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Demand Side Management of an Urban Water Supply Using Wholesale Electricity Price

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Abstract

Municipal water supply consumes large quantities of electrical energy to move water from catchment areas to service reservoirs near centres of population. Pumping does not necessarily occur round the clock, but rather when necessary to uphold constraints relating to reservoir levels and system pressure. There is a degree of flexibility in the timing of pumping that makes it an excellent candidate for Demand Side Management, meaning that it can provide opportunities for improving power system operation and reducing electricity costs for the water utility. The extent of this flexibility depends on a number of factors. This study examines the optimisation of two water supply systems - the 'Van Zyl' benchmark system and a representation of the supply for the city of Belfast, Northern Ireland. The potential to employ intelligent operation of pumps to help bolster uptake of variable wind generation is assessed, as is quantification of the potential savings for a water utility. The results show significant potential savings for the water utility as well as a substantial increase in the utilisation of wind power.

Keywords: Demand Side Management, Real Time Pricing, Genetic Algorithms, Wind Energy, Renewable Energy, Optimisation, Water Pumping

1 Nomenclature

i	Time period ($i = 1, 2, \dots, 24$, 60 min/period)
m	Mourne supply
n	Lough Neagh supply
d	Inside pipe diameter (m)
h_f	Head loss (m)
C	Hazen-Williams pipe roughness coefficient
L	Pipe length (m)
Q	Volumetric flow rate (m^3/s)
E_i	Electricity cost, i^{th} period (£)
W_i	Wind generation as % of total in i^{th} period
$F_{p,i}$	Pump p flow rate, i^{th} period (l/s)
M_i	Energy cost per unit, i^{th} period (£/kWh)
$D_{p,i}$	Flow from service reservoir p , i^{th} period (l/s)
$P_{p,i}$	Pump p energy consumption, i^{th} period (kWh)
$R_{p,i}$	Service reservoir p water volume, i^{th} period (l)
$R_{p,max}$	Maximum water volume, service reservoir p (l)
$R_{p,min}$	Minimum water volume, service reservoir p (l)

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2 1. Introduction

The drive to phase out fossil-fired generation has increased investment in renewable generation. In North-west Europe, wind is an abundant renewable resource [1], and, as such, significant efforts have been made to increase the penetration of wind generation in power systems.

Ireland, although composed of two political jurisdictions (the Republic of Ireland and Northern Ireland), has one synchronised power system and Single Electricity Market (SEM). The Irish power system supports a relatively small population of 6.5 million people and has 750 MW of HVDC interconnection with Britain [2]. A target of 40% of all electricity is to come from renewable sources by 2020, predominantly from wind power [3]. This target causes some issues for the Irish system, some of which are unique due to its relative isolation and limited available interconnection.

Modern wind turbines, unlike traditional synchronous generators, do not provide inertia to the power system as their rotating masses are connected to the grid through power electronics. Significant power system inertia mitigates frequency transients during system faults

25 and large disturbances [4], and hence it is necessary to
26 maintain a minimum level of system inertia. Unlike
27 other countries with high penetrations of wind power
28 (such as Denmark), Ireland has only limited HVDC inter-
29 connection, which provides no inertial support. Be-
30 cause of this constraint, System Non-Synchronous Pen-
31 etration (SNSP) is currently limited to 55% on the Irish
32 power system [5], with any renewable generation above
33 this level wasted. Due to its variable nature, wind power
34 is non-dispatchable apart from curtailment by a system
35 operator.

36 In order to meet the high targets for wind power inte-
37 gration, it is estimated that the SNSP limit would have
38 to be raised to 70% to avoid excessive curtailment [2].
39 This will be a significant challenge, especially for con-
40 ventional generators [5], but presupposes that genera-
41 tion must be varied to meet a varying demand beyond
42 the operator's influence. Under this regime, the system
43 operator would have more problems when controlling
44 a power system with high penetrations of wind power
45 than one without. Dispatchable generation would see
46 much greater variation in output in order to address
47 wind variability, which is undesirable as it prevents gen-
48 erators operating at their most efficient settings.

49 Demand Side Management (DSM) provides a means
50 of mitigating the regulation duty of conventional gen-
51 eration. DSM has traditionally been seen as a method
52 whereby a system operator or utility would exert direct
53 control over load [6]. The main contribution of this
54 work is in investigating whether market-driven DSM
55 can provide improvements in wind power utilisation to
56 the power system without explicit system operator inter-
57 vention, but rather by the load responding to changes in
58 system price. This is the first study to optimise a water
59 network on the basis of Real-Time Pricing (RTP) and
60 quantify both the energy cost savings and wind power
61 utilisation.

62 2. Scope for Optimising Water Supply

63 2.1. Demand Side Management

64 With DSM, supply of managed load is encouraged
65 when net demand (consumer demand less renewable
66 generation) is low. The incentive is the lower cost of
67 electricity at such times. Conversely, the supply of man-
68 aged load is discouraged when net demand, and elec-
69 tricity price, are high. The boost to net demand when
70 renewable generation is plentiful eases the SNSP con-
71 straint.

72 DSM is regarded as an important part of the future
73 operation of power networks and as such has been the

74 focus of a number of studies. Where DSM has been
75 carried out based on energy cost, it has primarily been
76 on the basis of Time of Use (ToU) pricing [8][9][11].
77 These are multi-rate tariffs which change several times
78 a day. Although promoting energy use during off-peak
79 times, ToU tariffs do not track the actual market price
80 of electricity and thus do not provide an incentive
81 for consumers to respond to specific events, such as
82 generator outages or high-wind scenarios. ToU tariffs
83 reflect only the general trends of electricity cost and
84 usually have no more than four changes per day.
85 Increased penetrations of variable generation such as
86 wind generation mean that price peaks do not always
87 occur at the same time of day, as high penetrations of
88 low marginal cost generation during peak times reduce
89 the need for low merit generation, thus reducing market
90 prices. ToU tariffs do not reflect these day-to-day
91 variations. An RTP tariff, based on the wholesale cost
92 of electricity, offers a realistic means of tracking the
93 variation in system price.

94 RTP-based DSM has been implemented in [12]-[15]
95 with significant savings in energy cost. Finn *et al.* in
96 [14] optimised residential load on the basis of RTP and
97 saw increases in wind power utilisation of up to 23.3%,
98 while in [15], RTP-based optimisation of industrial
99 loads saw wind power utilisation increase by 5.8%
100 while also reducing energy cost.

101 A common theme is the aggregation of flexible
102 residential loads through the use of smart meters and a
103 central controller in order to minimise decision making
104 and maximise savings [7]-[9]. Such schemes have the
105 disadvantage of involving a large number of stake-
106 holders (residential consumers) who must voluntarily
107 submit to having their energy consumption controlled
108 externally. However, the potential has been shown
109 for significant savings in energy costs for consumers.
110 Vanthournout *et al.* in [10] found that it was difficult
111 to maintain involvement of residential consumers in
112 RTP schemes due to response fatigue - automation was
113 required in order to make it viable.

114 DSM has also been demonstrated as being viable for
115 provision of balancing reserve for wind generation [9].

116 Industrial loads frequently have a higher degree of
117 operational flexibility than residential loads [13],[15].
118 Industrial consumers represent 42% of global electrical
119 consumption. Industrial units are large compared
120 to residential or commercial loads and are centrally
121 controlled and owned, reducing the complexity of
122 co-ordination and thus making them very attractive for
123 DSM [16]. In [13], DSM of aggregated residential load
124 was compared with that of representative commercial
125 demand and a number of typical industrial processes. A

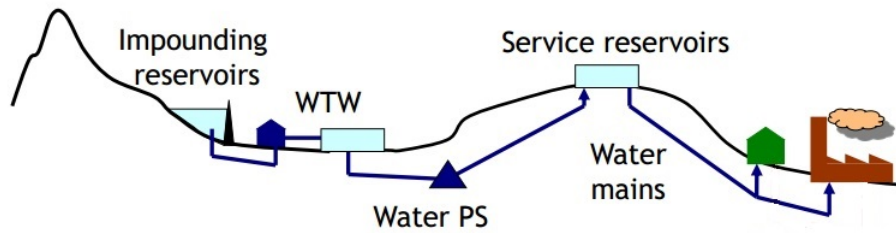


Figure 1: Layout of a water supply network

126 10% saving in energy costs was seen with the industrial
 127 DSM, compared to 5.8% for commercial and 5% for
 128 residential. Similarly high savings were also seen in
 129 [12].

164 A total of 23 impounding reservoirs supply more than
 165 370 supply reservoirs [17].

131 2.2. Public Water Supply

132 Public water supply is an excellent candidate for the
 133 application of DSM due its significant potential for
 134 a large number of operating modes. Water networks
 135 are centrally owned and controlled and would require
 136 minimal modification to allow optimised operation.

137 Water pumping can be classed broadly as an inter-
 138 ruptible load. In [16], a steel mill was optimised on
 139 the basis of several smart pricing scenarios. Under
 140 each pricing model, optimal scheduling resulted in
 141 higher profit, although higher profits were seen with
 142 ToU pricing compared to RTP - the steel mill which
 143 was modelled operated on a batch cycle, meaning
 144 that once a batch started it could not be interrupted
 145 - making it less suitable for taking advantage of the
 146 higher level of variability of RTP compared to ToU
 147 pricing. Water pumping can be interrupted, provided
 148 reservoir level constraints are maintained and wear
 149 from pump switching is considered. The basic layout
 150 of a water supply system can be seen in Fig. 1. Large,
 151 centrally controlled pumps are used to move water
 152 from catchment areas to service reservoirs (SRs) near
 153 centres of population, from which water flows to
 154 consumers. The hydrostatic head of these SRs is used
 155 to maintain system pressure and, as long as SR water
 156 levels are maintained between minimum and maximum
 157 levels, there is a high degree of flexibility over the
 158 timing of pumping. The electricity demand of Northern
 159 Ireland Water (NIW) accounts for approximately 3%
 160 of all electrical demand in Northern Ireland, a figure
 161 representative of water supply systems worldwide.

162 NIW oversees 26,700 km of water mains, supplying
 163 563 million litres of water per day to 1.8 million people.

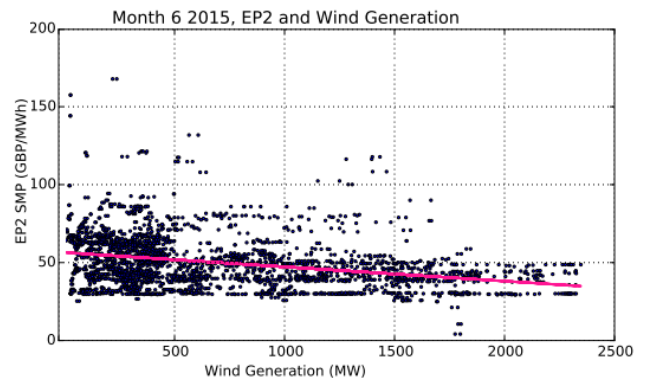


Figure 2: SMP and wind generation, June 2015

167 Many of NIW's facilities are run on ToU tariffs. NIW
 168 have carried out basic optimisation at some of their
 169 pumping stations in the past, trying to carry out as much
 170 pumping as possible during low-price periods.

171 In the SEM, System Marginal Price (SMP) changes
 172 every 30 minutes and reflects the operating cost of the
 173 single most expensive generator required to fulfill de-
 174 mand [20]. The higher the penetration of wind genera-
 175 tion on the power system, the lower the requirement for
 176 expensive generation. Since wind is considered to have
 177 no marginal cost, higher wind penetrations should result
 178 in a lower system cost. Fig. 2 shows the final SMP plot-
 179 ted against wind generation for one month in 2015. It is
 180 clear from this graph that there is some degree of cor-
 181 relation between wind and SMP: this can be explained
 182 by the current conservative operation of the power sys-
 183 tem. When wind penetrations are high, marginal gen-
 184 eration is not decommitted but rather dispatched down.
 185 This policy, though resulting in generators running at
 186 low efficiencies, gives the system operator a margin for

187 error with regard to wind forecasting uncertainty. At
188 very high wind penetrations such a policy would not be
189 justifiable.

190 SMP-based optimisation of load would nonetheless
191 help to flatten the demand curve, as it would promote
192 operation during low demand and low price scenarios
193 while discouraging consumption during peak periods.

194 There are several different ‘versions’ of SMP. The ac-
195 tual price paid to generators (termed as Ex Post 2 or
196 EP2) is not published by the SEM Operator (SEM-O)
197 until four days after the day in question (D+4). A full
198 day forecast (Ex-ante 1, EA1) is made available at 11:00
199 one day before actual trading. This is updated at 16:00
200 with the Ex-Ante 2 or EA2 forecast, and again at 9:30
201 on the day itself with the Within Day 1 (WD1) forecast
202 [21]. It is on the basis of these forecasts that pump-
203 ing optimisation is proposed in this work. Optimising
204 demand on the basis of the forecast wholesale price of
205 electricity could provide a means to increase the uptake
206 of wind generation by encouraging demand when wind
207 generation is high as well as minimising the price paid
208 by the consumer.

209 In [14], Finn *et al.* carried out a 6-month study on
210 a domestic dishwasher, optimising operation based on
211 EA1 and EP2 SMP. EP2 optimisation saw energy cost
212 decrease by more than 20% and wind power utilisation
213 increase by 23.5%, while EA1 optimisation saw
214 a 17.5% reduction in cost and wind power utilisation
215 increase by 16.9%. The inherent uncertainty of price
216 forecasting means that it would be almost impossible to
217 make the savings seen in the EP2 scenario. This study
218 found that scheduling load on the basis of the EA1 fore-
219 cast was a viable way to reduce energy costs and im-
220 prove wind power utilisation.

221 In [22], Paudyal *et al.* applied an industrial load man-
222 agement model to a simplified representation of a water
223 pumping facility, based on one day of data relating to
224 an RTP tariff in Ontario, Canada. A 38.1% decrease
225 in energy costs compared to non-optimised operation
226 was observed. This simulation, although short in du-
227 ration and disregarding hydraulic constraints, is notable
228 in that it considers the impact of water pumping opti-
229 misation on the power system, citing its implementation as
230 a means by which system operators could reduce peak
231 demand.

232 DSM of water networks is cost effective and tech-
233 nically feasible, and price based optimisation of water
234 networks has been carried out in the past [22]-[30].

235 3. Optimisation

236 Various methods have been proposed for pumping
237 optimisation, including linear programming [23],
238 non-linear programming [24] and dynamic program-
239 ming [25]. Heuristic methods, particularly Genetic
240 Algorithms (GAs), have been used successfully in a
241 number of studies, as they avoid the combinatorial
242 explosion inherent in other methods [27]-[30].

243 GAs are meta-heuristic algorithms which simulate
244 evolution and natural selection to select solutions in
245 a given generation based on a measure of fitness (the
246 *fitness function*). The algorithm initialises by randomly
247 creating a population of potential solutions. The fittest
248 solutions in each generation are bred with each other
249 (*crossover*) to create the next generation. An individual
250 solution’s chance of survival is proportional to its
251 fitness. Random mutation is employed in order to
252 diversify the population and reduce the likelihood of
253 convergence to a non-global optimum [31]. Mutation
254 and crossover are controlled by predefined probabili-
255 ties. There are a number of different ways of defining
256 how many individuals survive from one generation to
257 the next - elitism was used here to ensure that the fittest
258 individual in a given generation was carried forward to
259 the next.

261 4. Water Network modelling and specification

262 In this work, the pumping schedules of two water supply
263 systems were optimised - the ‘Van Zyl’ benchmark net-
264 work, first proposed in [27], and the high-level supply of
265 the city of Belfast, Northern Ireland. Optimisation was
266 carried out using the ‘pyevolve’ toolkit in Python, inte-
267 grated with the EPANET water network modelling soft-
268 ware [26]. Potential solutions were generated by a GA,
269 which were then evaluated for violation of hydraulic
270 constraints in EPANET before being passed back to the
271 GA to evaluate reservoir level and maximum daily flow
272 constraints. Feasible solutions were scored on the basis
273 of the optimisation objective (fitness function), depend-
274 ing on the scenario.

275 4.1. ‘Van Zyl’ benchmark system

276 The ‘Van Zyl’ test system was first used by Van
277 Zyl *et al.* in [27] and has been frequently used as a
278 benchmark system for testing optimisation algorithms
279 and investigating new operating procedures. It con-
280 sists of a reservoir supplying two tanks (at different
281 altitudes) via two primary pumps and one boost pump
282 (see Fig. 3, full system specification in [27]). Demand

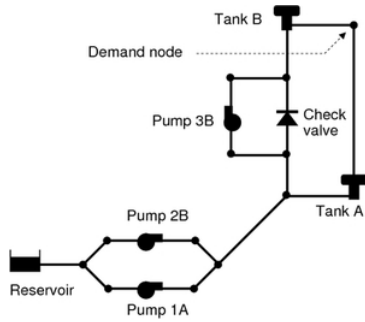


Figure 3: 'Van Zyl' test system

283 is taken from one node situated between both tanks.
 284 There are a large number of potential operating modes
 285 for this system, making it an excellent candidate for
 286 optimisation and testing of algorithms. Pump power
 287 varies slightly depending on the system pressure,
 288 but the primary pumps have an operating power of up
 289 to 200 kW while the boost pump consumes up to 50 kW.
 290

291 4.2. Belfast System

292 The largest component of NIW's supply network is
 293 that of the city of Belfast. A model of the Belfast wa-
 294 ter supply system was developed using data made avail-
 295 able by NIW. Belfast is a medium-sized city of approx-
 296 imately 500k inhabitants, who each consume 360 l/day
 297 of water on average [17]. Belfast's water supply system
 298 is representative of water supply systems on the island
 299 of Ireland, where the power system data from this study
 300 was taken.

301 The Belfast water network has a number of inter-
 302 esting characteristics. Most of the city's water supply
 303 comes from two catchments: the Mourne mountains to
 304 the South, and Lough Neagh to the Northwest (Fig. 4).
 305 The pumps at Dunore Point (part of the Lough Neagh
 306 supply) operate against a greater hydraulic head than
 307 those of the Mourne Conduit. Because of this, energy
 308 consumption of the Lough Neagh supply is higher than
 309 the Mourne supply. However, there is a limit of 130
 310 MI/day on abstraction from the Silent Valley reservoir in
 311 the Mournes, ensuring that both the Mourne and Lough
 312 Neagh supplies are always available to provide Belfast's
 313 water. Details of both sources can be seen in Table 1.

314 Data for the Belfast system were obtained from
 315 NIW's Asset Management division, as well as from
 316 Ordnance Survey maps and NIW press releases [18]-
 317 [19],[32]. Due to the difficulty with accessing specific
 318 data on system operation, a number of approximations
 319 were necessary. Service reservoir capacities were

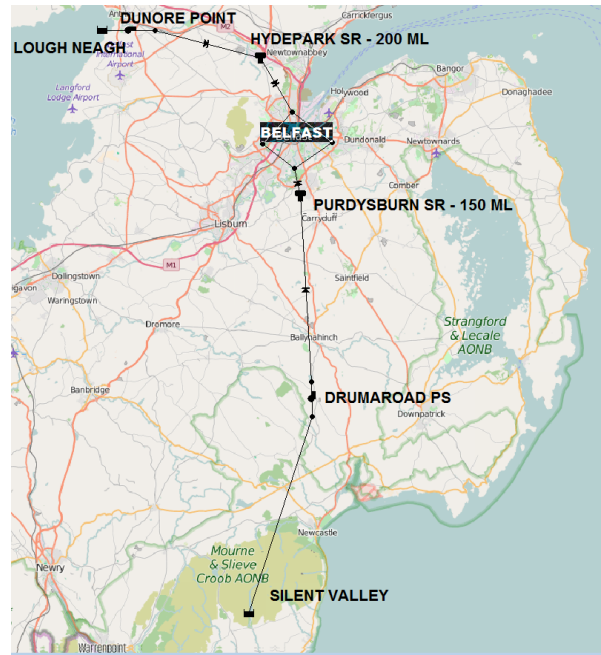


Figure 4: Simplified representation of Belfast water supply (EPANET)

Table 1: Belfast's main sources of water [18] [19]

	Mourne Conduit	Lough Neagh
Pipe length	56 km	18 km
Service reservoir capacity (approx. *)	150 MI	200 MI
Total head gain	-76 m	90 m
Max pumped flow	130 MI/day	180 MI/day
Pump power*	1.2 MW	3 MW

*Approximated from available data

320 inferred from satellite data, while pump power was
 321 calculated from pump flow rates and system head.
 322 Pumps were modelled as single-speed units. The water
 323 supply of Belfast is not isolated from the rest of the
 324 Northern Ireland network, and a small proportion of
 325 the water carried is diverted to other areas. In order
 326 to reduce the computational complexity of the model this
 327 off-take was ignored, and Belfast itself was represented
 328 as four equal demand nodes. Static head from the SRs
 329 was used to provide system pressure in the city.

331 4.3. Scenarios

332 For both models, four scenarios were considered:

- 333 • **Minimise consumption** - Minimising energy con-
 334 sumption and calculating cost on the basis of final
 335 EP2 price (base case).

- **EP2** - Minimising cost on the basis of the final EP2 price.
- **EA1** - Minimising cost on the basis of EA1 forecast price and calculating cost on the basis of final EP2 price.
- **Maximise wind** - Maximise wind power utilisation by aligning demand as much as possible with periods of high wind penetration.

4.4. Optimisation Method

Both systems were optimised on a daily basis in the period 1 April 2012 - 31 March 2015. Real data for EA1 and EP2 SMP were used as inputs, as were data for wind generation and penetration. Water demand profiles were taken from data supplied by NIW for previous work [33], and scaled according to the size of the system. A GA was used for the main optimisation, which integrated with the EPANET hydraulic solver to assess the viability of potential solutions. Candidate solutions were 72-bit binary strings in the case of the ‘Van Zyl’ model and 48-bit strings in the Belfast model, corresponding to the operation of each pump modelled hourly over a 24-hour period. Hydraulically infeasible solutions were penalised, and feasible solutions scored based on the objective function of the scenario modelled. A solution was produced for each day in the modelled period, with the outputs at the end of each day used as the initial conditions of the following day.

In the ‘Van Zyl’ model, 150 generations of GA were used, while 50 were used in the Belfast model. Both used a population of 200. The crossover rate was 100%, meaning all solutions were ‘interbred’. The mutation rate was 3%. These figures were arrived at through empirical evaluation. A flowchart of the methodology can be seen in Fig. 5.

4.5. Objective Function

For each scenario, the optimisation objective function was different. In the EA1 and EP2 scenarios, the objective was minimisation of cost (Eq. 1).

$$\text{minimise: } \sum_{i=1}^{24} E_i \quad (1)$$

In the ‘minimise consumption’ scenario, it was to minimise the overall quantity of energy consumed (Eq. 2).

$$\text{minimise: } \sum_{i=1}^{24} P_{p,i} \quad \forall p \quad (2)$$

The objective of the ‘max wind’ scenario was to maximise the quantity of wind energy consumed (Eq. 3).

$$\text{maximise: } \sum_{i=1}^{24} W_i \quad (3)$$

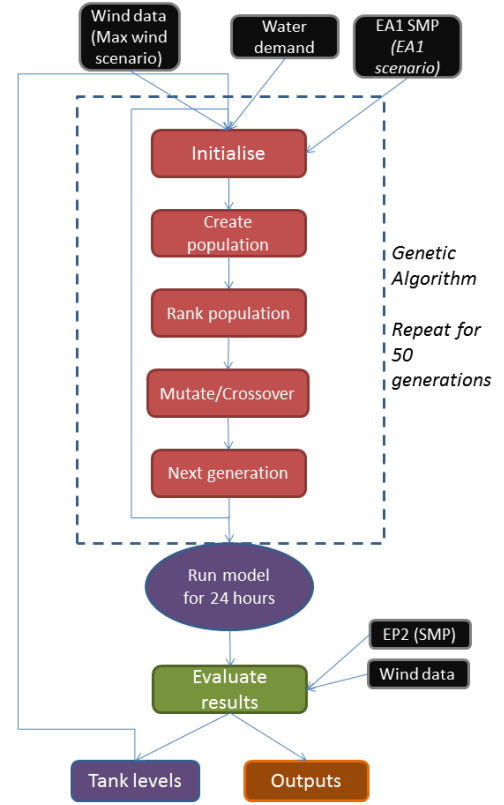


Figure 5: Genetic Algorithm and model methodology

4.6. Constraints

For both service reservoirs, the reservoir level at time period i was equal to the reservoir level at time period $i-1$ minus the outflow during $i-1$ plus the inflow during $i-1$.

$$R_{p,i} = R_{p,i-1} - D_{p,i-1} + F_{p,i-1} \quad \forall p \quad \forall i \quad (4)$$

The cost of electricity consumption during time period i was equal to the unit cost of electricity during i multiplied by the power consumption of the pumps during the same period.

$$E_i = M_i P_{p,i} \quad \forall p \quad \forall i \quad (5)$$

SR levels were allowed to vary between specified minimum and maximum levels (Eq. 6).

$$R_{p,min} \leq R_{p,i} \leq R_{p,max} \quad \forall p \quad \forall i \quad (6)$$

4.7. Belfast Model Constraints

There were two constraints implemented in the Belfast model that were not in the ‘Van Zyl’ model -

abstraction from Silent Valley Reservoir was limited to 130 MI per day, and a ‘mass balance’ constraint was enforced, requiring SR water levels to be at least 90% of initial level (on 1 April 2012) at the end of each day (see Eq. 7). The ‘mass balance’ constraint was necessary to prevent reservoirs having insufficient capacity for high-demand days.

$$\begin{aligned} \sum_{i=1}^{24} F_m &\leq 130 \times 10^6 \\ R_{p,i=24} &\geq 0.9R_{p,initial} \quad \forall p \end{aligned} \quad (7)$$

4.8. Hydraulic Modelling

The Hazen-Williams equation (Eq. 8), [34] is an empirical formula which models the pressure drop of water flowing in pipes. The EPANET solver uses this equation to calculate system pressure losses, allowing accurate calculation of F and D at each time step. Pipes were modelled as plastic-lined, with a roughness coefficient (C) of 130.

$$\frac{h_f}{L} = \frac{10.67Q^{1.85}}{C^{1.85}d^{4.87}} \quad (8)$$

5. Results

The algorithm output data for each day showing reservoir level variation, pump operation, flow rates, energy consumption and final solution feasibility (a feasible solution was found for all days with both models). Table 2 provides a summary of the salient data.

5.1. ‘Van Zyl’ Model

Despite serving the same demand, the scenarios modelled showed a significant variation in the total amount of water pumped. This is because pump 3B (see Fig. 3) acted as a top-up pump, transferring water from one SR to another. The ‘max wind’ scenario saw this pump used extensively, thus resulting in the higher energy consumption and pumped flow averages that can be seen in Table 2.

The ‘minimise consumption’ scenario consumed 2% less electricity than any other scenario while also maintaining the lowest average value of pumped flow. Despite this, it was the most expensive scenario, costing 13.4% more than the EP2-based optimisation (Fig. 6).

All scenarios showed an increase of wind power contribution compared to the system average (Fig. 7). Optimising on the basis of the wind penetration saw a large increase of wind contribution - 18.2% higher than what would be expected from the system average.

EA1 forecast price was consistently lower than the final EP2 price (underestimating final cost by 13.6%

on average) but was still cheaper than two of the three other scenarios. This optimisation also showed similar contributions from wind power to the EP2 case.

5.2. Belfast Model

All four scenarios of the Belfast model showed very similar values for total pumped flow, as would be expected from the radial nature of this network. Energy consumption and pumped flow do not correlate directly due to the different energy consumptions of both supplies, and the fact that the relationship between flow rate and power depend on the operating head of the system, which vary due to the level in the SRs. The ‘max wind’ scenario, which paid no heed to the cost or quantity of energy, gave the highest values for pumped flow and power consumption but also saw a 19.7% increase in wind contribution compared to the system average (Fig. 9) while also being 10.4% cheaper than the ‘minimise consumption’ scenario.

A similar pattern of operating cost was evident for the Belfast model as for the ‘Van Zyl’ model: EP2 optimisation was the cheapest, followed by EA1. The one exception to this was the ‘minimise consumption’ scenario - this actually produced higher power consumption than either the EA1 or EP2 optimisations. This is due to a cycle observed in the output data, caused by the 24-hour horizon of the optimisation - initially, both service reservoirs would be allowed to drain as much as possible in order to minimise pumping. As the optimisation started again for the following day, both reservoirs would be depleted and significant pumping would be required to maintain water supply. The Lough Neagh supply consumed approximately 2.5 times more energy for each litre of water pumped compared to the Mourne supply. In the price- and wind-based scenarios, more use was made of the cheaper Mourne supply, thus reducing the need for the more expensive Lough Neagh water. In the Belfast model, ‘max wind’, was cheaper than ‘minimise consumption’ (Fig. 8). This may have been due to the fact that the ‘Van Zyl’ ‘max wind’ scenario consumed significantly more power than the other scenarios (thus increasing energy cost) while the Belfast ‘max wind’ scenario consumed only slightly more.

EA1 optimisation underestimated the final EP2 cost by 13.8% on average but saw an increase in wind power contribution of 7.8%.

On average, across all scenarios, the Lough Neagh supply provided 51% more water than the Mourne supply, due to the constraint on abstraction from Silent Valley and the larger volume of the HydePark SR. 0.16 kWh were used by the Mourne supply pumps for each

Table 2: Summary of Results, April 2012 - March 2015

Daily Averages	Min. Cons.	EA1	EP2	Max. Wind
<i>'VAN ZYL' MODEL</i>				
Energy consumption (kWh)	3628	3705	3713	3885
Final (EP2) cost (£)	189.6	173.8	164.2	183.1
EP2 unit cost (p/kWh)	4.79	4.69	4.42	4.71
Pumped flow (m ³)	14885	15359	15613	16229
Cost per m ³ pumped (p)	1.274	1.131	1.052	1.128
Expected wind contribution (kWh) (18.65% system av. penetration)	676.6	690.8	692.4	724.4
Wind contribution (kWh)	689.8 (+1.95%)	732.7 (+6.06%)	745.9 (+ 7.73%)	856 (+18.17%)
<i>BELFAST MODEL</i>				
Energy consumption (kWh)	55250	55071	55045	55874
Final (EP2) cost (£)	2846	2425	2278	2550
EP2 unit cost (p/kWh)	5.15	4.40	4.14	4.56
Pumped flow (m ³)	180449	180873	180903	185957
Cost per m ³ pumped (p)	1.577	1.341	1.259	1.371
Expected wind contribution (kWh) (18.65% system av. penetration)	10303	10270	10265	10419
Wind contribution (kWh)	10473 (+1.65%)	11066 (+7.75%)	11352 (+ 10.60%)	12467 (+19.65%)

454 m³ of water supplied, while the Lough Neagh pumps
 455 consumed 0.4 kWh for each m³ pumped. This was con-
 456 sistent across all scenarios and is due to the fact that the
 457 Lough Neagh pumps had to pump against a head of 90
 458 m, while the Mourne pumps were moving water against
 459 a negative head (-76 m).

460 6. Discussion

461 In this research, two water supply systems (the 'Van
 462 Zyl' test system and a model representing the supply
 463 for the city of Belfast) were optimised on the basis
 464 of minimising electricity consumption, maximising
 465 wind power contribution, and minimising electricity
 466 cost (using both forecast and actual system price).
 467 Pumping costs and contribution from wind power
 468 were quantified, with the Belfast model giving results
 469 consistent with the benchmark system.

470 EP2 optimisation was consistently the least expen-
 471 sive, as might be expected as EP2 represents the final
 472 cost of wholesale electricity. It would not be possible
 473 to optimise on the basis of EP2 in reality as it is not known
 474 until four days after the event, but it represents the most
 475 cost-efficient operation possible. EA1 optimisation is
 476 achievable, as EA1 data are made available one day
 477 in advance. Despite underestimating final costs by

478 approximately 14%, EA1-based optimisation nonethe-
 479 less represented a significant saving compared to the
 480 non-price-based scenarios. A water utility optimising
 481 pumping on the basis of the publicly available SMP
 482 forecast could make significant savings compared to
 483 normal operation.

484 It should be noted that all prices discussed here are
 485 wholesale prices - they do not reflect the final price a
 486 customer would pay as SMP does not include the cost
 487 of distribution or transmission. It can be reasonably
 488 assumed that this added cost would be fairly constant
 489 [35] and would not affect the results seen here, other
 490 than to increase the cost of all scenarios by a compa-
 491 rable margin. A further limitation is that neither of the
 492 models analysed here included constraints relating to
 493 water treatment, which is either a continuous or batch
 494 process. Water is treated before being pumped to ser-
 495 vice reservoirs, with the treatment plant usually being
 496 on the same site as the pumping station (as is the case
 497 with both Dunore Point and Drumaroad). The Belfast
 498 model represents a simplification of the reality, in that
 499 the city itself was modelled as four demand nodes and
 500 offtake from both conduits for other areas were ignored;
 501 however, this should not have a significant effect on the
 502 results as the demand was scaled to compensate for the
 503 excess water that would have otherwise served areas
 504 beyond Belfast, and flow within the Belfast network

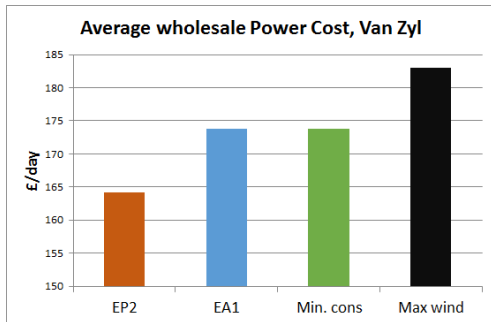


Figure 6: Average SMP energy cost, 'Van Zyl' model

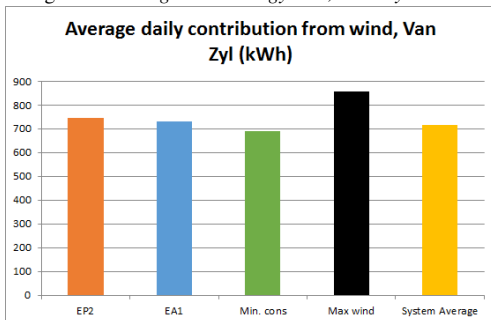


Figure 7: Average contribution of energy consumption from wind, 'Van Zyl' model

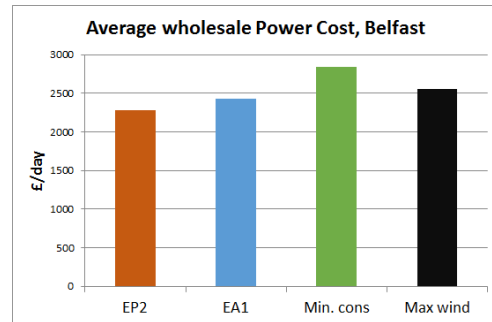


Figure 8: Average SMP energy cost, Belfast model

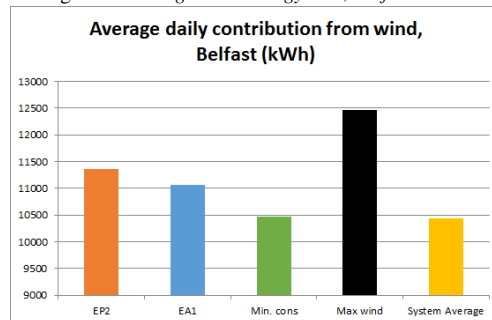


Figure 9: Average contribution of energy consumption from wind, Belfast model

505 itself would have little bearing on the demand from the 531
506 SRs. 532

507 For both models, the 'max wind' scenario showed 533
508 a significant cost saving compared to the 'minimise 534
509 consumption' scenario. Both SMP-based optimisa- 535
510 tions also showed significant increases in wind power 536
511 contribution compared to both the system average and 537
512 the 'minimise consumption' scenario. This reinforces 538
513 the suggestion that there is a correlation between wind 539
514 penetration and system price. While not as conducive 540
515 to high wind contributions as wind-based optimisation, 541
516 SMP-based optimisation represents a viable means 542
517 of incentivising demand to react to wind generation. 543
518 However, the difference in wind contribution between 544
519 the EA1 and EP2 scenarios shows that this link is 545
520 dependent on the accuracy of wind forecasting in the 546
521 operation of the electricity market. The very high 547
522 increases in wind contribution seen in the 'maximise 548
523 wind' scenario are also unlikely to be achievable in 549
524 reality as they are based on perfect foresight of wind 550
525 generation. 551

526 In the Irish SEM, the EA1 forecast is updated later 550
527 on D-1 with an EA2 forecast, and then again on the 551
528 morning of the day itself with the WD1 forecast. 552
529 In practice, an EA1-based pumping schedule could 553

530 be updated when these forecasts are released. The 531
532 increased accuracy of these forecasts should correlate 533
534 with costs and wind contributions closer to those seen 535
536 in the EP2 scenario. High-wind events are frequently 537
538 multi-day, and so if a period of sustained high wind was 539
540 forecast, relaxing the mass balance constraint of the 541
542 Belfast system could allow tanks to be filled during this 543
544 period of low cost generation, or allow the water level 545
546 to gradually deplete in anticipation of such an event. 547

540 7. Conclusion

541 The main contribution of this study is in showing that 542
543 price-based optimisation of water supply provides an 544
545 opportunity to benefit both the water utility (through re- 546
547 duced cost) and the power system (through increased 548
549 uptake of wind power). Providing that the consumer 550
551 is paying a tariff based on the wholesale cost of en- 552
553 ergy, optimising pump operation on the basis of an SMP 554
555 forecast would allow the water utility to make signifi- 556
557 cant cost savings compared to normal operation while 558
559 increasing utilisation of wind generation. In a mar- 559
560 ket such as the Irish SEM, where wind power is price- 560
561 taking rather than price-making, optimising on the ba- 561
562 sis of SMP effectively amounts to market-driven DSM 562

(rather than that which involves explicit operator control) which has the advantage of encouraging alignment of energy consumption with wind generation. Optimising on the basis of the wind penetration itself increases the contribution of wind generation even further, while still reducing the cost of electricity. Implementing this in reality would be a more explicit form of DSM, either by direct signal from the energy utility or by designing a tariff based entirely on wind generation rather than SMP.

Both approaches provide advantages for both consumer and system, but a trade-off is required between cost and wind power uptake. If the system operator wished to maximise wind generation to the fullest extent, more explicit DSM would be desirable, thus providing the benefit seen in the ‘max. wind’ scenario here. However, if flattening of the load curve was also a priority for the system then SMP-based optimisation would be advantageous in that it would discourage load during peak times (which, due to variable generation, do not always occur at the times reflected by standard multi-rate tariffs) while also, to a certain extent, promoting utilisation of wind power.

The methodology used here could be applied to any water supply system, with modifications to suit the needs of the particular system - for example, to take account of water treatment constraints, or daily or seasonal limits on water abstraction. The effectiveness of the method would in large part be dictated by the flow rate of the pumps and storage capacity of service reservoirs in relation to the water demand. It should also be noted that the approach detailed here could be applied to any dispatchable load. If implemented on a sufficient scale, it would reduce both the need for thermal generation and for wind power curtailment.

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