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Sun, H., Zhang, Y., Guan, S., Huang, J., & Wu, C. (2020). Direct and highly selective conversion of captured CO2 into methane through integrated carbon capture and utilization over dual functional materials. Journal of CO2 Utilization, 38, 262. https://doi.org/10.1016/j.jcou.2020.02.001

#### Published in:

Journal of CO2 Utilization

# **Document Version:**

Peer reviewed version

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# Direct and highly selective conversion of captured CO<sub>2</sub> into methane through integrated carbon capture and utilization over dual functional materials

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# ABSTRACT

Excessive atmospheric CO<sub>2</sub> emission is regarded as one of the main factors causing global climate change. Thus, there is an urgent need to explore the possibility of CO<sub>2</sub> capture and converting the captured CO<sub>2</sub> to fuels or value-added products. Recently, an integrated carbon capture and utilization (ICCU) process performed in a single reactor under isothermal conditions draws intensive attentions due to the reduction of energy requirement for sorbent regeneration. However, from literature, normally a low loading of sorbent in dual functional materials (DFMs) was applied resulting in a very low CO<sub>2</sub> capture capacity and consequent low CH<sub>4</sub> yield in the ICCU process. Herein, we demonstrate the intermediate-temperature DFMs using inexpensive high-capacity MgO sorbent. The synthesized DFMs are a physical mixture of sorbent and Ru/CeO<sub>2</sub> catalyst by the mass ratio of 2:1 allowing simultaneous regeneration of sorbent and conversion of CO<sub>2</sub> in a single reactor at 300 °C. During the 1st cycle of ICCU process, 10Ru/CeO2-MgO exhibits the best ICCU performance with the highest CH<sub>4</sub> yield of 7.07 mmol g<sup>-1</sup> and CO<sub>2</sub> conversion of 89%. However, after 10 cycles of ICCU process, 5Ru/CeO<sub>2</sub>-MgO exhibits the highest CH<sub>4</sub> yield (3.36 mmol g<sup>-1</sup>) and CO<sub>2</sub> conversion (79%), which are much higher than that of 2.5Ru/CeO<sub>2</sub>-MgO (1.14 mmol g<sup>-1</sup> and 39%) and 10Ru/CeO<sub>2</sub>-MgO (2.31 mmol g<sup>-1</sup> and 69%). It is mainly attributed to that more oxygen vacancies are remained in 5Ru/CeO<sub>2</sub>-MgO resulted from the metal-support interaction. Keywords: sorbent; catalysts; CO<sub>2</sub> capture and conversion; the Sabatier reaction; methane

#### **1. Introduction**

The earth's surface temperature exhibited a dramatic increase and will increase continually due to the anthropogenic  $CO_2$  emissions [1, 2]. Thus, many efforts are being made to developing new

technologies for carbon dioxide mitigation [3, 4]. Carbon capture and utilization (CCU) is a very promising strategy to reduce  $CO_2$  emissions due to  $CO_2$  acting as the carbon source can be used to produce value-added products [5, 6]. However, the current state-of-art of CCU has several steps including  $CO_2$  capture, the regeneration of sorbent, and the conversion of captured  $CO_2$ . The transportation of sorbent from carbon capture reactor to sorbent regeneration reactor using temperature swing process has caused significant challenges e.g. sorbent attrition [7]. Recently, an integrated carbon capture and utilization (ICCU) process has been proposed to combine the regeneration of sorbent and catalytic conversion of the captured  $CO_2$  in a single fixed bed reactor under isothermal conditions [8-10], which can reduce the energy required for sorbent regeneration, the infrastructure to transport and store captured  $CO_2$ .

The reverse water-gas shift (RWGS) as shown in Eq.(1) is a promising reaction for the utilization of  $CO_2$  because carbon monoxide (CO) acts as a feedstock to produce fuels and chemicals via Fischer-Tropsch process [11, 12]. In our previous work, the ICCU process has been proven for the CO production [8]. The captured  $CO_2$  was converted into CO in a single reactor under isothermal conditions using one-pot method synthesized DFMs, which exhibited a good stability after 20 cycles of ICCU process. In addition, dry reforming of methane or ethane has also attracted significant attentions because these two processes can convert two major greenhouse gases including  $CO_2$  and  $CH_4$  or  $C_2H_6$  into a mixture of CO and  $H_2$  (Eq. (2) or Eq. (3), respectively) [13, 14].

$$CO_{2}+H_{2}\leftrightarrow CO+H_{2}O, \Delta H_{r,298K}= + 41.2 \text{ kJ mol}^{-1}$$
(1)  

$$CO_{2}+CH_{4}\leftrightarrow 2CO+2H_{2}, \Delta H_{r,298K}= + 247 \text{ kJ mol}^{-1}$$
(2)  

$$2CO_{2}+C_{2}H_{6}\leftrightarrow 4CO+3H_{2}, \Delta H_{r,298K}= + 429 \text{ kJ mol}^{-1}$$
(3)

Recently, the Sabatier reaction (Eq. (4)) has attracted considerable attention due to the existence of infrastructure for CH<sub>4</sub> applications and environmental benefits [15, 16]. CO<sub>2</sub> methanation is strongly exothermic ( $\Delta$ H=-164 kJ mol<sup>-1</sup>) and limited by thermodynamics at high temperature. Relatively mild reaction conditions can not only maximize the reaction conversion but also largely increase the selectivity of CH<sub>4</sub> due to avoiding the formation of by-product such as CO [17]. Various metals (Ni, Pt, Rh, and Ru) and supports (CeO<sub>2</sub>, TiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, and ZrO<sub>2</sub>) have been extensively investigated for CO<sub>2</sub> methanation [18]. At a low operating temperature, it is found that Ru is highly active and selective to methane, especially when it is supported on reducible supports (CeO<sub>2</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub>) [19, 20]. Duyar et al. successfully captured CO<sub>2</sub> from flue gas and converted the captured CO<sub>2</sub> to natural gas at 320 °C sequentially in the same reactor by DFMs, which consist of nano-dispersed CaO and Ru acting as sorbent and methanation catalyst, respectively [5]. Bermejo-López et al. investigated the utilization of Na<sub>2</sub>CO<sub>3</sub> as the sorbent to convert the captured CO<sub>2</sub> to

CH<sub>4</sub> and proposed a mechanism of CO<sub>2</sub> capture and hydrogenation process [21]. However, a low loading of sorbent in this integrated process resulted in a very low CO<sub>2</sub> uptake and consequent low CH<sub>4</sub> production. In addition, the desired temperature of Ru in Sabatier reaction is around 300 °C, which is much lower than the temperature of carbon capture using CaO-based materials (normally 600 °C and 900 °C for carbonation and regeneration, respectively) [22]. Therefore, the consistency of carbon capture temperature using the sorbent and conversion temperature using catalytic sites is very important for the synthesis of DFMs. Further increasing the loading of sorbent is also crucial important.

CO<sub>2</sub>+4H<sub>2</sub>↔CH<sub>4</sub>+2H<sub>2</sub>O,  $\Delta$ H<sub>r.298K</sub>= -164 kJ mol<sup>-1</sup> (4)

Magnesium oxide (MgO) appear to be particularly advantageous in ICCU process because the temperature for carbon capture is around 300 °C, which is also a desirable temperature for  $CO_2$  methanation using Ru-based catalysts [23]. However, pure MgO exhibits a moderate  $CO_2$  capture capacity, which is normally lower than 1 mmol g<sup>-1</sup> and poor thermal stability during the cyclic performance of sorbent [24]. Recently, incorporating alkali metal nitrates into MgO molten state received intensive attention to improve  $CO_2$  capture capacity [24, 25]. This is attributed to the introduction of molten nitrates into MgO sorbent can prevent the generation of rigid  $CO_2$ -impermeable product layer of unidentate carbonates on the surface of MgO and then promote the formation of carbonate ions ( $CO_3^{2-}$ ) in the molten salts [24]. Therefore, we synthesised an inexpensive high-capacity MgO sorbent modified by the alkali metal nitrates.

Here, we develop Ru/CeO<sub>2</sub>-MgO as DFMs, which is a physical mixture of an inexpensive highcapacity MgO sorbent and a Ru/CeO<sub>2</sub> catalyst with the mass ratio of 2:1. CeO<sub>2</sub> nanorods are used as Ru support as the reaction rate can be dramatically improved by the oxygen vacancies on the surface of CeO<sub>2</sub> through absorbing and activating the carbon-oxygen bond [20]. The schematic diagram of the proposed ICCU process using the synthesized Ru/CeO<sub>2</sub>-MgO DFMs is displayed in Fig. 1. This ICCU process has two steps. The first step is CO<sub>2</sub> capture from flue gas using highcapacity MgO sorbent. The second step is converting the captured CO<sub>2</sub> into CH<sub>4</sub> using Ru/CeO<sub>2</sub> catalysts in a single reactor at the same temperature via Eq. (5) after switching the feed gas to renewable H<sub>2</sub>.

$$MgCO_{3}+4H_{2}\leftrightarrow MgO+CH_{4}+2H_{2}O, \Delta H_{r,298K}=-67 \text{ kJ mol}^{-1}$$
(5)



**Fig. 1.** Schematic diagram of ICCU process directly converting the captured CO<sub>2</sub> into methane over DFMs.

#### 2. Experimental section

#### 2.1. Preparation of Catalyst

A hydrothermal process as previously reported was used to synthesize CeO<sub>2</sub> nanorods [26]. Typically, 1.730 g of Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O and 28.0 g of NaOH were dissolved in 10 mL and 70 mL of deionized water, respectively. These two solutions were mixed in a plastic beaker and stirred for 30 min to form light purple slurry. After that, the mixture was transferred into a stainless-steel autoclave (100 mL) and put into the oven at 120 °C for 24 h. After cooling down to the room temperature, the white precipitates were filtered using vacuum pump and washed until the pH reached 7 with deionized water and ethanol. The obtained yellow powder was dried at 80 °C overnight and calcined at 600 °C for 5 h.

Ru/CeO<sub>2</sub> catalyst was prepared by a wet impregnation method using the synthesized CeO<sub>2</sub> nanorods as the support. Typically, 0.5 g CeO<sub>2</sub> nanorods were added into 20 mL solution with predetermined amount of RuCl<sub>3</sub>, corresponding to 2.5wt%, 5wt% and 10wt% of Ru. The black slurry was stirred for 24 h at room temperature and then evaporated water at 80 °C. After that, the obtained black powder were dried at 100 °C overnight, calcined at 300 °C for 2 h and reduced at 300 °C for 2 h in 5%  $H_2/N_2$  with a flow rate of 50 mL min<sup>-1</sup>. The synthesized catalysts are donated as 2.5Ru/CeO<sub>2</sub>, 5Ru/CeO<sub>2</sub> and 10Ru/CeO<sub>2</sub>.

#### 2.2. Preparation of DFMs

High-capacity MgO sorbent was prepared as reported by Harada et al. [24]. Typically, 9.713 g of  $4MgCO_3 \cdot Mg(OH)_2 \cdot 5H_2O$  and 0.207 g of LiNO<sub>3</sub>, 0.153 g of NaNO<sub>3</sub>, and 0.526 g of KNO<sub>3</sub> were added in 40 mL of deionized water at room temperature and stirred for 60 min. The obtained white slurry was dried at 120 °C overnight and then calcined at 450 °C for 4 h.

The fabrication of DFMs was performed by physically mixing high-capacity MgO sorbent and reduced Ru/CeO<sub>2</sub> catalysts by the mass ratio of 2:1.

#### 2.3. Material characterization

The loading of Ru on  $CeO_2$  nanorods was determined by inductively coupled plasma-optical emission spectroscopy (ICP-OES, 5300DV). Nitric acid was utilized to dissolve the catalysts. Firstly, the samples which are dissolved into the nitric acid are heated in the microwave to 180 °C and held for 10 min. After that, it was cool down to room temperature. Powder X-ray diffraction (XRD) patterns ranging from 10 to 80° were collected by a PANalytical empyrean series 2 diffractometer with Cu Ka X-ray source. Scherrer's equation was utilized to calculate the average crystallite size of CeO<sub>2</sub> nanorods based on the diffraction peaks at 28.5°. BET surface area was measured by ASAP 3000 analyser at 77 K. The Brunauer-Emmett-Teller (BET) surface area was calculated by the adsorption branch data when the relative pressure  $(P/P_0)$  ranges from 0.06 to 0.2. Scanning electron microscopy (SEM) images coupled with an energy dispersive X-ray spectrometer (EDX) were measured by Stereoscan 360. Transmission electron microscopy (TEM, JEOL 2010) and high-resolution TEM (HRTEM, FEI talos F200) are utilized to observe the detailed structure of DFMs. The samples which are dispersed in acetone uniformly were dropped on Cu grids coated with carbon and dried for TEM characterization. Valence states on the surface of Ru/CeO<sub>2</sub> catalysts and spent DFMs were acquired by X-ray photoelectronic spectrometer (XPS, Escalab 250Xi) using Mg Ka radiation. The binding energies were calibrated by the C1s peak centred at 284.8 eV of adventitious carbon. CO<sub>2</sub> temperature-programmed desorption (CO<sub>2</sub>-TPD), H<sub>2</sub> temperatureprogrammed reduction (H<sub>2</sub>-TPR) and CO chemisorption of Ru/CeO<sub>2</sub> catalysts were characterized by the Micromeritics Autochem II 2920 analyser. The catalyst around 100 mg was placed in a Ushape tube and pre-treated at 100 °C in the inert gas to remove absorbed gases and moisture. For CO<sub>2</sub>-TPD, CO<sub>2</sub> adsorption was conducted in 10% CO<sub>2</sub>/He. CO<sub>2</sub> desorption was conducted with the temperature increasing from 50 °C to 800 °C. For H<sub>2</sub>-TPR, after the temperature of U-shape tube decreased to 50 °C, the catalyst was reduced with the temperature ranging from 50 °C to 800 °C at a heating rate of 10 °C min<sup>-1</sup> in 5% H<sub>2</sub>/N<sub>2</sub> (30 mL min<sup>-1</sup>). For CO chemisorption, firstly, the catalyst was reduced in 10% H<sub>2</sub>/Ar at 300 °C for 2 h and then the U-shape tube was purged by pure He at 350 °C for 30 min. After cooling down to 50 °C, the chemisorption was performed in 10% CO/He. The Raman spectra were collected using 532 nm as the excitation wavelength and 1  $cm^{-1}$  as the resolution.

#### 2.4. Integrated CO<sub>2</sub> capture and utilization

A fixed-bed reactor coupled with an online gas analyser purchased from ETG Risorse & Tecnologia as shown in Fig. S1 (Supporting Information, SI) was utilized for the evaluation of ICCU performance of synthesized DFMs. The length and inner diameter of stainless steel tube in this fixed bed reactor is 50 cm and 0.635 cm, respectively. Typically, 450 mg of powdered DFMs was placed in the middle of the reactor and two ends were fixed by quartz wool. The carbonation reaction (carbon capture stage) was performed in 65% CO<sub>2</sub>/N<sub>2</sub> (50 mL min<sup>-1</sup>) at 300 °C for 60 min. Then, the reactor was purged by pure N<sub>2</sub> for 5 min. The second stage is converting the captured CO<sub>2</sub> into CH<sub>4</sub> at the same temperature after switching the feed gas to renewable H<sub>2</sub> (5% H<sub>2</sub>/N<sub>2</sub>) with a flow rate of 50 mL min<sup>-1</sup>. In total, 10 cycles of ICCU process were conducted as the description. The calculation of carbon balance and CO<sub>2</sub> conversion are shown in supporting information.

The mechanism study of ICCU process was investigated by in-situ DRIFTS (Spectro-meter: JASCO-4600, DRIFTS cell: Bruker). The first step is carbon capture from 65% CO<sub>2</sub>/N<sub>2</sub> at 300 °C for 60 min. Then, the DRIFTS cell was purged by pure N<sub>2</sub> for 5 min. The conversion of captured CO<sub>2</sub> into CH<sub>4</sub> at the same temperature was conducted after switching the feed gas to 5% H<sub>2</sub>/N<sub>2</sub> (50 mL min<sup>-1</sup>). The spectra ranging from 4000 to 400 cm<sup>-1</sup> were collected with a resolution of 4 cm<sup>-1</sup>.

#### 3. Results and discussions

#### 3.1. Characterization of fresh catalysts

The elemental analysis of pristine CeO<sub>2</sub> and reduced Ru/CeO<sub>2</sub> catalysts is studied by ICP-OES. The obtained results are summarised in Table 1. It is found that there are no Ru species in pristine CeO<sub>2</sub>, which is consistent with the predetermined metal contents. After impregnating Ru on CeO<sub>2</sub> nanorods, the percentage of Ru element is calculated as 3.52%, 6.60% and 12.75%, respectively, which are used to investigate the influence of Ru loadings in the ICCU process.

Ru element percentage <sup>a</sup>	CeO <sub>2</sub> <sup>b</sup>	SBET <sup>C</sup>	Ru dispersion <sup>d</sup>
(%)	( <b>nm</b> )	$(m^2 g^{-1})$	(%)
0	15.6	42	/
3.52	18.3	42	61.28
6.60	16.9	40	23.69
12.75	16.8	27	5.29
	Ru element percentage <sup>a</sup> (%) 0 3.52 6.60 12.75	Ru element percentage <sup>a</sup> CeO2 <sup>b</sup> (%)         (nm)           0         15.6           3.52         18.3           6.60         16.9           12.75         16.8	Ru element percentage <sup>a</sup> CeO2 <sup>b</sup> SBET <sup>c</sup> (%)         (nm)         (m <sup>2</sup> g <sup>-1</sup> )           0         15.6         42           3.52         18.3         42           6.60         16.9         40           12.75         16.8         27

Table 1 Elemental analysis and average crystallite size of reduced catalysts.

<sup>a</sup> Element percentage calculated from ICP results.

<sup>b</sup> Average crystallite size obtained from Scherrer's equation.

<sup>c</sup> BET surface area.

<sup>d</sup> Ru dispersion obtained from CO chemisorption.



Fig. 2. XRD patterns (a) and CO<sub>2</sub>-TPD profiles (b) of CeO<sub>2</sub> nanorods and Ru/CeO<sub>2</sub> catalysts.

The X-ray diffractogram of reduced pristine CeO<sub>2</sub> nanorods and Ru/CeO<sub>2</sub> catalysts with different Ru loadings, as well as the reference peak positions of hcp-structured Ru (JCPDS 6-0663) is presented in Fig. 2. The peaks centred at 28.5°, 33.2°, 47.6°, 56.5°, 59.2°, 69.4°, 76.7° and 79.1° are assigned to the lattice plane of (111), (200), (220), (311), (222), (400), (331) and (420), respectively in the cubic structure of CeO<sub>2</sub> (JCPDS 34-0394) [19]. The average CeO<sub>2</sub> crystallite size is calculated as 15.6, 18.3, 16.9, 16.8 nm for CeO<sub>2</sub>, 2.5Ru/CeO<sub>2</sub>, 5Ru/CeO<sub>2</sub> and 10Ru/CeO<sub>2</sub>, respectively, using Scherrer's equation. However, no distinct diffraction peaks belonging to Ru or RuO<sub>2</sub> species can be detected in the reduced and non-reduced Ru/CeO<sub>2</sub> catalysts, respectively in Fig. 2 and Fig. S2. This indicates that the Ru active sites are well dispersed on CeO<sub>2</sub> nanorods or partly incorporated into the lattices of CeO<sub>2</sub> nanorods [27].

 $CO_2$ -TPD profiles of pristine CeO<sub>2</sub> and Ru/CeO<sub>2</sub> catalysts are displayed in Fig. 2b. Two CO<sub>2</sub> desorption peaks centred at 106 °C and 324 °C are attributed to the weak and strong CO<sub>2</sub> chemisorption, respectively indicating the basic property of CeO<sub>2</sub> nanorod as reported in the previous study [28]. With the increase of Ru loading, the intensity of CO<sub>2</sub> desorption peaks is increased, which implies the Ru species can enhance the basic sites and resulting a better CO<sub>2</sub> adsorption ability.



**Fig. 3.** TEM images of reduced catalysts CeO<sub>2</sub> (a), 2.5Ru/CeO<sub>2</sub> (b), 5Ru/CeO<sub>2</sub> (c) and 10Ru/CeO<sub>2</sub> (d). HRTEM (e) and element mapping (f-h) of reduced 5Ru/CeO<sub>2</sub>.

SEM images of the synthesized Ru/CeO<sub>2</sub> catalysts and corresponding element mapping of 5Ru/CeO<sub>2</sub> are shown in Fig. S3. It is found that the Ru/CeO<sub>2</sub> catalysts can inherit the original morphology of CeO<sub>2</sub> after introducing Ru active sites. The detailed morphologies and active components of CeO<sub>2</sub> support and Ru/CeO<sub>2</sub> are determined by TEM and HRTEM, as well as element mapping analysis as displayed in Fig. 3. The width and length of the well-crystallized CeO<sub>2</sub> nanorods prepared by the hydrothermal method is ranging from 10 to 20 nm and 100 to 200 nm, respectively, as shown in Fig. 3a. The EDX spectrum as shown in Fig. S4 proves the successful introduction of Ru species on CeO<sub>2</sub> support. As for the reduced 5Ru/CeO<sub>2</sub>, the interplanar spacing of 0.206 nm and 0.312 nm represent lattice plane (101) of Ru and (111) of CeO<sub>2</sub>, respectively [29]. The element mappings of 5Ru/CeO<sub>2</sub> as shown in Fig. 3f-h and Fig. S3e-f demonstrate the uniform distribution of Ce, Ru and O elements, which is important to prevent the aggregation of Ru species. In addition, with the further increase of Ru loadings, the length of CeO<sub>2</sub> nanorods and the surface

area are decreased as shown in Fig. 3c, d and Table 1. In addition,  $2.5Ru/CeO_2$  exhibits a much higher Ru dispersion (61.28%) than that of  $5Ru/CeO_2$  and  $10Ru/CeO_2$  from the CO chemisorption results in Table 1.



#### 3.2. Oxygen vacancies of fresh catalysts

Fig. 4. H<sub>2</sub>-TPR profiles of CeO<sub>2</sub>, 2.5Ru/CeO<sub>2</sub>, 5Ru/CeO<sub>2</sub> and 10Ru/CeO<sub>2</sub>.

The close relationship between metal-support interaction and oxygen vacancies has received intensive attention due to the promotion for the catalytic reaction [30]. Therefore, a further insight of the mentioned relationship was studied using TPR, Raman and XPS. The reducibility of CeO<sub>2</sub> support and Ru/CeO<sub>2</sub> catalysts is studied by H<sub>2</sub>-TPR in Fig. 4. In the reduction process of CeO<sub>2</sub> support, the temperature below 500 °C and higher than 700 °C is normally attributed to the reduction of surface CeO<sub>2</sub> and bulk CeO<sub>2</sub>, respectively [27]. For the Ru/CeO<sub>2</sub> catalyst, there is a shoulder peak lower than 100 °C due to the oxygen adsorption [26]. Two other peaks centred at 120-160 °C (peak I) and 200-260 °C (peak II) are observed, which are attributed to the interaction between  $RuO_x$  species and  $CeO_2$  supports [27]. The temperature of peak I is gradually decreased from 138 °C in 10Ru/CeO<sub>2</sub> to 128 °C in 2.5Ru/CeO<sub>2</sub>, which is attributed to the reducibility was improved [31]. Compared to pristine CeO<sub>2</sub>, ceria support in Ru/CeO<sub>2</sub> catalyst exhibits a lower reduction temperature, indicating that the introduction of Ru species promote the reduction of ceria. In addition, a quantitative H<sub>2</sub> consumption for RuO<sub>2</sub> reduction as shown in Table 2 greatly exceeds the stoichiometric H<sub>2</sub> consumption for the complete reduction of RuO<sub>2</sub> (15.0 mmol/g RuO<sub>2</sub>). This phenomenon indicates that a large amount of H<sub>2</sub> is used to remove the surface oxygen of ceria and sequentially generate the oxygen vacancies [32].



Fig. 5. Visible Raman spectra of CeO<sub>2</sub>, 2.5Ru/CeO<sub>2</sub>, 5Ru/CeO<sub>2</sub> and 10Ru/CeO<sub>2</sub>.

Except for the metal active sites, the oxygen vacancies in the Ru/CeO<sub>2</sub> catalysts may serve as an important cooperative site for CO<sub>2</sub> conversion. Raman spectra are employed to investigate the concentration and formation of oxygen vacancies as shown in Fig. 5. The sharp peak at 462 cm<sup>-1</sup> indicates the presence of vibration mode of octahedral local symmetry around CeO<sub>2</sub> lattice (F<sub>2g</sub>). Another peak at 598 cm<sup>-1</sup> is assigned to the defect-induced (D) mode in CeO<sub>2</sub> phase. After the introduction of Ru active species, those Raman peaks remained. However, compared to the pristine ceria, the peak corresponding to F<sub>2g</sub> exhibited a red shift, which is attributed to the presence of oxygen vacancies derived from the introduction Ru into CeO<sub>2</sub> nanorods [33]. In addition, another weak peak centred at 1174 cm<sup>-1</sup> is attributed to the second-order longitudinal modes of CeO<sub>2</sub> [34]. The intensity ratio of  $I_D/I_{F2g}$  is defined as the concentration of oxygen vacancies in CeO<sub>2</sub>, which increases in the order of CeO<sub>2</sub> (0.018) < 2.5Ru/CeO<sub>2</sub> (0.047) < 5Ru/CeO<sub>2</sub> (0.051) < 10Ru/CeO<sub>2</sub> (0.072) as shown in Table 2. Importantly, the  $I_D/I_{F2g}$  ratio increases significantly due to the addition of Ru on the CeO<sub>2</sub> nanorod support, which indicates the crucial role of the H<sub>2</sub> reduction in the formation of oxygen vacancies.



Fig. 6. XPS spectra and peak fitting curves Ce 3d (a), Ru 3d (b) and O 1s (c) of reduced catalysts.

Sample .	H <sub>2</sub> consumption <sup>a</sup>	Raman	Ru 3d	Ce 3d	O 1s
	(mmol/g RuO <sub>2</sub> )	$I_{\rm D}/I_{\rm F2g}$	$Ru^{\delta +}/(Ru^{\delta +}+Ru^0)$	Ce <sup>3+</sup> /Ce <sup>4+</sup>	Ov/OL
CeO <sub>2</sub>	/	0.018	/	0.37	0.38
2.5Ru/CeO <sub>2</sub>	25.6	0.047	0.22	0.37	0.51
5Ru/CeO <sub>2</sub>	20.9	0.051	0.35	0.39	0.53
10Ru/CeO <sub>2</sub>	20.4	0.072	<mark>0.41</mark>	0.56	1.56

Table 2 TPR, Raman and XPS data of the reduced CeO<sub>2</sub> and Ru/CeO<sub>2</sub>.

<sup>a</sup>  $H_2$  consumption calculated by  $H_2$ -TPR

XPS spectra for the pristine CeO<sub>2</sub> and Ru/CeO<sub>2</sub> catalysts are conducted for the study of valence states and chemical composition and the results are displayed in Fig. 6. Eight main binding energy peaks can be observed in Fig. 6a. The six peaks centred at 916.3, 907.4, 900.6, 898.0, 888.9 and 881.8 eV are assigned to Ce<sup>4+</sup>, and the two peaks centred at 902.4 and 883.6 eV are ascribed to Ce<sup>3+</sup> [35]. The ratios of Ce<sup>3+</sup> to Ce<sup>4+</sup> are increased with the increase of Ru loadings as shown in Table 2 indicating that more oxygen vacancies are generated on the surface of CeO<sub>2</sub> nanorods.

The peaks of Ru 3d are deconvoluted to analyse the Ru species in different oxidation states, which are mainly composed of Ru<sup>0</sup> and Ru<sup> $\delta^+$ </sup> from Ru nanoparticles and the interface between Ru and CeO<sub>2</sub>, respectively [27]. The existence of Ru<sup> $\delta^+$ </sup> species is caused by the metal-support interaction with the electrons transferring from Ru to CeO<sub>2</sub> support as shown in Eq. (6), which could result in a better catalytic performance. The percentage of Ru<sup> $\delta^+$ </sup> is increased from 22% in 2.5Ru/CeO<sub>2</sub> to 41%

in  $10Ru/CeO_2$  implying that the catalytic activity would be enhanced with the increase of Ru loading.

$$Ru^{0} + {}^{\delta}Ce^{4+} \rightarrow Ru^{\delta_{+}} + {}^{\delta}Ce^{3+}$$
(6)

The presence of oxygen vacancies in the synthesized catalysts is further proved by O 1s spectra as shown in Fig. 6c. The peak at ~529.1 and ~531.8 eV is assigned to the lattice oxygen (O<sub>L</sub>) and oxygen deficient regions (O<sub>V</sub>), respectively. As shown in Table 2, with the increase of Ru loading,  $O_V/O_L$  exhibits an obvious increase which confirms the more oxygen vacancies are generated in a higher Ru loading catalyst [36, 37]. It agrees with the enhancement of Ce<sup>3+</sup> and Ru<sup> $\delta+$ </sup> peaks.

# *3.3. Integrated CO*<sup>2</sup> *capture and utilization performance*



**Fig. 7.** ICCU performance of CeO<sub>2</sub>-MgO (a); 2.5Ru/CeO<sub>2</sub>-MgO (b); 5Ru/CeO<sub>2</sub>-MgO (c) and 10Ru/CeO<sub>2</sub>-MgO (d).



**Fig. 8.** XRD patterns of MgO and spent DFMs (CeO<sub>2</sub>-MgO is after 2 ICCU cycles and others are after 10 ICCU cycles).

The ICCU performance of various DFMs is displayed in Fig. 7 and Table S1-3. As a comparison, CeO<sub>2</sub>-MgO demonstrates a low activity of CO<sub>2</sub> hydrogenation and almost no CH<sub>4</sub> can be observed in the second step (switching feed gas to 5% H<sub>2</sub>/N<sub>2</sub>) in Fig. 7a due to the absence of Ru active sites. The captured CO<sub>2</sub> is considered in the form of MgCO<sub>3</sub>, which is further confirmed by the MgCO<sub>3</sub> diffraction peaks centred at 32.6° and 53.9° in XRD results of the spent CeO<sub>2</sub>-MgO sample as shown in Fig. 8. After introducing Ru species on CeO<sub>2</sub> nanorods, CH<sub>4</sub> can be clearly detected after switching to 5% H<sub>2</sub>/N<sub>2</sub> in the ICCU process, and only a small amount of CO<sub>2</sub> and almost no CO can be observed for all the DFMs during the methanation process as shown in Fig. 7b-d. It is indicated that the captured CO<sub>2</sub> has been mostly utilised and converted into CH<sub>4</sub> when the feed gas was switched from CO<sub>2</sub> to 5% H<sub>2</sub>/N<sub>2</sub>. This is consistent with the superior methanation activity of Ru [38].

 Table 3 ICCU performance of DFMs.

	1 <sup>st</sup> cycle		1	10 <sup>th</sup> cycle	
Samples	CH <sub>4</sub> yield <sup>a</sup>	CO <sub>2</sub> conversion <sup>b</sup>	TOF <sup>c</sup>	CH <sub>4</sub> yield	CO <sub>2</sub> conversion
	(mmol $g^{-1}$ )	(%)	(h <sup>-1</sup> )	(mmol g <sup>-1</sup> )	(%)
2.5Ru/CeO <sub>2</sub> -MgO	5.73	60	113.4	1.13	39
5Ru/CeO <sub>2</sub> -MgO	6.60	74	361.6	3.36	79
10Ru/CeO <sub>2</sub> -MgO	7.07	89	1511.8	2.31	69

<sup>a</sup> calculated by per gram of sorbents

<sup>b</sup>CO<sub>2</sub> conversion= CH<sub>4</sub> yield/CO<sub>2</sub> capture capacity

<sup>c</sup> TOF= Number of moles of reactant consumed/ (number of active centres\*reaction time)

Regarding CO<sub>2</sub> utilisation, the CH<sub>4</sub> yield, CO<sub>2</sub> conversion as well as TOF derived from different DFMs are summarized in Table 3. As for the 1<sup>st</sup> cycle of ICCU process, 2.5Ru/CeO<sub>2</sub>-MgO exhibits a relatively low CH<sub>4</sub> yield (5.73 mmol g<sup>-1</sup>) and CO<sub>2</sub> conversion (60%) due to the limited Ru active sites. The TOF is determined as low as 113.4 h<sup>-1</sup>. With the increase of Ru loadings, the CH<sub>4</sub> yield and CO<sub>2</sub> conversion are increased to 6.60 mmol g<sup>-1</sup> and 74% for 5Ru/CeO<sub>2</sub>-MgO and further increased to 7.07 mmol g<sup>-1</sup> and 89% for 10Ru/CeO<sub>2</sub>-MgO. In addition, TOF displayed a dramatic increase after introducing Ru species and reached 1511.8 h<sup>-1</sup> for 10Ru/CeO<sub>2</sub>-MgO, which is attributed to more oxygen vacancies are generated in the sample with a higher Ru loading as proved by XPS results in Table 2.



Fig. 9. Ten cycles of ICCU process of DFMs: CO<sub>2</sub> capture capacity (a) and CH<sub>4</sub> yield (b).



Fig. 10. XPS spectra and peak fitting curves: Ce 3d (a) and Ru 3d (b) of spent DFMs after 10 cycles of ICCU process.

The stability of synthesized DFMs are evaluated by 10 cycles of ICCU process and the results of CO<sub>2</sub> capture capacity and CH<sub>4</sub> yield are presented in Fig. 9. After 10 cycles of ICCU process, all these DFMs exhibit a decrease of CH<sub>4</sub> yield and CO<sub>2</sub> conversion as shown in Table 3 due to the sintering of MgO sorbent. This is further demonstrated in Fig. S5. The CH<sub>4</sub> yield obtained from 2.5Ru/CeO<sub>2</sub>-MgO drops from 5.73 mmol g<sup>-1</sup> to 1.13 mmol g<sup>-1</sup> after 10 cycles of ICCU as shown in Fig. 9b. Even though 10Ru/CeO<sub>2</sub>-MgO exhibits the best performance in the 1<sup>st</sup> cycle of ICCU process due to more oxygen vacancies, CO<sub>2</sub> capture capacity and CH<sub>4</sub> yield exhibits a dramatic decrease after 10 cycles of ICCU process from 7.90 mmol g<sup>-1</sup> and 7.07 mmol g<sup>-1</sup> to 3.33 mmol g<sup>-1</sup> and 2.31 mmol g<sup>-1</sup>, respectively. In addition, the CO<sub>2</sub> conversion and carbon balance also decreased from 89% and 99% to 69 and 87%, respectively as shown in Table S3. Compared to 2.5Ru/CeO<sub>2</sub>-MgO and 10Ru/CeO<sub>2</sub>-MgO, 5Ru/CeO<sub>2</sub>-MgO demonstrates a better stability. After 10 cycles of ICCU process, 5Ru/CeO<sub>2</sub>-MgO exhibits the highest CH<sub>4</sub> yield (3.36 mmol g<sup>-1</sup>) and CO<sub>2</sub> conversion (79%), which is more than 8 times than the performance of ICCU process reported by Bermejo-López et al. using Ru15%CaO/Al<sub>2</sub>O<sub>3</sub> and Ru10%Na<sub>2</sub>CO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> as the DFMs [21]. The detailed comparison of ICCU process proposed in this work and reported in other literatures are summarised in Table S4. In addition, the carbon balance and CO<sub>2</sub> conversion reaches up to 91% and 79%, respectively, which are much better than the performance reported by Sakpal et al. (CO<sub>2</sub> conversion is 75%) and Dreyer et al. (CO<sub>2</sub> conversion and CH<sub>4</sub> selectivity are 55% and 98%, respectively) [19, 39] as shown in Table S5. XPS spectra are employed to the analysis of chemical states of used DFMs after 10 cycles of ICCU process as displayed in Fig. 10 and Table S6. Compared to 2.5Ru/CeO<sub>2</sub>-MgO and 10Ru/CeO<sub>2</sub>-MgO, spent 5Ru/CeO<sub>2</sub>-MgO exhibits the highest ratio of Ce<sup>3+</sup> to  $Ce^{4+}$  and the highest  $Ru^{\delta+}$  percentage (63%) indicating more surface oxygen vacancies are generated after 10 cycles of ICCU process and resulting in a highest CH<sub>4</sub> yield and CO<sub>2</sub> conversion. This is also confirmed by the Raman spectra of DFMs after 10 cycles as shown in Fig. 11. The intensity ratio (I<sub>D</sub>/I<sub>F2g</sub> in Table S6) of spent 5Ru/CeO<sub>2</sub>-MgO is much higher than that of spent 2.5Ru/CeO<sub>2</sub>-MgO and 10Ru/CeO<sub>2</sub>-MgO further indicating the existence of more oxygen vacancies.



Fig. 11. Visible Raman spectra of DMFs after 10 cycles of ICCU process.

It is well accepted that the catalytic activity can be enhanced by the interaction between reducible supports and oxygen vacancies, which promote CO<sub>2</sub> activation and be restored through the reduction of the oxide surface [40]. The in-situ DRIFTS were further conducted for the mechanism study of ICCU process under the co-existence of Ru active sites and oxygen vacancies. As shown in Fig. 12, 1350 cm<sup>-1</sup> and 1550 cm<sup>-1</sup> are considered as the characteristic peaks of v(O-C-O) in the formate species and  $v_{as}$ (COO<sup>-</sup>) in the carbonate species, respectively [41]. Compared to the carbon capture stage, the spectra of CeO<sub>2</sub>-MgO after switching to H<sub>2</sub> for conversion remained unchanged in Fig. 12a, while the peak of 5Ru/CeO<sub>2</sub>-MgO at 1350 cm<sup>-1</sup> disappears gradually. This indicates that the formed formate species in CO<sub>2</sub> capture stage are consumed in the conversion reaction. Thus, formate is proposed to be the main reaction intermediate in this ICCU using the synthesized DFMs. This proposal can also be confirmed by the existence of peaks at 2032 cm<sup>-1</sup> in 5Ru/CeO<sub>2</sub>-MgO, which are attributed to the linearly adsorbed CO over the low-coordinated Ru sites [33].

The reaction mechanism for the conversion of captured  $CO_2$  via formate route over the Ru/CeO<sub>2</sub> catalyst is proposed in Fig. 13. Two key steps are involved. 1) CO<sub>2</sub> species are activated by an oxygen vacancy and the CeO<sub>2</sub> nanorod is oxidised, meanwhile the Ru active site is chemisorbed with H species. The first step results in the formation of bidentate formate, which will decompose into metal carbonyl and terminal hydroxyl groups. 2) The Ru carbonyls are activated by chemically adsorbed H atoms, and finally converted to CH<sub>4</sub> molecules, which is a rate determining step [42]. The formed hydroxyl groups on the oxygen vacancies react with hydrogen resulting in the

formation of  $H_2O$ , which is the reduction of  $CeO_2$  support. Therefore, the DFMs with more oxygen vacancies coupled with a good Ru dispersion exhibit a better ICCU performance.



**Fig. 12.** In-situ DRIFTS spectra during the ICCU process over CeO<sub>2</sub>-MgO (a) and 5Ru/CeO<sub>2</sub>-MgO (b).



**Fig. 13.** Schematic illustration for the conversion of captured CO<sub>2</sub> via formate route over the Ru/CeO<sub>2</sub> catalyst.

The SEM images of spent DFMs (except for CeO<sub>2</sub>-MgO is after 2 cycles, all other DFMs are after 10 cycles of ICCU process) and the corresponding TEM images of spent 5Ru/CeO<sub>2</sub>-MgO have been displayed in Fig. 14. It should be noted that the rod-like material in Fig. 14a is the quartz wool used

during the ICCU process. Nanorods can be observed on the surface of spent CeO<sub>2</sub>-MgO, indicating that CeO<sub>2</sub>-MgO can inherit its original morphology. Compared to the bulk structure of spent 2.5Ru/CeO<sub>2</sub>-MgO and 10Ru/CeO<sub>2</sub>-MgO, the spent 5Ru/CeO<sub>2</sub>-MgO catalyst after 10 cycles of ICCU process exhibits a loose structure in Fig. 14c indicating the sintering resistance, which is also confirmed by the uniform mixture of MgO sorbent and CeO<sub>2</sub> nanorods as shown in Fig. 14e and f (TEM images) [43]. Therefore, compared to both the traditional CO<sub>2</sub> methanation and ICCU process reported in the previous literatures, the ICCU process using MgO and Ru as the sorbent and active site, respectively demonstrates a high CO<sub>2</sub> conversion and CH<sub>4</sub> selectivity coupled with a good stability.



Fig. 14. SEM and TEM images of DFMs after 10 cycles of ICCU process: CeO<sub>2</sub>-MgO (a), 2.5Ru/CeO<sub>2</sub>-MgO (b), 5Ru/CeO<sub>2</sub>-MgO (c, e, f) and 10Ru/CeO<sub>2</sub>-MgO (d).

#### 4. Conclusions

A novel ICCU process for carbon capture and methane production has been demonstrated using DFMs, which is a physical mixture of an inexpensive high-capacity MgO sorbent and  $CO_2$  methanation catalyst (Ru supported on the CeO<sub>2</sub> nanorods) by the mass ratio of 2:1. In this ICCU

process, the regeneration of the sorbent and the conversion of cpatured CO<sub>2</sub> are carried out in a single reactor at the same intermediate temperature (300 °C) simultaneously, reducing the energy requirement for the sorbent regeneration. The produced CH<sub>4</sub> can be used based on existing infrastructure while the reduction of CO<sub>2</sub> emission is fulfilled. It is found that 10Ru/CeO<sub>2</sub>-MgO exhibits highest CH<sub>4</sub> yield (7.07 mmol g<sup>-1</sup>) and CO<sub>2</sub> conversion (89%) in the 1<sup>st</sup> cycle of ICCU process due to more oxygen vacanies are generated. However, 5Ru/CeO<sub>2</sub>-MgO remains most oxygen vacanies caused by the metal-spport interaction compared to other DFMs and demonstrates the highset CH<sub>4</sub> yield (3.36 mmol g<sup>-1</sup>) and CO<sub>2</sub> conversion (79%) after 10 cycles of ICCU process.

#### Acknowledgements

The authors thank the financial support from National Natural Science Foundation of China (No. 21706050) and the China Scholarship Council (No. 201606450016). The authors also thank the funding from the European Union's Horizon 2020 research and innovation programme under the Marie Skłodowska-Curie Grant Agreement (No. 823745).

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