  conversion and  $H_2/CO$  ratio. Again, CO<sub>2</sub> conversions are higher than the corresponding CH<sub>4</sub> conversions at all reaction temperatures due to RWGS which consumes CO<sub>2</sub> as well. Furthermore, these catalysts showed high stability at all reaction temperatures. This can be explained by the synergistic effect between the metals by forming smaller sized bimetallic oxides that are resistant to be oxidised under the reaction conditions. These two bimetallic catalysts (CoNi-2 and CoNi-4) also have the highest pore diameters. The  $CH_4$  conversions for CoNi-4 are 15, 35, 69 and 90% at 500, 600, 700 and 800 °C, respectively, with the H<sub>2</sub>/CO ratio approaching unity at 800 °C. The increase in H<sub>2</sub>/CO ratio at high temperature can be explained by an increase of endothermic methane decomposition to carbon and hydrogen.



**Fig. 14:** course of a) CO<sub>2</sub> conversion and H<sub>2</sub>/CO ratio and b) CH<sub>4</sub> conversion with time on stream over CoNi-2 at reaction temperatures of 500-800 °C, atmospheric pressure, CH<sub>4</sub>/CO<sub>2</sub> = 1:1, catalyst weight = 150 mg, WHSV = 18000 ml·g<sup>-1</sup>·h<sup>-1</sup>.



**Fig. 15:** course of a) CO<sub>2</sub> conversion and H<sub>2</sub>/CO ratio and b) CH<sub>4</sub> conversion with time on stream over CoNi-4 at reaction temperature of 500-800 °C, atmospheric pressure, CH<sub>4</sub>/CO<sub>2</sub> = 1:1. Catalyst was reduced in H<sub>2</sub> at 800 °C, catalyst weight = 150 mg, WHSV = 18000 ml·g<sup>-1</sup>·h<sup>-1</sup>.

To distinguish the nature of coke deposits formed at different reaction temperature, a TGA study for spent catalysts after 6 h on stream was conducted (Figures 10 and 11). Coke deposition over CoNi-4 was less than for CoNi-2 at all reaction temperatures, as Co and Ni were better dispersed on the surface of the support due to the strong interaction as it has

been confirmed by TPR. In addition, it possesses the highest pore diameter due to hightemperature pre-treatment of the catalyst [28, 29]. For CoNi-4 (Figure 11), the weight losses are 5, 13, 15 and 30% at 800, 700, 500 and 600 °C, respectively.

Moreover, for both catalysts CoNi-2 (Figure 10) and CoNi-4 (Figure 11) the lowest coke deposition rate was observed at 800 °C. This can be attributed to the fact that the Boudouard reaction (Eq. 4) is exothermic and becomes thermodynamically less favourable above 700 °C [45, 37, 50]. Moreover, at 800 °C the presence of zirconia in the support suppresses the methane decomposition (Eq. 3) and also promotes the reverse Boudouard reaction [5]. The highest amounts of coke deposits were measured at 600 °C, as this intermediate temperature allows both methane decomposition (Eq. 3) and Boudouard reaction (Eq. 4) in remarkable extent [45].

Regarding the activity, CoNi-4 showed high CH<sub>4</sub> conversion of 91% without deactivation and a H<sub>2</sub>/CO ratio of 0.96 at 800 °C and therefore it was chosen for further long-term tests (28 h on stream at 800 °C), and the courses of H<sub>2</sub>/CO ratio, CO<sub>2</sub> and CH<sub>4</sub> conversion are presented in Figure 16. The catalyst showed only minor loss of its activity after 24 h. However, with ongoing test, sharp drops in CH<sub>4</sub> and CO<sub>2</sub> conversion from 88.8 % to 84 % and from 94 % to 80 %, respectively, were observed (relative loss of initial activity: 5% in CH<sub>4</sub>, 15% in CO<sub>2</sub>). The main cause of deactivation is carbon deposition as confirmed by TEM (Figure 12), TPO (Figure 13) and XRD (Figure 2) studies with the spent catalyst.





**Fig. 16:** long-term stability of CoNi-4 catalyst at 800 °C, atmospheric pressure, CH<sub>4</sub>/CO<sub>2</sub> = 1:1. Catalyst was reduced in H<sub>2</sub> at 800 °C, catalyst weight = 150 mg, WHSV = 18000 ml·g<sup>-1</sup>·h<sup>-1</sup>.

The addition of steam or oxygen to the feed thermodynamically suppresses the coke formation [51]. An increase of the methane conversion with steam addition has been reported in literature [52-54]. Moreover, steam acts as an oxidant removing carbon species from the surface of the catalyst [55]. It is well known that in the presence of a small amount of steam a higher stability of DRM catalysts and a H<sub>2</sub>/CO ratio close to unity are obtainable due to the WGS side reaction [53, 54]. In the present study, addition of small amounts of steam or oxygen to the feed has been tested as a way to increase the stability of the CoNi-4 catalyst. The resulting course of CH<sub>4</sub> conversion for CO<sub>2</sub> reforming of methane at 700 °C is compared to conventional DRM in Figure 17. This particular catalyst lost around 9.4% of initial activity in DRM, but only 5.4% in presence of water and only 3.2% in presence of O<sub>2</sub>.





**Fig. 17:** Effect of steam or oxygen addition on long-term stability of CoNi-4 catalyst at 700 °C, atmospheric pressure, catalyst was reduced in H<sub>2</sub> at 800 °C, catalyst weight = 100 mg.

TGA of spent CoNi-4 catalyst was conducted afterwards (Figure 18). The amount of carbon deposits decreased with the addition of a small amount of water or oxygen, which is in agreement with the catalyst stability (Figure 17).





**Fig. 18:** TGA curves for spent CoNi-4 catalysts used with different feeds at 700°C, measured in  $N_2$  atmosphere with heating rate of 20 K/min.

## Conclusions

Various monometallic and bimetallic catalysts supported on Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> (Co, Ni and bimetallic Co-Ni) at different calcination and pre-treatment temperatures were tested for dry reforming of methane. The pre-treatment improved the catalytic performance and bimetallic catalysts outperformed the monometallic catalysts mainly due to synergy between both Ni and Co. Interestingly the higher conversions resulted in higher carbon deposition which played significant role in catalyst deactivation. The least carbon deposition was observed on bimetallic CoNi-4 catalyst calcined under air at 800 °C and

operated at 800 °C after 6 h on stream. This means that high calcination temperature triggers sintering and reduction of surface area and thus particle growth which in turn has an impact on the stability of the catalyst. As it has been reported, this catalyst showed high stability at these conditions for 28 h on stream. The deactivation is assigned to carbon deposition and was confirmed by XRD, TEM and TPO data. The catalyst stability was improved when steam or oxygen were added in the feed stream.

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