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Pokhrel, S., Waters, B., Felton, S., Huang, Z. F., & Nadgorny, B. (2021). Percolation in metal-insulator composites of randomly packed spherocylindrical nanoparticles. *Physical Review B*, 103(13), [134110]. <https://doi.org/10.1103/PhysRevB.103.134110>

Published in:
Physical Review B

Document Version:
Peer reviewed version

Queen's University Belfast - Research Portal:
[Link to publication record in Queen's University Belfast Research Portal](#)

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Percolation in metal-insulator composites of randomly packed spherocylindrical nanoparticles

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(Dated: March 31, 2021)

While classical percolation is well understood, percolation effects in randomly packed or jammed structures are much less explored. Here we investigate both experimentally and theoretically the electrical percolation in a binary composite system of disordered spherocylinders, to identify the relation between structural (percolation) and functional properties of nanocomposites. Experimentally, we determine the percolation threshold p_c and the conductivity critical exponent t for composites of conducting (CrO_2) and insulating (Cr_2O_3) rodlike nanoparticles that are nominally geometrically identical, yielding $p_c = 0.305 \pm 0.026$ and $t = 2.52 \pm 0.03$ respectively. Simulations and modeling are implemented through a combination of the mechanical contraction method and a variant of random walk (de Gennes ant) approach, in which charge diffusion is correlated with the system conductivity via the Nernst-Einstein relation. The percolation threshold and critical exponents identified through finite size scaling are in good agreement with the experimental values. Curiously, the calculated percolation threshold for spherocylinders with an aspect ratio of 6.5, $p_c = 0.312 \pm 0.002$, is very close (within numerical errors) to the one found previously in two other distinct systems of disordered jammed spheres and simple cubic lattice, an intriguing and surprising result.

I. INTRODUCTION

The concept of percolation enables a connection between the long-range connectivity of randomly distributed objects within a network to global properties of the system spanned by this network. The behavior of such systems can be described by a standard model in which a random probabilistic process shows a continuous phase transition from a finite size percolating cluster below a critical value of the percolation threshold p_c to an infinite cluster above p_c [1]. Percolation is indispensable in interpreting a wide variety of physical, chemical, mechanical, and biological phenomena occurring in disordered systems, from the spread of diseases [2], thermal transport [3], electrical conduction in composites [4], to metal-insulator [5], magnetic [6], and spin quantum Hall [7] phase transitions, and to pharmaceutical drug delivery [8, 9]. Electrical conductivity in a percolating system can be modeled by progressively adding larger numbers of identical conducting particles to an insulating matrix until a geometrically connected conducting phase is generated. The electrical conductivity σ then scales as $\sigma \propto (p - p_c)^t$, where p_c is the percolation threshold, the critical value of the concentration or fraction p of the conducting particles, and t is a critical exponent. The percolation threshold is normally dependent on the specific system configuration and the geometry of constituent particles. On the other hand, the critical exponent t was expected to be universal, i.e., independent of details of system structures and components ($t = \mu \simeq 2$

in three dimensions [1]), whereas more recent studies indicated the nonuniversality of t , the values of which were found to range from 1.3 to 4.0 or even higher in various composites [10–12].

While the classical percolation picture described above has been well established, a variant of this problem which addresses the percolation effects of particles packed in disordered (random) or jammed structures is much less thoroughly explored and understood [13] (see Fig. 1 for some examples of such disordered packings). Compared to lattice-like, ordered structures, randomly packed systems usually have different packing fractions, which, in turn, would affect the critical behavior of the system and could play a key role in defining the functionality of the sample. A recent example is the occurrence of double percolation observed in a disordered binary mixture [14], in which both types of particles (CrO_2 and MgB_2) are conducting or superconducting but their volume fraction vs conductivity relation shows an insulating region in between two separate percolation thresholds. These two thresholds, corresponding to the conductor-insulator and superconductor-insulator transitions respectively, arose from the suppressed interface conduction between a half-metal (CrO_2) and a superconductor (MgB_2) [15, 16] and the large geometric disparity between particles in this rod-sphere system of binary species [14]. This effect underscores the fundamental and practical importance of the percolation threshold and the relationship between the thresholds, geometric contrast of constituent particles, and the transport properties of the system for various particle networks.

While percolation thresholds and the critical behavior in many ordered three-dimensional (3D) lattices of fixed coordination numbers have been investigated in detail [1, 4, 17–21], much less is known about systems

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FIG. 1. Sample systems of disordered packing, including closely packed homegrown lemons (top-left panel), a simulation snapshot of randomly packed conducting (green, with $p = 0.33$) and insulating (red) spherocylinders near the percolation threshold (top-right panel), and an SEM image of the densely packed $\text{CrO}_2/\text{Cr}_2\text{O}_3$ experimental sample at approximately the same fraction p (bottom panel). The average width and length of the $\text{CrO}_2/\text{Cr}_2\text{O}_3$ nanoparticles are measured to be approximately 40 nm and 300 nm, respectively.

of disordered packing which form networks of interparticle contacts with variable coordination numbers [22]. In these cases where the constituent particles could be of various types and geometries, such as particle shape and size, and the average number of nearest neighbors may be close to that in a specific ordered lattice, they are lacking long-range order and are randomly or quasi-randomly distributed with a broad range of neighboring particle contact numbers. To develop the methodology for identifying the corresponding percolation properties (such as percolation thresholds and critical exponents) and their correlation to the system functionalities, we will first limit ourselves to a more manageable problem related to dense random distribution of particles of the same size and shape, specifically the disordered mixture of two-component spherocylinders that are geometrically identical but functionally distinct, given that the understanding of this type of system is still lacking.

In this paper, we report both experimental and computational results for a randomly packed system comprising a binary mixture of nominally identical $\text{CrO}_2/\text{Cr}_2\text{O}_3$

spherocylinders (capsules); see Fig. 1 for a simulation snapshot (top-right panel) and a scanning electron microscopy (SEM) image of the system studied. Specifically, we study a dense disordered network of conducting and insulating spherocylinders of approximately the same size and aspect ratio. To examine the electrical percolation in this system, we first convert the conducting CrO_2 rodlike nanoparticles (spherocylinders with an average aspect ratio of 6.5) into nominally geometrically identical insulating Cr_2O_3 nanoparticles, and then prepare a series of samples of $\text{CrO}_2/\text{Cr}_2\text{O}_3$ mixture with varying conducting vs insulating volume fractions for electrical transport measurements. The experimental results are compared with large-scale 3D computer simulations and calculations on the corresponding binary disordered composite of non-overlapping hard spherocylinders, which are conducted through a combination of mechanical contraction and Monte Carlo methods and a random walk approach based on the de Gennes ant and the Nernst-Einstein relation.

Good agreement is obtained between our results from experiments and computation, for various percolation and electrical transport properties of this binary network of disordered packing. These include the percolation threshold $p_c = 0.305 \pm 0.026$ (experiment) and $p_c = 0.312 \pm 0.002$ (simulation), and the scaling behavior near the threshold and the corresponding critical exponent of the electrical conductivity, with $t = 2.52 \pm 0.03$ and a lower bound $\mu_l = 1.26$ identified through $t \leq 2\mu_l$ [12] (experiment) and $\mu = 1.62 \pm 0.04$ (simulation). The small discrepancy between the experimental and theoretical values can be partially attributed to the intrinsic polydispersity of the nanoparticles and some degree of local ordering of the composite used in experiments (see Fig. 1).

An intriguing finding is the calculated value of $p_c = 0.312 \pm 0.002$ in this binary system of dense randomly-packed (but not strictly jammed) spherocylinders with an aspect ratio of 6.5. This value is very close (within computational errors) to the site percolation threshold of $p_c = 0.3116(3)$ computed recently for disordered jammed spheres [22] and $p_c = 0.311608$ obtained earlier for simple cubic lattice [17, 19]. These are three distinct systems, with different packing fractions, degree of ordering, particle geometry, and different distribution of particle coordination numbers (although with similar values of average coordination numbers). While such an agreement may be accidental for any two systems, it is harder to assume that the same coincidence would occur for the three different systems, where the constraints of the ordered lattice and particle shape are being gradually removed. Hence, one may argue that this result manifests the existence of universality for the percolation threshold in a particular class of systems. Apart from pointing to the closeness of the average coordination numbers in all three systems, a plausible explanation of this result is still lacking; it remains an important open question.

II. EXPERIMENTS

A. Sample preparation and structural characterization

Here experimental measurements are conducted to study the electrical transport property of $\text{CrO}_2/\text{Cr}_2\text{O}_3$ half-metal/insulator nanocomposites at different fractions of CrO_2 . The CrO_2 and Cr_2O_3 nanoparticles are needle-shaped spherocylinders (see Fig. 1) of similar size, with the average length of approximately 300 nm and diameter of about 40 nm, corresponding to an average aspect ratio of 6.5. Composite $\text{CrO}_2/\text{Cr}_2\text{O}_3$ samples were prepared by mixing metallic ferromagnetic oxide CrO_2 nanoparticles with insulating Cr_2O_3 nanoparticles. The latter were formed by annealing commercially available CrO_2 (DuPont) nanoparticles at 550°C for 1 hour, using the procedure described in Ref. [23].

The resulting nanoparticles were then analyzed by x-ray diffraction (XRD) spectroscopy to confirm the complete conversion of half-metallic CrO_2 into insulating Cr_2O_3 nanoparticles. XRD spectra over a wide range of diffraction angles 2θ (varying from 10° to 80°) was collected with the help of an x-ray powder diffractometer (*Rigaku Miniflex*), using $\text{Cu } K\alpha$ radiation of wavelength $\lambda = 1.5418 \text{ \AA}$. The x-ray generator was operated at 40 kV with an anode current of 20 mA from stabilized power supplies. The scan was performed at a scanning rate of 1° per minute over the range of angles $10^\circ < 2\theta < 80^\circ$. Both annealed and unannealed samples of CrO_2 were analyzed by XRD, with results given in Fig. 2. Before annealing, peaks appear at 2θ angles of approximately 28° , 36° , 45° , ... These peaks correspond to the reflected intensity from the (110), (101), (211), ... planes of the tetragonal structure of CrO_2 . Based on the Scherrer formula, the typical crystalline size L_s of the CrO_2 nanoparticle is dependent on the wavelength λ , the line broadening $B(2\theta)$ which is the full width at half-maximum, and the Scherrer constant K (at the order of 1): $L_s \simeq K\lambda/[B(2\theta) \cos \theta] \sim 30 \text{ nm}$, which is close to the diameter of the spherocylinder. This estimate is consistent with the result of the high resolution STEM imaging (not shown), indicating good crystallinity of individual nanoparticles. Upon annealing, a clear signature of Cr_2O_3 peaks has been observed at (012), (104), (024), ..., as shown in Fig. 2, confirming the presence of Cr_2O_3 . This is accompanied by noticeably higher peak broadening, indicating a reduced crystalline size of Cr_2O_3 nanoparticles. Approximately 5 mm diameter pellets with 0.5 mm thickness were formed from the mixture of conducting CrO_2 and insulating Cr_2O_3 particles, using a cold-press die with a uniaxial pressure of 10 GPa. An SEM micrograph of a typical sample is shown in Fig. 1.

FIG. 2. The XRD intensity vs 2θ plots, with the peaks corresponding to the original CrO_2 nanoparticles before annealing and Cr_2O_3 nanoparticles after annealing.

B. Electrical characterization

Four-point electrical transport measurements were performed in a Quantum Design Physical Property Measurement System (PPMS), which allows a wide range of resistance measurements at variable temperatures. Gold wires were attached to the pellet using silver paste, and the sample was then mounted on a PPMS puck using GE varnish. The variation of resistivity as a function of fraction p of CrO_2 particles in a $\text{CrO}_2/\text{Cr}_2\text{O}_3$ composite was measured using PPMS in the temperature range $200 \text{ K} \leq T \leq 300 \text{ K}$. At each nominal composition at least two different samples were prepared. The resistivity was measured using the four-probe technique, which eliminates parasitic contributions from electrical contacts [24]. Experimental errors originated primarily from the geometric factors, such as the finite contact size and the contact placement uncertainty, as well as variations in the sample thickness and anisotropy. In addition to the classical percolation threshold reported here, we have observed tunneling percolation thresholds at lower fractions p , manifested by tunneling staircases similar to those described in Refs. [25, 26]. The detailed results of these measurements will be presented elsewhere.

Electrical characterization of nanocomposites for varying fractions of the conducting particles (CrO_2) was performed at five different temperatures, 300 K, 270 K, 250 K, 220 K, and 200 K, with the results shown in Fig. 3 and summarized in Table I. The values of the percolation threshold p_c were determined by optimizing nonlinear regression for $\log \sigma = A + t \log(p - p_c)$ (plots not shown) from these five independent measurements of the sample conductivity σ , as listed in Table I. Note that the con-

FIG. 3. Sample resistivity as a function of fraction p of CrO_2 at five different temperatures (a) $T = 300$ K, (b) $T = 270$ K, (c) $T = 250$ K, (d) $T = 220$ K, and (e) $T = 200$ K. Insets: Sample conductivity as a function of $p - p_c$ in log-log scale to identify the critical exponent t (where the error of p_c determined from a separate nonlinear fitting procedure has been incorporated).

TABLE I. Values of percolation threshold p_c and conductivity critical exponent t obtained from experimental measurements at different temperatures T .

T	p_c	t
300 K	0.360 ± 0.024	2.51 ± 0.05
270 K	0.295 ± 0.057	2.46 ± 0.06
250 K	0.307 ± 0.062	2.45 ± 0.06
220 K	0.315 ± 0.040	2.54 ± 0.05
200 K	0.293 ± 0.062	2.70 ± 0.08

ductivity of metallic CrO_2 in this temperature range is only weakly temperature dependent, while Cr_2O_3 components are at least an order of magnitude more resistive at $T = 250$ K as compared to room temperature (see Fig. 3). Thus, the conductivity at $T = 300$ K is affected by the leakage current through Cr_2O_3 nanoparticles and hence was excluded from the determination of the p_c and t values of the conducting-insulating system. Averaging over the four lower temperature values of p_c , we identify the percolation threshold as $p_c = 0.305 \pm 0.026$ for this nanocomposite system (using the proper weighted mean with the uncertainty evaluated via the standard error propagation). To perform the consistency check of these results, we used two supplementary methods for the threshold determination. In the first, the steepest descent (gradient) approximation [27], the threshold was associated with the extremum of the derivatives of

$\log \sigma$ plotted as a function of p . In the second method, we used temperature-dependent transport measurements to identify inflection points in the plot of the ratios of sample resistances at a given temperature to the room-temperature values, as described in Ref. [26]. The values of p_c obtained from all these three methods coincide within the experimental accuracy.

Once the percolation threshold at a given temperature was identified, we used its value (with the corresponding error correction) in standard log-log plots to determine the conductivity critical exponent t . The results are shown in the insets of Fig. 3 (see also Table I), demonstrating the scaling behavior of conductivity above the percolation threshold p_c . The average of four lower temperature results yields $t = 2.52 \pm 0.03$. This value of conductivity exponent for binary disordered spherocylinders is comparable to some previous results of 3D conductive networks, such as $t = 2.16$ for the conductor-insulator transition in $\text{CrO}_2/\text{MgB}_2$ (spherocylinder/sphere) double-percolating composites [14] and those found in various disordered composites [10, 11].

III. SIMULATIONS

A. Methods

1. The mechanical contraction method for random packing

To model the structure of a given nanocomposite, it is essential to produce dense random packings of its constituent hard particles in simulations. Conventional Molecular Dynamics simulations are too computationally expensive to be practical when the precise microstates of the system are not essential [28]. Standard Monte Carlo methods inherently sample the equilibrium distribution of particle states [29], while making rapid compression into a disordered, out-of-equilibrium state is not compatible with the premise of the model. Additionally, this results in poor performance since in a dense state an unacceptably high fraction of trial moves would fail the Metropolis criterion [30] for hard particles; that is, a vast majority of potential translations or rotations of particles produce states where particles overlap with their neighbors. These states are invalid and thus must be rejected.

Because of these limitations, here we use an alternative algorithm designed explicitly to produce random packings, the Mechanical Contraction Method (MCM), as developed in Ref. [31]. The premise of MCM is to take a system of spherocylinder particles in an initial low density random state, and bring them together directly, moving each particle only when it would collide with another and only just enough to avoid overlaps. By this approach, the initial entropy of the low density phase is carried through the compression until the entire system can no longer be transformed to a higher density state [32]. Details of the method are given in Ref. [31], with the implementation steps summarized below.

First, the particles' positions and orientations are randomized at low density (with packing fraction < 0.01) by a number of hard particle Monte Carlo moves. At such low densities, virtually all trial moves succeed; thus this step can be performed quickly, even for large systems. This provides the initial state for the MCM. Using the MCM algorithm, the whole system is then scaled down by a small volume factor ΔV , and the position of every particle is scaled down accordingly, bringing them uniformly together. The algorithm searches over all particles in the system in arbitrary order, to identify neighboring particles that might be overlapping. This is straightforward for spherocylinders which can be characterized as a set of points within radius R of a line segment of length l . If the shortest distance k between the two particles' axes of symmetry (within $l/2$ from the particle centroid) is within $2R$, they must be overlapping. The amount of overlap is defined as $\delta = 2R - k$.

The strategy of the MCM algorithm is to move a particle i in a direction that reduces the total of its overlaps with neighboring contacted particles $j = 1, 2, \dots, C$ the most quickly. This direction is determined by maximizing the effective speed, which is a weighted combination

of translational and rotational velocities with respect to all of its C contacted particles [31]. Along this direction the particle i is moved sufficiently far to reduce the smallest overlap δ_j by a tiny amount more than $\delta_j/2$, so that when particle j is moved in the opposite direction by the same amount the pair will barely break contact, typically separated by 1.0001 times the needed distance. This will minimize the probability of producing new overlaps when moving the particles. This process is iterated until all overlaps are removed, whereupon the simulation box is further reduced. The procedure is repeated until the system cannot be further compressed with all the generated particle overlaps being removed (within a large enough cutoff number of trials).

We have implemented the MCM algorithm as a custom module in HOOMD-Blue, an open-source general purpose particle simulation engine [33–35] that was used for generating the related Monte Carlo moves in this algorithm (with excluded-volume interparticle interaction). The custom module developed is available at Ref. [36]. The acquired data were visualized using Ovito open-source particle visualization software [37] (see e.g., Fig. 1).

2. The random walk method for conductivity calculation

Determining the conductivity of large networks of irregularly connected particles presents a considerable challenge. To directly analyze the circuit formed by conducting particles and use Kirchhoff's laws requires the construction and solution of a large set of linear equations, a procedure that is time consuming. Moreover, the bulk conductivity of the system is likely insensitive to many small changes in network structure. A more efficient approach can be obtained by tracing a randomly-moving test charge through the system and calculating its diffusion property, in a method analogous to the so-called de Gennes "ant in a labyrinth" [38] and "termite" [39], in concert with using the Nernst-Einstein relation.

This random-walk model was initially proposed by de Gennes to explore the percolation transition in cross-linked network systems [38], where he imagined a microscopic "ant" lost in a labyrinth of nodes, some of which are connected by bonds or chains. If these chains are sufficiently cross-linked to create a percolating network, there should be a finite probability that from any arbitrary starting point the ant could walk along the network to cover infinite distance. Later theoretical work expanded upon this simple percolation test and used this random-walk approach to measure properties related to the diffusion processes, connectivity, and transport in disordered systems or random networks [1, 40]. These include the use of the de Gennes ant to calculate the diffusion constant and hence the conductivity of the random resistor network through the Nernst-Einstein relation, the extension to the de Gennes termite [39] to study the random superconducting network consisting of

normal conductors and superconductors, and further to more complex cases of composites involving two [41] or three [42, 43] types of bonds with different conductances.

Here we use this random walk approach to obtain the conductivity of the disordered system of conducting-insulating spherocylinder nanoparticles, by imagining our ant as a test charge diffusing through the particle network, subject to the local conductivity of each particle. In practice, this is done by initializing the random walker on an arbitrarily chosen particle in the system consisting of all the clusters (i.e., the general ensemble [40]), following the procedure for a “blind ant” [44]. At each step, the walker (ant) located at particle i chooses at random one of the neighboring particles j which it is in contact with. The ant moves to that particle if it is conductive; otherwise the location of the ant remains unchanged. In either case the amount of time t taken by the ant is increased by one unit at every step. This corresponds to the assumption that in our system of $\text{CrO}_2/\text{Cr}_2\text{O}_3$ composites, only two types of particle-particle conductance are taken into account, with the interparticle hopping rates for a random walker being 1 and 0 respectively. The first case corresponds to the conductive type between two CrO_2 particles, while the second to the non-conductive type between two Cr_2O_3 particles or along a mixed CrO_2 - Cr_2O_3 link, neglecting any possible leakage current through Cr_2O_3 .

At the same time, each jump of the walker covers an amount of displacement, measured between the geometric centers of the particles, which is tracked and used to calculate the mean-square displacement $\langle r^2(t) \rangle$ as a function of total time t spent by the walker. (We have also evaluated $\langle r^2(t) \rangle$ based on the displacements between interparticle contacts, and obtained very similar results.) In our simulations the progress of each random walk was tracked for 10^6 steps through the system. The diffusion constant D can then be calculated via the relation $\langle r^2(t) \rangle \propto Dt$. It is, in turn, linearly proportional to the dc conductivity σ of the system via the Nernst-Einstein relation [40]

$$\sigma = (e^2/k_B T) n D, \quad (1)$$

where n is the density of the charge carriers. We can then map the behavior of the electrical conductivity of complex networks onto the diffusion property of random walks. In the disorderly packed system of binary composites studied here, the carrier density n is determined by the concentration of conductive (CrO_2) particles with fraction p ; thus it can be approximated as $n \sim pf$, where f is the packing fraction of all the particles (CrO_2 and Cr_2O_3) evaluated from simulations. In our calculations for each system size, this procedure was repeated with 20 different randomly selected starting particles (i.e., 20 independent walks) in each simulated configuration of binary spherocylinders, and the results were averaged over a large number of system configurations generated independently.

3. Finite size scaling

Continuum percolation models for disordered particle systems exhibit the same form of critical phenomena as the more-studied lattice percolation models by virtue of universality. This critical behavior is characterized by power-law scaling relations of geometrical, statistical, or some functional properties in terms of the particle probability or fraction p near the percolation threshold p_c [1], such as the scaling of conductivity $\sigma \propto (p - p_c)^\mu$ when $p \rightarrow p_c$ as examined here for the metal-insulator nanocomposite. Another important quantity is the correlation length ξ , scaling as $\xi \propto |p - p_c|^{-\nu}$, which represents the characteristic size of the finite clusters [1, 4].

In principle, all such critical behaviors are defined in the limit of infinite system sizes, requiring simulations to be related to the infinite system to obtain accurate scaling relations and critical exponents. It is particularly important for an accurate determination of p_c , because it defines the reference point of all the scaling relationships for the other critical properties of the system. The definition of p_c is the particle concentration or fraction at which the infinite system is first able to generate an infinite, percolating cluster. However, for finite systems what is measured instead is the effective percolation threshold as a function of the specific finite system size L , i.e., $p_c^{\text{eff}}(L)$. Thus the finite size scaling is needed to extract the infinite-system results of $p_c = p_c^{\text{eff}}(L \rightarrow \infty)$ and critical exponents from the finite-size simulations, for which we adopt the method of Ref. [45] as outlined below.

In practice, for each system size L , at a given value of p the probability $P(p, L)$ of getting at least one cluster of conducting particles that spans through the system across two sides of any direction is first evaluated over a number of independent realizations of system configurations (in the random packing state prepared by the mechanical contraction and MC methods described above). The value of $p_c^{\text{eff}}(L)$ can then be calculated by determining the value of p at which this spanning probability $P(p = p_c^{\text{eff}}, L) = 1/2$. $P(p, L)$ of a finite-size system is expected to follow the scaling relation [1]

$$P(p, L) = \Phi[(p - p_c)/\Delta(L)], \quad (2)$$

where Φ is the scaling function, and Δ is the percolation transition width which tends to decrease towards 0 as L increases towards the thermodynamic limit, typical of phase transitions. The percolation transition width scales as [1, 45]

$$\Delta(L) \propto L^{-1/\nu}, \quad (3)$$

which provides a simple way to determine the correlation-length exponent ν , leading, together with Eq. (2), to

$$p_c^{\text{eff}}(L) - p_c \propto L^{-1/\nu}, \quad (4)$$

a scaling relation that is used to obtain the accurate result of the percolation threshold p_c .

In the calculations this is done by fitting $P(p, L)$ with a function of the sigmoidal form. In Ref. [45] for a system of spheres, the scaling fitting function was chosen as $\{1 + \text{erf}[(p - p_c^{\text{eff}}(L))/\Delta(L)]\}/2$, i.e., the cumulative distribution function (CDF) for the normal distribution. In the currently studied system consisting of highly anisotropic spherocylinders, the probability distribution $P(p, L)$ does not have an antisymmetric form with respect to $P = 1/2$, as seen from our simulation results; thus, here the fitting function is assumed as the CDF for the skew normal (SN) distribution $\Phi_{\text{SN}}[(p - \xi)/\omega, \alpha]$, where the location, scale, and shape parameters of the SN distribution are denoted by ξ , ω , and α , respectively. If $\alpha = 0$ the CDF for the normal distribution (as used in Ref. [45]) is recovered. For each system size L , defining p_c^{eff} as the value when $\Phi_{\text{SN}}(p = p_c^{\text{eff}}) = 1/2$ and $y_0 = (p_c^{\text{eff}} - \xi)/\omega$, we have $\Phi_{\text{SN}}[(p - \xi)/\omega, \alpha] = \Phi_{\text{SN}}[(p - p_c^{\text{eff}})/\omega + y_0, \alpha]$, with very similar value of y_0 obtained from our simulation results of different L . Thus when setting $\omega \equiv \Delta(L)$, $P(p, L)$ can be fitted to the scaling function

$$P(p, L) = \Phi_{\text{SN}} \left[\frac{p - p_c^{\text{eff}}(L)}{\Delta(L)}, \alpha(L) \right]. \quad (5)$$

We have applied both fitting functions, i.e., CDFs for normal and skew normal distributions, to the simulation data, and obtained very similar results of p_c (within numerical errors) after performing the finite size scaling of Eq. (4). However, the CDF Φ_{SN} for the skew normal function is a better fit for $P(p, L)$ curves than the CDF for the normal distribution. Therefore, in the following only the results obtained from fitting to Eq. (5) are presented.

To summarize, by running a series of trials of various values of p across the transition regime near p_c^{eff} for a range of system sizes L , we can first evaluate $\Delta(L)$ and p_c^{eff} through the fitting to Eq. (5) and directly measure how they scale as a function of L . The next step is to use these scaling relations to identify the value of ν from Eq. (3) and then, based on Eq. (4), extrapolate to the infinite system to obtain the true percolation threshold p_c . The precise value of p_c identified from Eq. (4) can then be used to determine other critical exponents via scaling relations, particularly the critical exponent μ for conductivity $\sigma \propto (p - p_c)^\mu$ calculated from the random walk (de Gennes ant) method described above.

B. Simulation results

Using the methods described above, we conducted a series of simulations of randomly packed conducting-insulating spherocylinders, for six systems with total number of particles $N = 1728, 2744, 4096, 5832, 8000$, and 10648. In each system, the particle number is of the form $N = m^3$ where m is an integer ranging from 12 to 22, to allow for simple initialization in a cubic-shape simulation box with periodic boundary conditions. All

the spherocylinders were taken to be of the same size, with 0.16 units in diameter d and 1.04 units in length, corresponding to an aspect ratio of 6.5, same as that of $\text{CrO}_2/\text{Cr}_2\text{O}_3$ nanocomposites. A typical simulation started with a cubic box of edge length $2.5m$, to ensure sufficient spacing between the spherocylinders for the initial randomization steps. The positions and orientations of the particles were initially thermalized with 10^4 Hard-Particle Monte Carlo steps at a density < 0.01 . Then the MCM algorithm described above was applied to generate the final dense disordered state with the corresponding compressed system size L . For the example of $22^3 = 10648$ particles, the fully compressed system has an edge length of around 9 units, with $L/d = 56.54$. The list of contacting particles obtained during the steps of the MCM routines for overlap removal was utilized to identify connected clusters and percolation paths of the final dense packing state through the Hoshen-Kopelman algorithm [46] with off-lattice extension [47]. For a given system, at each fraction p of conducting particles, we performed a large number of replicate simulations, $\mathcal{R}$, with different initial random number seeds, to generate different configurations of dense random packing through MCM for each p to assure the results were independent. For our initial hypothesis exploration, the number of replicates was chosen in such a way that the expected relative statistical error $\sqrt{N}/N + \sqrt{\mathcal{R}}/\mathcal{R} < 0.1$. We then refined our data by adding approximately the same number of runs for each p , bringing the total statistical error close to 0.05. For example, for a system of $N = 22^3 = 10648$ particles, we generated 355 independent configurations via MCM to evaluate the system property at each p , while for $N = 12^3 = 1728$, we used 530 replicates for each p .

Figure 4(a) shows the plots of the spanning percolation probability P calculated over a range of p near the percolation threshold, for two different particle numbers, $N = 1728$ and $N = 10648$. A smaller N (corresponding to a smaller system size L) yields a broader probability distribution, with a larger width of percolation transition Δ , as expected. The quantitative values of Δ and the effective percolation threshold p_c^{eff} for various system sizes L were determined through the fits of the calculated probability data to Eq. (5), with results presented in Figs. 5 and 6, respectively.

Following the finite-size scaling procedure described above, we first determine the value of the correlation-length critical exponent ν by fitting the values of transition width Δ to Eq. (3), as shown in Fig. 5. It gives $\nu = 0.646 \pm 0.005$ which, in turn, is used to fit the values of p_c^{eff} plotted against $L^{-1/\nu}$ according to Eq. (4). The fitting result, presented in Fig. 6, is used to determine the extrapolated value of the percolation threshold $p_c = 0.312 \pm 0.002$ in the limit of infinitely large system of randomly packed spherocylinders. This value of p_c agrees well with the experimental finding of $p_c = 0.305 \pm 0.026$ reported in Sec. II B for $\text{CrO}_2/\text{Cr}_2\text{O}_3$ nanocomposites. We note that the value of correlation-length exponent

FIG. 4. Spanning percolation probability as a function of fraction p of the conducting spherocylinders, for (a) two sample systems with $N = 1728$ (open circles) and $N = 10648$ (filled squares) particles, and (b) an enlarged portion for all six systems of different N . Each set of simulation data (shown as symbols) is fitted to Eq. (5), with results shown as dashed curves. The vertical dashed line in both (a) and (b) indicates the location of $p_c = 0.312$.

ν ($= 0.646$) obtained here is smaller than the standard value of 0.876 in 3D, which could be attributed to the relatively large errors of width Δ evaluated in the fitting (see Fig. 5) and limited number of particles used in our simulations.

An alternative method to identify p_c can be used by noting that given a certain geometry of the constituent particles and a dimensionality of the system, the critical spanning probability at $p = p_c$ is a universal quantity [17]. Thus, for systems of different finite sizes the corresponding spanning probabilities $P(p, L)$ are expected to cross at $p = p_c$. This is consistent with our simulation

FIG. 5. Width Δ of the percolation transition as a function of system size L rescaled by the particle diameter d . The error bars are from the fitting of Eq. (5) to obtain Δ at each L . The dashed line is the power-law fit to Eq. (3), yielding a value of the critical exponent $\nu = 0.646 \pm 0.005$.

FIG. 6. Effective percolation threshold p_c^{eff} as a function of $(L/d)^{-1/\nu}$. The dashed line is the fit to Eq. (4), and its intersection with the y axis gives the percolation threshold $p_c = 0.312 \pm 0.002$ for the infinite system with $L \rightarrow \infty$.

results given in Fig. 4(b), which shows a narrow range of such crossing points located from $p = 0.307$ to 0.317 due to numerical variations, well agreeing with the result of $p_c = 0.312$ obtained above from finite size scaling.

Finally, we ran another series of simulations and applied the random walk method of de Gennes and described above to calculate the system conductivity σ for a narrow range of p above p_c . A large system size

FIG. 7. Rescaled conductivity, $\sigma(p)/\sigma(p=1)$, as a function of $p - p_c$ for systems of $N = 10648$ particles. The fitting to the scaling relation $\sigma \propto (p - p_c)^\mu$ (shown as the dashed line) gives the conductivity critical exponent $\mu = 1.62 \pm 0.04$.

with $N = 22^3 = 10648$ particles was used, with 350 independent configurations generated via MCM for each p . In each configuration 20 independent random walks of “blind ants” (with randomly chosen starting points) were conducted, and the outcomes were averaged over $350 \times 20 = 7000$ trials at each p to obtain the mean-square displacement $\langle r^2(t) \rangle$. The asymptotic regime of $t = 5 \times 10^5 - 10^6$ was used to calculate the system conductivity σ . The corresponding results of σ are presented in Fig. 7, where the conductivity data has been rescaled with respect to $\sigma(p=1)$, the conductivity of the system consisting of purely conducting particles that was evaluated at $N = 10648$. Using this data to fit into the scaling relation $\sigma \propto (p - p_c)^\mu$, we determined the critical exponent μ of the system conductivity, yielding $\mu = 1.62 \pm 0.04$.

This calculated value of the conductivity critical exponent is within the range of previous findings of $1.3 \leq t \leq 4.0$ in disordered composites [10–12], but much smaller than the value of $t = 2.52$ measured for this system experimentally. This discrepancy may be understood in light of analysis of Ref. [12], given that in the nanocomposite system studied here the electrical transport between any two adjacent spherocylinders is mainly governed by their interfacial resistance (due to the presence of surface oxide layers). Thus, the scaling of the system conductivity should be written as [12]

$$\sigma \propto (p_j - p_{jc})^\mu \propto (p^2 - p_c^2)^\mu = (p - p_c)^\mu (p + p_c)^\mu, \quad (6)$$

where p_j is the occupation probability of the conducting interjunction (proportional to the average contact number between conducting particles), and $p_j \propto p^2$ with p the fraction or concentration of conducting particles, as

confirmed in our numerical simulations. When p is close to p_c (as in our computation of σ shown in Fig. 7), from Eq. (6) the conductivity scaling behavior is dominated by $\sigma \propto (p - p_c)^\mu$, recovering the standard scaling relation for σ , with the value of $\mu = 1.62 \pm 0.04$ identified above. On the other hand, when p is far enough from the percolation threshold p_c , as occurred in our experimental measurement and data analysis (see Fig. 3), the range of $\mu < t \leq 2\mu$ for the conductivity exponent t , as measured for $\sigma \propto (p - p_c)^t$, is expected [12], leading to a lower bound of $\mu \geq \mu_l = t/2 = 1.26$ for the experimental result $t = 2.52 \pm 0.03$ given in Sec. II B. Our computed result of μ is then consistent with the experimentally measured value for the critical exponent, suggesting that our model correctly captures the essential electrical property of this percolating network of disordered spherocylinders.

IV. DISCUSSION AND CONCLUSIONS

We have investigated a binary composite system of randomly packed spherocylinders, to examine the relation between structural (percolation) and transport properties of the system. The composite consists of metal (CrO_2) - insulator (Cr_2O_3) nanoparticles that are of identical rodlike particle geometry but distinct functionality. Our experimental ($p_c = 0.305 \pm 0.026$, $t = 2.52 \pm 0.03$ with $\mu_l = 1.26$) and computational ($p_c = 0.312 \pm 0.002$, $\mu = 1.62 \pm 0.04$) results for both the percolation threshold and conductivity critical exponent are in good agreement. The small observed variations can be partially attributed to a different degree of disorder in experimental and theoretical arrangement of the spherocylinders. While in our simulations we have used a completely disordered system, the samples fabricated for the experimental measurements have a substantial degree of local nematic order which, in turn, may affect the threshold and the critical exponent values. The effects of polydispersity and particle irregularity, which are unavoidable in the experimental setup (see Fig. 1) but neglected in the simulations, may also account for the discrepancy between the experimental and computational results. In addition, the experimental results near the classical percolation threshold p_c may have been affected by the presence of tunneling percolation at lower values of p .

We note that our large-scale simulation result for the site percolation threshold of spherocylinders with an aspect ratio of 6.5, i.e., $p_c = 0.312 \pm 0.002$, is very close, within numerical errors, to the threshold found in Ref. [22] for jammed disordered spheres [$p_c = 0.3116(3)$] which, in turn, is almost identical to the threshold of the simple cubic lattice ($p_c = 0.311608$ [17, 19]). These three systems are geometrically quite distinct, with very different packing factors and different distribution of coordination numbers, although their average coordination numbers $\bar{Z}$ are close. The coordination number for the simple cubic lattice is exactly 6, the disordered jammed sphere packing has coordination numbers ranging from

4 to 12, with an average of 6 [22], while for the random close-packing of spherocylinders with a 6.5 aspect ratio studied here, a broader distribution of coordination numbers is obtained, ranging from 0 to 16 with an average of $\bar{Z} = 5.83 \pm 0.07$ (averaged over 200 simulations with 10648 particles each).

This value of $\bar{Z}$ is much lower than the isostatic value of $\bar{Z} = 2d_f = 10$ for spherocylindrical particles with $d_f = 5$ degrees of freedom per particle [49] at sufficiently large aspect ratios, indicating that the randomly packed systems examined here are not strictly jammed. It is likely due to the use of MCM, which has been known to produce states of lower $\bar{Z}$ for long rods with high aspect ratio [48] and the use of insufficiently small contact tolerance in our numerical simulations as compared to that generating random jammed packings of spheres [22, 50]. This results in a disordered packing state of spherocylinders that are not fully jammed, similar to the nanocomposite system studied here experimentally for which the strict jamming with higher $\bar{Z}$ is usually not accessible.

Although systems with the same average coordination number $\bar{Z}$ are likely to have similar values of p_c , such a close agreement is unexpected, given the different distribution of coordination numbers and noting that some other systems with the same average coordination number of 6 do not have such close values of p_c (see Table 1 of Ref. [22]). This result implies that not only the values of the threshold may be unaffected by the exact details of particle ordering, as in the case of ordered lattice vs

disordered packing of spheres with the same average coordination number, as has been pointed out in Ref. [22], but it may also be insensitive to the details of the particle geometric shape. While this may still be fortuitous, the coincidence seems less likely, given the independent research on three different systems, and with the new result presented here for the dense disordered state of spherocylinders that are geometrically distinct from spheres. If this result also holds for other systems, it may indicate a possible *universality* of the percolation threshold based on a more profound underlying mechanism which is presently unknown and needs further investigation.

These results are relevant for future device applications of functional nanoparticle composites, for which the ability to control the percolation threshold is critically important. They can also be of interest for a broader range of packing and percolation systems, such as drug release and the design of drug tablets [51], for which the percolation of soluble drug nanoparticles in the packed soluble/insoluble composite plays an important role [22].

ACKNOWLEDGMENTS

Z.-F.H. acknowledges support from the National Science Foundation under Grant No. DMR-1609625. The authors are grateful to Isaac Balberg, Robert Ziff, and Salvatore Torquato for illuminating discussions and helpful suggestions.

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