



**QUEEN'S  
UNIVERSITY  
BELFAST**

## **Experimental Investigation into a Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfields, Iraq**

Lin, X., Huang, X., You, F.-C., Xu, J., Xu, M.-B., Gao, J., & Huang, M. (2020). Experimental Investigation into a Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfields, Iraq. *ARABIAN JOURNAL FOR SCIENCE AND ENGINEERING*. <https://doi.org/10.1007/s13369-020-04911-x>

**Published in:**  
ARABIAN JOURNAL FOR SCIENCE AND ENGINEERING

**Document Version:**  
Peer reviewed version

**Queen's University Belfast - Research Portal:**  
[Link to publication record in Queen's University Belfast Research Portal](#)

### **Publisher rights**

Copyright King Fahd University of Petroleum & Minerals 2020.  
This work is made available online in accordance with the publisher's policies. Please refer to any applicable terms of use of the publisher.

### **General rights**

Copyright for the publications made accessible via the Queen's University Belfast Research Portal is retained by the author(s) and / or other copyright owners and it is a condition of accessing these publications that users recognise and abide by the legal requirements associated with these rights.

### **Take down policy**

The Research Portal is Queen's institutional repository that provides access to Queen's research output. Every effort has been made to ensure that content in the Research Portal does not infringe any person's rights, or applicable UK laws. If you discover content in the Research Portal that you believe breaches copyright or violates any law, please contact [openaccess@qub.ac.uk](mailto:openaccess@qub.ac.uk).

### **Open Access**

This research has been made openly available by Queen's academics and its Open Research team. We would love to hear how access to this research benefits you. – Share your feedback with us: <http://go.qub.ac.uk/oa-feedback>

# Arabian Journal for Science and Engineering

## Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq --Manuscript Draft--

<b>Manuscript Number:</b>	AJSE-D-20-01628R1	
<b>Full Title:</b>	Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq	
<b>Article Type:</b>	SCI / ENG - Research Article	
<b>Section/Category:</b>	ENG-Petroleum Engineering	
<b>Corresponding Author:</b>	Lin Xu, Ph.D Zhejiang Ocean University Zhoushan, Zhejiang CHINA	
<b>Corresponding Author Secondary Information:</b>		
<b>Corresponding Author's Institution:</b>	Zhejiang Ocean University	
<b>Corresponding Author's Secondary Institution:</b>		
<b>First Author:</b>	Lin Xu	
<b>First Author Secondary Information:</b>		
<b>Order of Authors:</b>	Lin Xu	
	Xin Huang	
	Fu-chang You	
	Jie Xu	
	Ming-biao Xu	
	Mei-lan Huang	
	Jun Gao	
<b>Order of Authors Secondary Information:</b>		
<b>Funding Information:</b>	Zhejiang Province Public Welfare Technology Application Research Project (LGG20E040002)	Dr. Lin Xu
	Educational Commission General Project of Zhejiang Province (Y201840431)	Dr. Lin Xu
	Bureau of Science and Technology of Zhoushan (2019C21006)	Dr. Lin Xu
<b>Abstract:</b>	<p>The supersaturated saline drilling fluid(SDF) with strong inhibition, as a novel alternative to anhydrite formation drilling, is crucial for the safe and economic drilling operation. In this work, a high performance supersaturated SDF was experimentally formulated in combination to the long anhydrite features of Missan Oilfields. A composite weighting approach involving liquid and solid materials was introduced to reinforce the inhibition of supersaturated SDF. A suite of laboratory tests was conducted to screen the essential viscosifiers and filtrate reducers, and optimize the formula of supersaturated SDF, by means of evaluating the basic rheological and filtration properties. The results showed that univalent salts NaCl, KCl, and HCOONa are utilized to formulate the multiple brine phase, and polymeric additives, VIS and S-FLO, are selected to improve rheological and filtration properties. The newly developed supersaturated SDF provides the excellent thermal stability, lubricity, as well as inhibition capability, which should be an instructive solution to minimize the hole problems in the anhydrite drilling.</p>	

**Response to Reviewers:**

Dear Reviewers:

We are truly grateful to your critical comments and thoughtful suggestions. Based on these comments and suggestions, we have made careful modifications on the original manuscript and, in particular, the section of “result and discussion” has been partially rewritten. Below you will find our point-by-point responses to the comments (or questions). In the paper, all the modified parts are marked in red.

Response to comment:

Reviewer #1

Comment 1:

Fig 1:

- Please explain in the caption what do the color codes mean? - Green, yellow, white boxes and the lines.
- Please put all abbreviations in the caption as well even though you have already mentioned them in the paper, e.g. SDF.
- Put space in before ( to be saline drilling fluid (SDF).
- AIM equals to purpose?
- No need all capital if it is not an abbreviation. - Start all word with capital (standardize them)

Response: According to this advice, Fig.1 has been re-presented, and the improper caption has been modified; the color code has been remarked and explained for better understanding; all abbreviations involved in the paper have been elucidated; space has been added;

Comment 2:

Fig 2: Please show the error bars. State in the caption the repeatability. Please put in the caption the full name of each chemicals (abbreviations).

Response: According to this advice, some experiments have been complemented, and error bars have been given in Fig. 2 to state the repeatability. The abbreviations of chemicals are the industrial codes, and they have been introduced in Table 1.

Comment 3:

Fig 3:

- Please show the error bars. State in the caption the repeatability.
- So, black and red refer to left? Put arrow - Write the word legend next to the curve (no need inside a box)
- Legend must use same color as the curve color

Response: According to these advices, Fig.3 has been reconstructed in the form of bar error. Some improper description has been eliminated. Some detailed information can be found in P14.

Comment 4:

I found many () or [] and you do not use space before ( or [. Please give a space.

Response: According to this advice, we checked the paper and the lost space has been added before all () or [].

Comment 5:

Please move all Tables 2-5 into a SUPPLEMENTARY INFORMATION (SI). Show in the paper as figures or bar charts; with known error bar and repeatability.

Response: According to this advice, Tables 2-5 have been provided as a supplementary information together with complementary experiments, and some key information such as rheological and filtrate data has been given in the form of bar chart. The detailed description can be found in the section “results and discussion” in P8-P15.

Comment 6:

Please consider more papers >7 from this journal itself. What is the suitability merit to get published here if there is no attachment of references to this journal itself?

Response: Arab. J. Sci. Eng. has involved limited papers on brine drilling fluid system. According to your advice, we have made an effort to cite 6 papers that are contacted with the present work from this journal.

Comment 7:

Please note that the presence of salts may break the polymer or viscosifier chain and results in a lower viscosity; and viscosity increases with increasing polymer concentrations due to the increasing intermolecular entanglement.

Response: According to this advice, we have provided simple description on relation of polymer concentration and intermolecular effect, and cited Hakiki's work.

Comment 8:

Please note that the viscosity of fluids is shear-rate dependent. Please declare not only

	<p>the unit mPa.s but also measured at what shear rate? (1/s)  Response: As for rheological property of drilling fluids, the viscosity is always tested with a 6-speed rotator apparatus, which can exhibit relation between viscosity and shear rate. To clarify this point, we have supplied the experimental process in P6.</p> <p>Comment 9:  Regarding comment #7 and #8 above, please cite and consider these papers in your references: - Hakiki, F, Maharsi, DA, Marhaendrajana, T. 2015. Surfactant-polymer coreflood simulation and uncertainty analysis derived from laboratory study. Journal of Engineering and Technological Sciences 47 (6), 706-725. DOI: <a href="http://dx.doi.org/10.5614%2Fj.eng.technol.sci.2015.47.6.9">http://dx.doi.org/10.5614%2Fj.eng.technol.sci.2015.47.6.9</a> - Hakiki et al. 2015. Is Epoxy-Based Polymer Suitable for Water Shut-Off Application? SPE-176457-MS. DOI: <a href="https://doi.org/10.2118/176457-M">https://doi.org/10.2118/176457-M</a></p> <p>Response: These two papers are instructive to our work, and we have cited them in the section of "screening of viscosifier".</p> <p>Comment 10:  Make sure all references are mentioned in the paper passage and also provide the DOI link (if any).  Response: all references have been mentioned, and the DOI link (if any) has been provided.</p> <p>Comment 11:  In the optimization process, please show in new figures the variables you played with.  Response: New figures linked with the optimization process were presented in "results and discussion".</p> <p>Comment 12:  So, which one is the best viscosifier, filtrate reducer, and VIS content? At what concentrations? Could you please create a 3D map optimization? Please give a case study with a given reservoir properties to handle with.  Response: The advice would be helpful to explicitly determine the optimized ingredient, but it will inevitably demand a large quantity of experiments. To meet the requirement on-site, a single-factor experiment is enough and moderate, which is also cost-effective in building appropriate formula. Using the single-factor method, we attained the optimized formula of saturated SDF: fresh water+ 0.25 wt.% Na<sub>2</sub>CO<sub>3</sub> + 0.10 wt.% NaOH + (30 wt.% NaCl + 6 wt.% KCl + 8 wt.% HCOONa) mixed-salt water+ 3.0 wt.% S-FLO + 0.2 wt.% VIS + barite (1.23 s.g.).  In addition, according to the advice, the title of paper has been modified as "Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq"</p> <p>Reviewer #2  Comment 1: The experimental part should be supplemented with a description of the experimental procedure used to analyze the dispersion of the drilling fluid, that is, measuring viscosity and fluid loss.  Response: According to this helpful advice, we have complemented experimental procedure.  Comment 2: The article also presents a wide range of different thickeners and filtrate reducing agents. The composition of all types of additives should be described or referred to.  Response: All types of additives are commercially used in petroleum industry, and we presented a description on additive composition in Table 1.</p>
<p><b>Suggested Reviewers:</b></p>	<p>Jihua Cai, Doctor  Professor, China University of Geosciences  caijh@cug.edu.cn  Research interests focus on oilfield chemistry, drilling fluid and technology</p> <p>Nianyin Li, Doctor  Associated Professor, Southwest Petroleum University  linianyin@swpu.edu.cn  Research interests are focused on oil &amp; gas exploration and oilfield chemistry</p> <p>Hanyi Zhong, Doctor  Associated Professor, China University of Petroleum Huadong  zhonghanyi@126.com  his research is focused on oilfield chemistry, design and development of downhole</p>

	working fluid
	Xijin Xing, Master Engineer, China National Offshore Oil Corp xingxj2@cnooc.com.cn His research is concentrated on drilling fluids, corrosion and anticorrosion
	Chao Ma, Doctor Professor, Yangtze University 500526@yangtzeu.edu.cn He is interested in oilfield chemistry and polymer chemistry.

[Click here to view linked References](#)

# Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid

## Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq

Lin Xu<sup>1</sup>, Xin Huang<sup>2</sup>, Fu-chang You<sup>3,4</sup>, Jie Xu<sup>5</sup>, Ming-biao Xu<sup>4,\*</sup>, Mei-lan Huang<sup>6</sup>

<sup>1</sup> College of Petrochemical and Energetic Engineering, Zhejiang Ocean University, Zhoushan 316022, China;

<sup>2</sup> College of Petroleum Engineering, China University of Petroleum(Beijing), Beijing 102249, China;

<sup>3</sup> Hubei Collaborative Innovation Center for Unconventional Oil and Gas, Yangtze University, Wuhan 430100, China;

<sup>4</sup> Jiahua Technology Co., Ltd, Jingzhou 434000, China;

<sup>5</sup> Institute of Exploration Techniques, Chinese Academy of Geological Sciences, Langfang, Hebei 065000, China;

<sup>6</sup> School of Chemistry and Chemical Engineering, Queen's University Belfast, Belfast BT95AG, United Kingdom;

---

\* Corresponding author. Fax: +86 716 8060863.

E-mail addresses: xuhu\_11@yeah.net (M.-B. Xu).

1 **ABSTRACT**

2  
3 The supersaturated saline drilling fluid(SDF) with strong inhibition, as a novel alternative to  
4 anhydrite formation drilling, is crucial for the safe and economic drilling operation. In this work, a  
5 high performance supersaturated SDF was experimentally formulated in terms of the long anhydrite  
6 features of Missan Oilfields. Composite weighting approach involving liquid and solid materials  
7 was introduced to reinforce the inhibition of supersaturated SDF. A suite of laboratory tests was  
8 conducted to screen the essential viscosifiers and filtrate reducers, and optimize the formula of  
9 supersaturated SDF, by means of evaluating the basic rheological and filtration properties. The  
10 results showed that univalent salts NaCl, KCl, and HCOONa are utilized to formulate the multiple  
11 brine phase, and polymeric additives, VIS and S-FLO, are selected to improve rheological and  
12 filtration properties. The newly developed supersaturated SDF provides the excellent thermal  
13 stability, lubricity, as well as inhibition capability, which should be an instructive solution to  
14 minimize the hole problems in the anhydrite drilling.  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34

35  
36 **Keywords:** Anhydrite formation, Supersaturated brine, Weighted drilling fluid, High performance  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

# 1. Introduction

Drilling through anhydrite formations is always challenging, due to the plastic deformation and cramping property of anhydrite, which can cause various drilling problems such as drilling fluid contamination, hole shrinkage, hole washout, hole collapse, and pipe sticking (Emmanuel et al. 2011; Wu et al. 2007). It has been established in the last decade that, drilling operation of anhydrite can be significantly improved by saltwater drilling fluids. Salts can dissolve in water necessitating the salinity of based fluid be kept near or at saturation to minimize wellbore enlargement (Dusseault et al. 2004; Akers et al. 2015; Jia et al. 2019). Therefore, the saline drilling fluid (SDF) play a crucial role in successful anhydrite drilling operations, which has also been one of the most widely used systems over the past decades.

SDFs are formulated with a brine as the liquid phase and selected polymers. The brine liquid phase may be composed of NaCl, KCl, NH<sub>4</sub>Cl, NaBr, KBr, HCOOK, HCOONa, CaCl<sub>2</sub>, and CaBr<sub>2</sub> as single or multiple brine solutions, with which the designated density can be attained from dissolved salts (Amer et al. 2016; Jin et al. 2012; Kemp 1990). Selected polymers are, in general, added to offer appropriate suspension and required rheological properties (Knox et al. 2002; Zhou et al. 2015; Salkla and Mahto 2018). Generally, the higher the density of clear saline, the stronger the inhibition of drilling fluids can possess. To balance the formation pressure, a weighted SDF system involving solid weight agents appears to be necessary. The weighted SDFs can not only prevent and eliminate the plastic deformation and cramping behavior of anhydrite, but also effectively reduce drilling problems.

In spite of numerous studies on strongly inhibited SDFs, previous achievements should be limited for the complicated anhydrite formation. That is, the weighted drilling fluid needs to be especially designed on the basis of the detailed downhole conditions, for the purpose of meeting individual drilling requirements (Wajheuddin et al. 2018). In addition to the necessary drilling fluid weight, the fluids type and specification need to be suitable to make sure no downhole problems happen while drilling the long anhydrite. Therefore, investigation on functional SDFs should be conducted, in combination to on the corresponding formation conditions and, in this case, the saline and additives should be selected in order to produce the multifunctional SDFs available in the target anhydrite.



1 As a part of our ongoing study on SDFs (Xie et al. 2020), a novel supersaturated SDF has been  
2 designed and developed by lots of laboratory experiments, in terms of the features of anhydrite  
3 formation in Missan Oilfield. In this work, the supersaturated saline was exclusively employed to  
4 reinforce the fluid inhibition. The composite weighting manner was firstly defined, and then a  
5 suitable of polymeric additives were selected. Next that, the relevant amounts of additives were  
6 optimized by evaluating the properties of rheology and filtration under the simulated downhole  
7 conditions. Finally, the inhibition and lubricity of SDF were examined. These conclusions not only  
8 are meaningful to enrich a family of SDF available in anhydrite formation, but also will provide  
9 important technical reference for design on high performance working fluids.

## 19 **2. Methodology**

### 21 **2.1 Design of Supersaturated SDF**

#### 23 2.1.1 Supersaturated SDF construction

25 Missan Oilfields was explored with a long section of anhydrite formation at about 2,000m. The  
26 downhole temperature is anticipated to be 100°C, and the high formation pressure is inspected. To  
27 avoid potential drilling problems encountered in anhydrite formation, a novel supersaturated SDF  
28 with a density of 2.3s.g is designed, in which mixed-salt water involving organic and inorganic salts  
29 is employed as the weighted liquid to enhance the inhibition.

31 Construction of supersaturated SDF is given in Figure 1. As described above, the density control  
32 of SDF is essential, and thus the composite weighting approach concerning liquid and solid  
33 materials has been investigated. Note that, the focus of composite weighting approach is on analysis  
34 of liquid weighting materials and, in this regards, univalent salts and the relevant ratio were  
35 discussed. In addition, the key additives (e.g., viscosifier and filtrate reducer) were taken into  
36 account, in order to facilitate the performance of supersaturated SDF. Two steps constitute the  
37 majority of developing the basic formula of supersaturated SDF. Moreover, a series of lab tests was  
38 conducted to explore the applied properties of supersaturated SDF. At the same time, optimization  
39 tests of additive concentration were conducted to improve rheological and filtration properties.  
40 Finally, thermal stability, inhibition and lubricity were evaluated for meeting requirements of  
41 anhydrite formation drilling.

**Fig. 1** Schematic of constructing the supersaturated saline drilling fluid (SDF). The key process of constructing the supersaturated SDF are marked in yellow.

### 2.1.2 Weighting approach

Composite weighting approach mentioned above was adopted in the supersaturated SDF. It is well documented that the soluble univalent salts can effectively raise the liquid density, with which interstitial hydration of clays and rock cramping deformation may be prevented (Lin et al. 2011; Yang et al. 2013). Herein, typical univalent salts such as NaCl, KCl, and HCOONa were introduced as liquid weighting materials. To obtain the supersaturated solution, the excess salts were added. Undoubtedly, these univalent salts can cooperatively increase the density of continuous phase of SDF, which should contribute largely to the inhibition. Given the anhydrate pressure, the solid weighting material was synchronizedly employed to raise the density of supersaturated SDF up to 2.3s.g., wherein the conventional barite powder was used as the weighting agent. Once the weighted liquid of supersaturated SDF was determined, functional additives were further screened and evaluated to determine the basic formula.

## 2.2 Materials and tests

### 2.2.1 Materials

Unless otherwise noted, functional additives were obtained from Jiahua Technology Co. Three typical kinds of viscosifiers, including cellulose series, polyacrylamide series, and biopolymer series, and three kinds of filtrate reducers such as sulphonated series, starch series, and celluloses series, were used as received. Some information on these commercial additives can be found in Table 1. Note that, these functional reagents were widely employed in constructing the high performance drilling fluids. Sodium chloride (NaCl), potassium chloride (KCl), and sodium formate (HCOONa) were purchased from Wuxi Jingke Fine Chemical Co.

Table 1 Information on additives applied here

additives	ingredients	industry code
liquid weighting materials	NaCl, KCl, HCOONa	
viscosifiers	cellulose	CMC and PAC
	polyacrylamide series	PLUS, PLH, and PHPA
	biopolymer	XC, VIS, MC-VIS, and XAN
filtrate reducers	sulphonated series	SMP-I, SMPC, SMP-II, TEMP, and TX
	starch series	CMS, HPS, B-LOSE, FLO, and S-FLO
	cellulose	MIL, CMC-LV, and PAC-LV

## 2.2.2 Tests of rheological and filtrate property

The SDF system under consideration was firstly aged at 100°C for 16h., and then quench cooled for rheology and filtration tests. Rheological data of SDF system were measured at six specific shear rates, i.e., 600, 300, 200, 100, 6, and 3 rpm using a Fann 35 viscometer. American petroleum Institute (API) filtration was conducted with a ZNS-2 pressure filtration apparatus.

## 2.3 Experimental process

### 2.3.1 Preparation of supersaturated SDF

Table 1 provides the components of supersaturated SDF, and the preliminary formula is: fresh water + 2.0wt.% filtrate reducer + 0.6wt.% viscosifier + mixed-salt water, which is based on the previous studies. Apparently, the supersaturated SDF mainly contains viscosifier, filtrate reducers, the pH adjusting agent, the hardness control agent other than weighting materials, through which the comprehensive performance can be attained.

### 2.3.2 Screening of key additives

Viscosifier and filtrate reducers are always fundamental to develop high performance drilling fluids. Hence several typical kinds of additives were screened in terms of property of rheology and filtration within the simulated downhole environments. It should be pointed out that the rheology and filtration parameters, e.g., apparent viscosity (AV), plastic viscosity (PV), yield point (YP), and standard fluid loss ( $FL_{API}$ ) before and after aging process, were comparatively investigated here, in order to determine the basic formula of supersaturated SDF.

### 2.3.3 Optimization of supersaturated SDF

As for the supersaturated SDF preliminarily obtained, rheology and filtration properties were further optimized by a set of single-factor experiments. During the optimization process, dosages of key additives were varied in a certain range to determine an appropriate formula. In addition, test of thermal stability was conducted on the optimized system and the temperature changed in the range of 90 ~120°C. Meanwhile, the properties of inhibition and lubricity were examined for the potential application on-site.

## 3.Results and discussion

### 3.1Construction of supersaturated SDF

#### 3.1.1 Analysis on weighting materials

1 Previous studies have validated the application of solid-liquid composite weighting fluid in  
2 enhancing inhibition and density of drilling fluids (Wang et al. 2009; Jiang et al. 2014; Li et al.  
3 2011). The weighting capability of supersaturated solution can be further reinforced by mixing  
4 inorganic and organic salts. Herein, univalent salts, NaCl, KCl, and HCOONa, are typically utilized  
5 to construct the supersaturated state. In the investigated univalent salts, NaCl is the main  
6 composition of the saturated solution, and KCl and HCOONa are further introduced to improve the  
7 inhibition. The compositions of basic saline are given as: fresh water + 30wt.% NaCl + 6wt.% KCl  
8 + 8wt.% HCOONa, and the density of supersaturated solution can be controlled at 1.23 s.g.  
9

10 Undoubtedly, such supersaturated solution involving composite salts can not only work as the  
11 basic continuous phase for drilling fluids, but also reinforce the weighting and inhibition properties.  
12 Moreover, the solid weighting material, i.e., barite, is introduced to raise the density of drilling fluid  
13 to 2.3 s.g. As a result of composite weighting, the cramp of anhydrite upon drilling can be prevented  
14 or even eliminated, and wellbore stability of the anhydrate formation can be obtained.  
15

### 16 3.1.2 Screening of viscosifiers

17 Viscosifiers are fundamental to modify rheology of multifunctional drilling fluids. To ascertain  
18 a suitable viscosifier, we investigated three representative kinds of viscosifiers consisting of  
19 cellulose(CMC and PAC), polyacrylamide (PLUS, PLH, and PHPA), and biopolymer(XC, VIS,  
20 MC-VIS, and XAN), and comparatively analyzed the rheological and filtration property of  
21 supersaturated SDF formulated here. Note that, the formula of supersaturated SDF was: fresh water  
22 + 0.6wt.% viscosifier + (30wt.% NaCl + 6wt.% KCl + 8wt.% HCOONa) mixed-salt water.  
23  
24  
25  
26

27 **Fig. 2** Comparison of rheological property for the SDFs formulated with different viscosifiers. Three typical  
28 kinds of viscosifiers were investigated and means of some characteristic parameters (A) AV, (B) PV, (C)  
29 YP, and (D) 6 rpm readings ( $\Phi_6$ ) were presented. Data are shown as mean  $\pm$  s. e. m. (n = 3,  
30 replicates).  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43

44 Fig. 2 presents typical rheological and filtrate data of the investigated SDF, including AV, PV,  
45 YP, and 6 rpm readings ( $\Phi_6$ ). Based on performance requirements of drilling fluid, AV and PV are  
46 crucial to the cycling property, while YP and  $\Phi_6$  contribute largely to the capability of carrying  
47 cutting upon drilling. It is clear in Fig. 2 that after an aging treatment, all of the rheological data  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

1 decreased, meaning that the aging process can influence chemical functional groups of polymeric  
2 additives and rheological property of fluid (Yang et al. 2019). For example, AV and PV of the SDFs  
3 with polyacrylamide and cellulose series were tested to decrease by about 50% after aging. In  
4 contrast with polyacrylamide and cellulose series, biopolymers exhibited a better aging-resistant  
5 property, as can be seen in Fig. 2. The rheological data of the SDFs with biopolymers exhibited a  
6 slight decrease after aging. In particular, the low shear rate reading (i.e.,  $\Phi_6$ ) can be detected (see  
7 Fig. 1D), while  $\Phi_6$  of other specimen were tested to be 0. The fact indicated that biopolymer series  
8 should possess more excellent salt-resistant capacity relative to polyacrylamide and cellulose series.  
9 Such salt-resistant capacity should be attributed to special steric configuration of biopolymers.  
10 There are lots of side groups in the biopolymers, which will prevent dehydration and sediment of  
11 polymers in brine. As a result, the thickening property of biopolymers can be maintained for the  
12 designed SDFs. Meanwhile, one can find that in the biopolymers studied here, VIS exhibited the  
13 most prominent rheological modification, and can meet both rheology and cutting carrying  
14 requirements. Therefore, VIS was selected as the viscosifier for further construction of the  
15 supersaturated SDF.

### 31 3.1.3 Screening of filtrate reducers

32  
33 Filtrate reducer is another kind of additives to drilling fluids, which is of much importance in  
34 improving the filtration property. To determine a moderate filtrate reducer, similarly, three kinds  
35 of filtrate reducers involving sulphonated specimen (SMP-I, SMPC, SMP-II, TEMP, and TX),  
36 starch specimen (CMS, HPS, B-LOSE, FLO and S-FLO), and celluloses specimen (MIL, CMC-  
37 LV and PAC-LV) that are usually employed in construction of drilling fluid, were systematically  
38 investigated, by means of evaluating their effect on rheological and filtrate performance. The testing  
39 results are presented in Fig. 3. Note that, the formula of supersaturated SDF is given as follows:  
40 fresh water + 2.0 wt.% filtrate reducer + 0.6 wt.% VIS + (30 wt.% NaCl + 6 wt.% KCl + 8 wt.%  
41 HCOONa) mixed-salt water, wherein the selected viscosifier, VIS, are used here.

52  
53  
54 **Fig. 3** Comparison of rheological and filtrate property for the SDFs formulated with different filtrate  
55 reducers. Three kinds of filtrate reducers were investigated and means of some characteristic parameters (A)  
56 AV, (B) PV, (C) YP, (D) 6 rpm readings ( $\Phi_6$ ), and (E)  $FL_{API}$  were presented. Data are shown as  
57 mean  $\pm$  s. e. m. (n = 3, replicates).

1 In Fig. 3, all of the rheological data have a minor increase with an incursion of filtrate  
2 reducers, and thus this finding reveals that filtrate reducers can vary the rheology of the SDF to  
3 some degree. Given the long-chain configuration of filtrate reducers, not surprisingly, the fluid  
4 viscosity can increase, due to adsorption effect of end chains (Elkatatny 2019). In principle, the  
5 additives are expected with unique function, which would be useful for the facile control of fluid  
6 property. Accordingly, it is necessary to select the filtrate reducers with weak thickening character.  
7 In the considered filtrate reducers, S-FLO and sulphonated series displayed weaker thickening  
8 effect, and appeared to be more appropriate than others. Meanwhile, S-FLO and sulphonated series  
9 can effectively maintain  $\Phi_6$ , which enable strong suspension capability of fluid. Moreover, a  
10 comparison of  $FL_{API}$  showed that S-FLO should be more suitable than sulphonated series, due to a  
11 lower  $FL_{API}$ . Based on weak thickening property and stronger capability of depressing filter loss,  
12 S-FLO was selected as a proper filtrate reducer for the construction of supersaturated SDF.  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24

## 25 **3.2 Optimization of supersaturated SDF**

### 26 **3.2.1 Viscosifier concentration**

27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

VIS concentration was further optimized for future field application. Similar to tests of additive selection, the rheological and filtrate properties were pursued upon optimization. The testing results are shown in Fig. 4. Note that, the formula of supersaturated SDF is given as: fresh water + 0.25 wt.%  $Na_2CO_3$  + 0.10 wt.% NaOH + (30 wt.% NaCl + 6 wt.% KCl + 8 wt.% HCOONa) mixed-salt water + (0 ~ 0.4 wt.%) VIS + 2.0 wt.% S-FLO + barite, wherein the fluid density was increased to 1.23 s.g. in terms of in-field requirement.

Fig. 4 presents AV, PV, YP,  $\Phi_6$ , and  $FL_{API}$  of the supersaturated SDF while varying VIS concentration in the range of 0 ~ 0.4wt.%. According to data variation shown in Fig. 2, one can notice two trends that (1) rheological parameters became much larger, and (2) filtrate losses decreased with an increment of the VIS concentration. In Fig. 4A, fluid viscosity displayed a dramatic increase with the VIS concentration. For example, the increasing magnitude of  $AV_t$  and  $PV_t$  are as high as 138% and 35%, respectively, while varying the concentration from 0 to 0.4 wt.%. This result is well consistent with previous studies performed by Hakiki et al. (Hakiki et al. 2015). An increase of the concentration of polymer additive will inevitably lead to the increasing intermolecular entanglement. As a result, influence of brine on the polymer chain and fluid viscosity

1 can be retarded by effect of concentration compensation. Considering the pumping capacity on-  
2 site, on one hand,  $AV_t$  should be less than 60 mPa·s and, thus, the addition of VIS are recommended  
3 to be 0.2 wt.%. On the other hand, while the VIS concentration is of 0.2 wt.%, the mean values of  
4 PV and  $\Phi_6$  are 9 Pa and 2.8 (see Fig. 4B and 4C), respectively, indicating that the cutting suspension  
5 capability can be obtained for the designed fluid. In Fig. 4D, one can observe that the decrease of  
6 filtrate loss focuses on the concentration range of 0 ~ 0.2 wt.%, reflecting a limited impact on filtrate  
7 loss by increasing the VIS concentration. Hence the VIS concentration is proposed to be 0.2 wt.%,  
8 in combination with rheological and filtrate loss analyses.  
9

10  
11  
12  
13  
14  
15  
16  
17  
18 **Fig. 4** Effect of viscosifier (VIS) concentration on rheological and filtrate property of the supersaturated  
19 SDF: (A) viscosity ( $AV$  and  $PV$ ), (B)  $YP$ , (C) 6 rpm readings ( $\Phi_6$ ), (D)  $FL_{API}$ . Data are shown as  
20 mean  $\pm$  s. e. m. ( $n = 3$ , replicates). The subscript “0” and “t” separately correspond to the tested  
21 system without and with aging treatment.  
22  
23

### 24 3.2.2 Filtrate reducer concentration

25  
26 Influence of S-FLO concentration on rheological and filtrate loss property was also investigated.  
27 It will be instructive to help improve the formula of supersaturated SDF. According to the results  
28 achieved above, the relative formula was given as: fresh water + 0.25 wt.%  $Na_2CO_3$  + 0.1 wt.%  
29  $NaOH$  + (30 wt.%  $NaCl$  + 6 wt.%  $KCl$  + 8 wt.%  $HCOONa$ ) mixed-salt water + (1.5~3.0 wt.%) S-  
30 FLO + 0.2 wt.% VIS + barite, wherein S-FLO concentration varied in the range of 1.5~3.0 wt.%,  
31 and the fluid density was increased to 1.23 s.g. in terms of in-field requirement.  
32  
33  
34  
35  
36  
37  
38  
39  
40

41 **Fig. 5** Effect of filtrate reducer (S-FLO) concentration on rheological and filtrate property of the  
42 supersaturated SDF: (A) viscosity ( $AV$  and  $PV$ ), (B)  $YP$ , (C) 6 rpm readings ( $\Phi_6$ ), (D)  $FL_{API}$ . Data  
43 are shown as mean  $\pm$  s. e. m. ( $n = 3$ , replicates). The subscript “0” and “t” separately correspond to  
44 the tested system without and with aging treatment.  
45  
46  
47  
48

49  $AV$ ,  $PV$ ,  $YP$ ,  $\Phi_6$ , and  $FL_{API}$  of the supersaturated SDF were given in Fig. 5. As might be  
50 anticipated, all of the rheological data increase with increasing S-FLO concentration. Besides, the  
51 magnitudes of data variation in the aged specimen are remarkably higher than those in the initial  
52 specimen. In the S-FLO concentration range investigated here, for example, the variation  
53 magnitudes of  $AV_0$  and  $AV_t$  were 17% and 8% (see Fig. 5A), respectively. Obviously, the aged  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

1 temperature plays an important role in determining stability of supersaturated SDF. In Fig. 5D,  
2 FL<sub>API</sub> reduced with an increment of S-FLO concentration, which can be mainly attributed to the  
3 stronger intermolecular entanglement. It is worthwhile to remark that while the S-FLO  
4 concentration is of 3 wt.%, FL<sub>API</sub> was tested to be less than 7.5 ml, meeting the industrial  
5 requirement. Meanwhile, one can facilely find that for the constructed SDF with 3 wt.% S-FLO,  
6 moderate YP and  $\Phi_6$  that are related with suspension capability of fluid can be obtained. In views  
7 of results obtained above, the S-FLO concentration is recommended to be 3.0 wt.%. Therefore, the  
8 optimized formula of supersaturated SDF is: fresh water+ 0.25 wt.% Na<sub>2</sub>CO<sub>3</sub> + 0.10 wt.% NaOH  
9 + (30 wt.% NaCl + 6 wt.% KCl + 8 wt.% HCOONa) mixed-salt water+ 3.0 wt.% S-FLO + 0.2 wt.%  
10 VIS + barite (1.23 s.g.).

### 21 3.3 General applied properties

#### 22 3.3.1 Analysis on thermal stability

23 To meet the drilling operation on-site, thermal stability of the formulated supersaturated SDF  
24 was evaluated in the range of 90~120°C. Herein, only the relationships between rheological and  
25 filtrate data and temperature of the aged specimen are given in Fig. 6.

26 **Fig. 6** Effect of temperature on rheological and filtrate property of the supersaturated SDF: (A)  
27 viscosity (AV and PV), (B) YP, (C) 6 rpm readings ( $\Phi_6$ ), (D) FL<sub>API</sub>. Data are shown as mean  $\pm$  s.  
28 e. m. (n = 3, replicates).

29 As follows from the data present in Fig. 6, the rheological parameters will decline with the  
30 elevated temperature, but reverse tendency can be observed for the filtrate parameters. For example,  
31 as the temperature varied from 90°C to 120°C, AV, PV, YP, and  $\Phi_6$  reduced by 10%, 10%, 12%  
32 and 36%, respectively, while FL<sub>API</sub> increased by 10%. The property changes can be partially  
33 ascribed to thermal degradation of polymeric additives (Sreekumar 2014), which can make property  
34 of drilling fluid bad. Although a certain variation happened, these characteristic parameters were  
35 still at an acceptable level, implying that the supersaturated SDF constructed here has proper  
36 thermal stability in the investigated temperature range.

#### 37 3.3.2 Analyses on inhibition and lubricity

38 It is generally known that for the drilling fluids, the inhibition and lubricity is significant for  
39 safe and economic drilling. Note that, the inhibition is closely related with wellbore stability, and  
40



1 the lubricity contributes largely for reducing torque and friction. Consequently, two properties of  
2 supersaturated SDF were examined.  
3

4 As for the supersaturated SDF, the recovery rate of solid phase arrives up to 93.35%, indicating  
5 excellent property of cuttings dispersion and cuttings hydration prevention. Additionally, the  
6 friction coefficient of supersaturated SDF is of 0.17, which is less than that of the common water-  
7 based muds, suggesting better lubricity relative to the general water-based muds. In view of these  
8 conclusions achieved, it can be concluded that the supersaturated SDF is developed with excellent  
9 performance, which would be a novel alternative to anhydrite formation drilling.  
10

#### 11 **4. Conclusions**

12 Drilling through anhydrate formations is generally challenging due to wellbore stability problems.  
13 In the present work, a novel supersaturated saline drilling fluid that can be used to drill anhydrates  
14 has been designed and developed, in combination with characteristics of the long anhydrate in  
15 Missan Oilfields. The liquid-solid composite weighting manner was utilized, and supersaturated  
16 saline containing three kinds of univalent salts was employed to reinforce the inhibition of drilling  
17 fluid. The filtrate reducer and viscosifier were experimentally selected, and the relative  
18 concentrations were also optimized by evaluation on rheology and filtration loss. The inhibition  
19 and lubricity of supersaturated saline drilling fluid were measured. The formulated supersaturated  
20 saline drilling fluid exhibits excellent rheology, filtration property, as well as excellent inhibition  
21 and lubricity properties, which would be a novel alternative to anhydrate formation drilling. These  
22 conclusions can not only facilitate improvement of supersaturated saline drilling fluid, but also  
23 extend a new family of drilling fluids available in anhydrate formations.  
24

#### 25 **Acknowledgements**

26 The authors thank the Welfare Technology Research Project of Zhejiang Province (No.  
27 LGG20E040002), Educational Commission General Project of Zhejiang Province(No.  
28 Y201840431), and Zhoushan Science and Technology Plan Project(2019C21006) for financial  
29 support.  
30

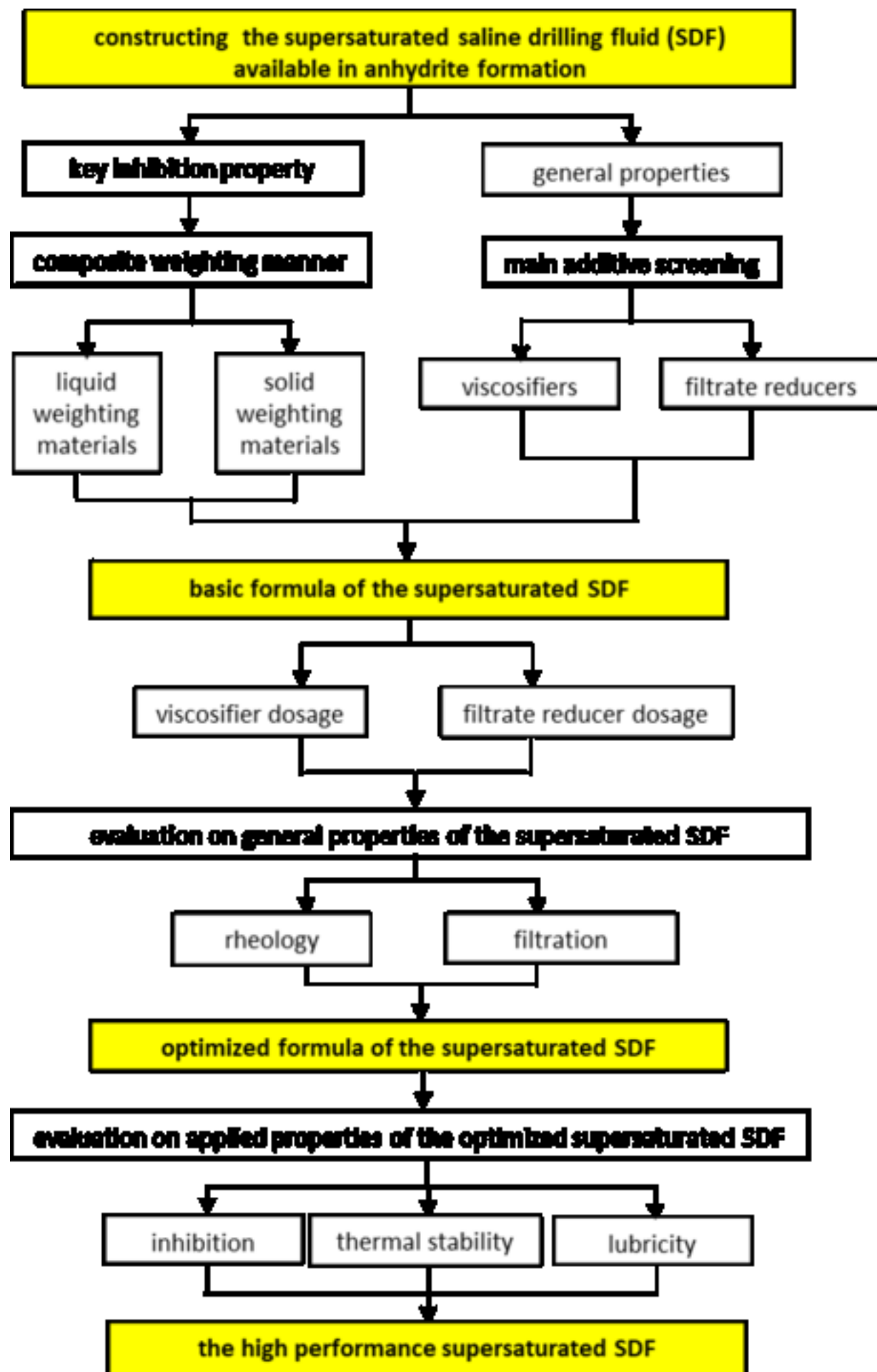
#### 31 **References**

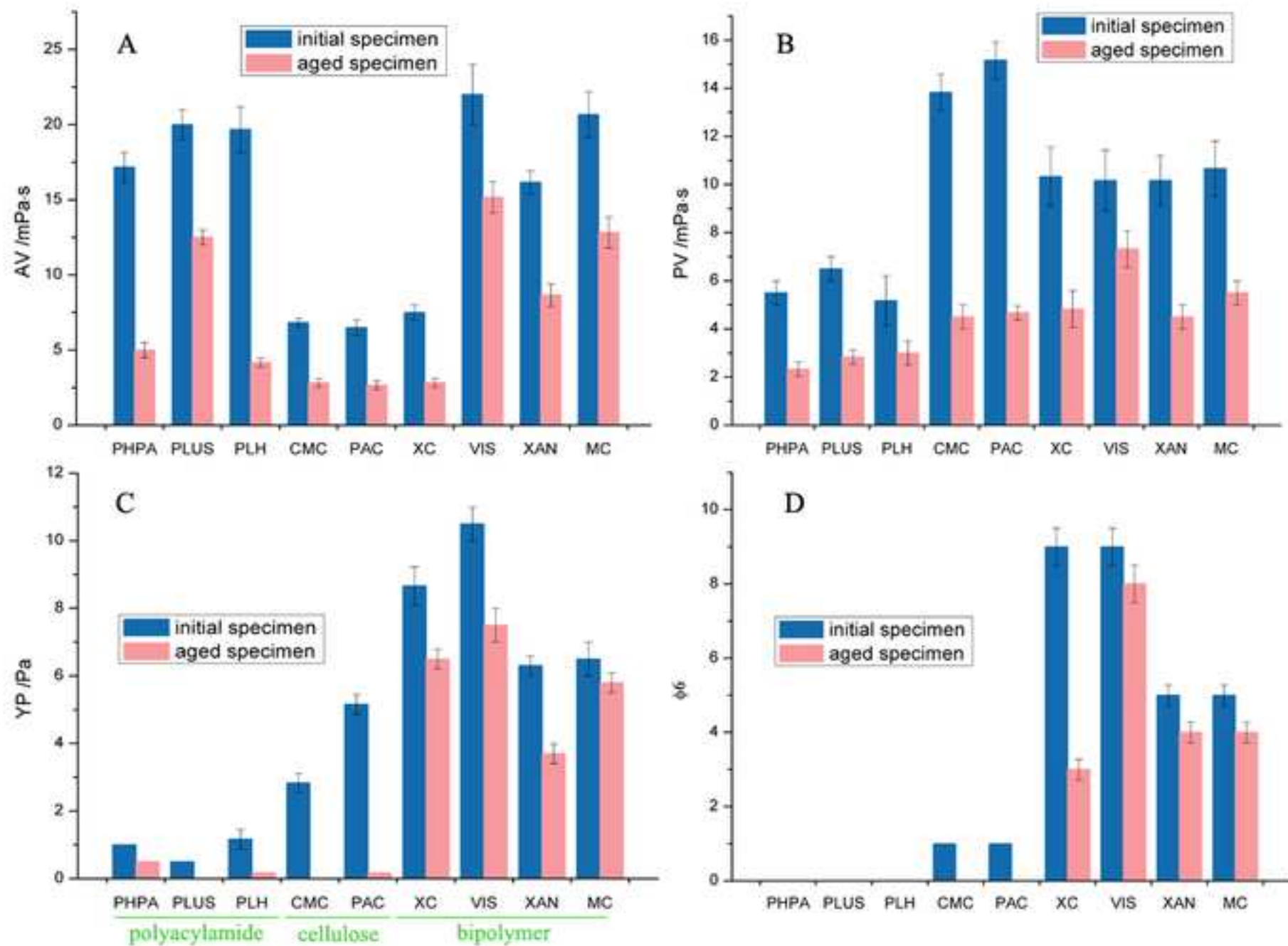
- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65
- [1] Omojuwa, E.O.; Osisanya, S.O.; Ahmed, R.: Properties of salt formations essential for modeling instabilities while drilling. In: SPE Nigeria Annual International Conference and Exhibition, Society of petroleum engineers (2011). <https://doi.org/10.2118/150801-MS>
- [2] Wu, H.; Zhang, K.M.; He, S.G.: Drilling fluid for salt-gypsum beds in deep wells in Tahe Oilfield. *TUHA Oil & Gas*. 12(2), 169-174 (2007)
- [3] Dusseault, M.B.; Maury, V.; Sanfilippo, F.; Santarelli, F.J.: Drilling through salt: constitutive behavior and drilling strategies. In: ARMA-04-608 presented at 6th North America Rock Mechanics Symposium, Houston, Texas (2004)
- [4] Akers, T.J.: Salinity-based pump-and-dump strategy for drilling salt with supersaturated Fluids. *SPE Drill and Compl.* 26(1), 1-9 (2011). <https://doi.org/10.2118/128405-PA>
- [5] Jia, H.; Hu, Y.X.; Zhao, S.J.; Zhao, J.Z.: The feasibility for potassium-based phosphate brines to serve as high-density solid-free well-completion fluids in high temperature/ high-pressure formations. *SPE Journal*. 24(5), 1-14 (2019). <https://doi.org/10.2118/194008-PA>
- [6] Amer, A.; Dearing, H.; Jones, R.; Sergiacomo, M.: Drilling through salt formations: a drilling fluids review. In: SPE-180326-MS presented at deepwater drilling and completions conference, Galveston, Texas (2016). <https://doi.org/10.2118/180326-MS>
- [7] Jin, C.P.; Ma, G.C.; Wang, C.S.; Ou, Y.W.; Li, W.; He, H.; Wang, L.; Wang, X.B.: The Application of Polymer-sulfonated Saturated Salt Based Mud System on the Right Bank of the Amu Darya in Turkmenistan. In: IADC/SPE Asia Pacific Drilling Technology Conference and Exhibition, Society of petroleum engineers (2012). <https://doi.org/10.2118/155685-MS>
- [8] Kemp, N.P.: Mutual solubility of salts in drilling and completion fluids. *SPE Drilling Engineering*. 5(1), 21-26 (1990). <https://doi.org/10.2118/16688-MS>
- [9] Knox, D.; Bye, G.K.; Horton, R.; Svoboda, C.; Foxenbr, W.; Tresco, K.: Application of a novel, high-density, brine-based, biopolymer-free reservoir drilling fluid: a case study. In: SPE-73765-MS presented at International symposium and exhibition on formation damage control, Lafayette, Louisiana (2002). <https://doi.org/10.2118/73765-MS>
- [10] Aizuddin, S.; Ahmad, K.I.: Effects of surfactant-polymer formulation and salinities variation towards oil recovery. *Arab. J. Sci. Eng.* 39, 4251-4260 (2014). <http://doi.org/10.1007/s13369-014-1025-7>

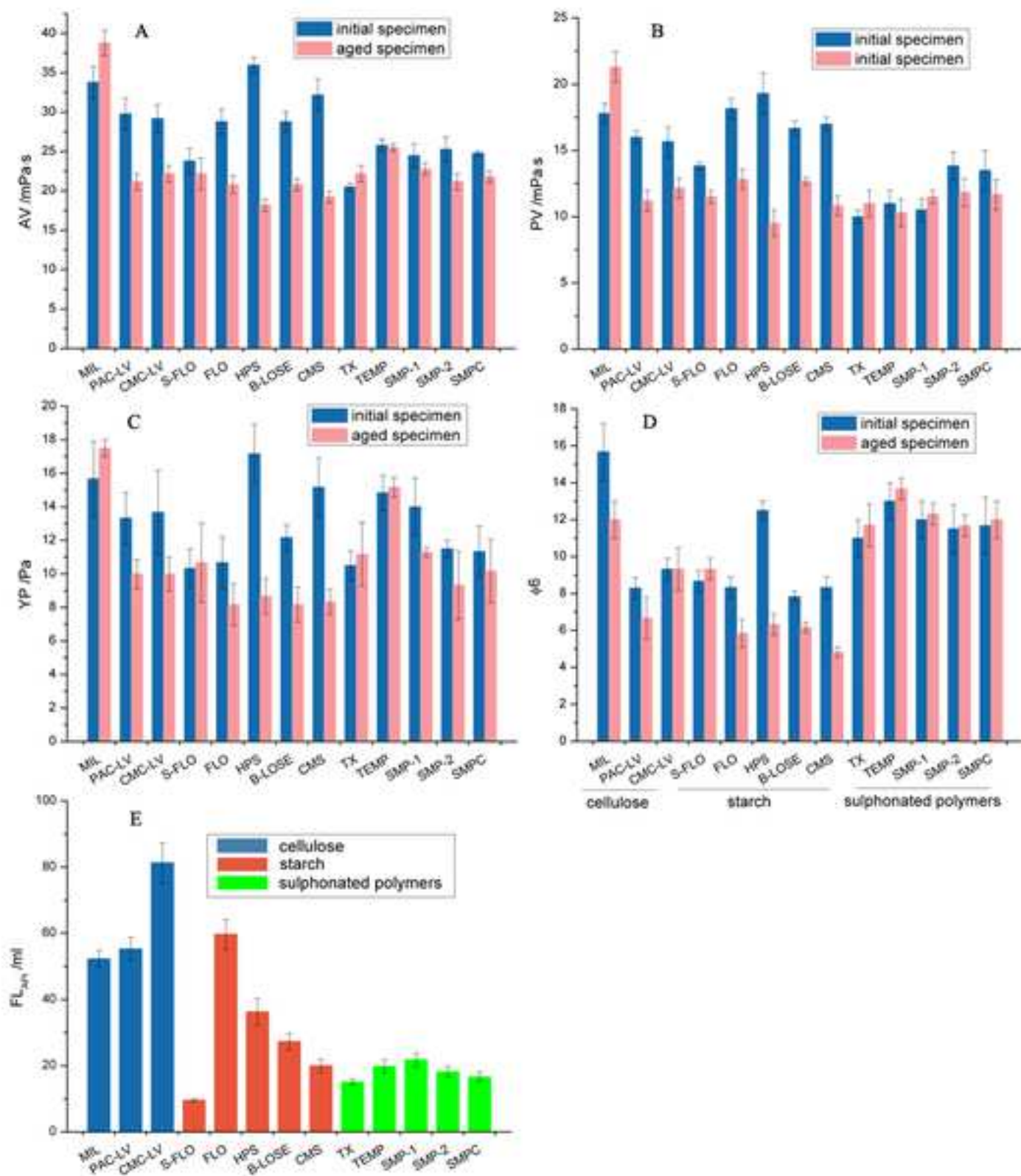
- 1 [11] Zhou, H.; Deville, J.P.; Davis CL. Novel thermally stable high-density brine-based drill-in  
2 fluids for HP/HT application. In: SPE-172659-MS presented at SPE Middle East Oil & Gas  
3 Show and Conference, Manama, Bahrain (2015). <https://doi.org/10.2118/172659-MS>  
4  
5  
6 [12] Salkla, T.; Mahto, V. Experimental investigations and optimizations of rheological behavior  
7 of drilling fluids using RSM and CCD for Gas hydrate-bearing formation. Arab. J. Sci. Eng. 43,  
8 6541-6554 (2018). <http://doi.org/10.1007/s13369-018-3292-1>  
9  
10 [13] Wajheuddin, M.; Hossain, M.E.: Development of an environmentally-friendly water-based  
11 mud system using natural materials. Arab. J. Sci. Eng. 43, 2501-2513 (2018).  
12 <http://doi.org/10.1007/s13369-017-2583-2>  
13  
14 [14] Xie, C.L.; Wang, Z.Y.; Qiu, Y.; Gou, G.z.; Gao, J.F.; Yin, G.; Wu, Y.: Safe Drilling  
15 Technology of High Pressure Salt Paste Formation in Halfaya Oilfield, Iraq. Journal of Jilin  
16 University(Earth Science Edition). 50(2), 589-597 (2020).  
17 <http://xuebao.jlu.edu.cn/dxb/CN/Y2020/V50/I2/589>  
18  
19 [15] Lin, W.J.; Huang, Z.Y.; Zhuang, Y.D.: Maintenance technology of high-density saturated brine  
20 drilling fluid during drilling into salt-gypsum layer. Natural Gas Exploration & Development.  
21 34(1), 64-67 (2011)  
22  
23 [16] Yang, P.; Lv, K.H.; Zhen, P.P.; Hong, W.: Laboratory research on saturated salt water based  
24 clay-free drilling fluids with thermal stability. Oilfield Chemistry. 4, 482-485 (2013).  
25 <http://doi.org/10.19346/j.cnki.1000-4092.2013.04.002>  
26  
27 [17] Hu, W.J.; Luo, P.Y.; Bai, Y.; Lin, L.: Study on a new high temperature high density saltwater  
28 drilling fluid. Drilling Fluid & Completion Fluid. 34(3), 1-10 (2017).  
29 <http://doi.org/10.3969/j.issn.1001-5620.2017.03.001>  
30  
31 [18] Li, J.; Zhao, C.X.; Lv, E.C.; Hu, J.P.; Xu, G.H.: Characteristics of formate and organic salt  
32 base fluid. Drilling Fluid and Completion Fluid. 28(4), 72-77 (2011)  
33  
34 [19] Yang, Z.; Zhang, X.; Yu, J.; Xu, W.: Effects of aging on the multiscale properties of SBS-  
35 modified asphalt. Arab. J. Sci. Eng. 44, 4349-4358 (2019). <http://doi.org/10.1007/s13369-018-3399-4>  
36  
37 [20] Elkatatny, S.: Enhancing the rheological properties of water-based drilling fluid using  
38 micronized starch. Arab. J. Sci. Eng. 44: 5433-5442 (2019). <http://doi.org/10.1007/s13369-019-3399-4>  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

03720-1

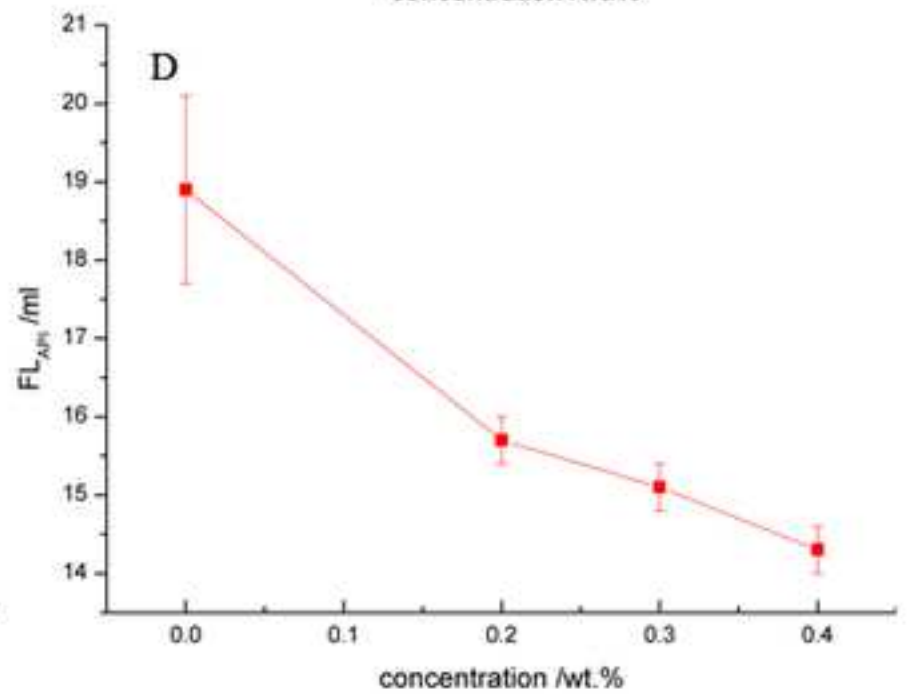
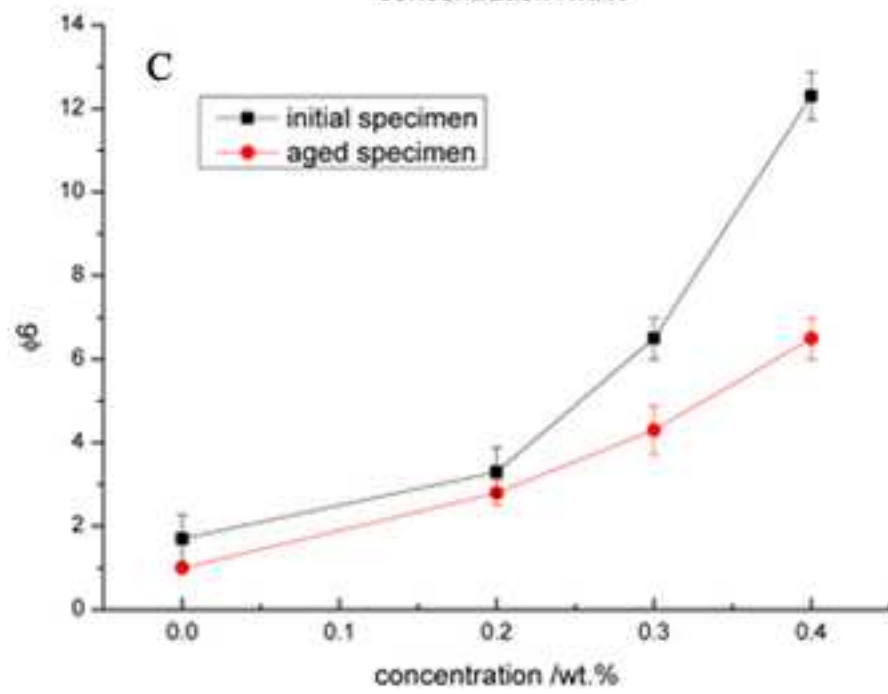
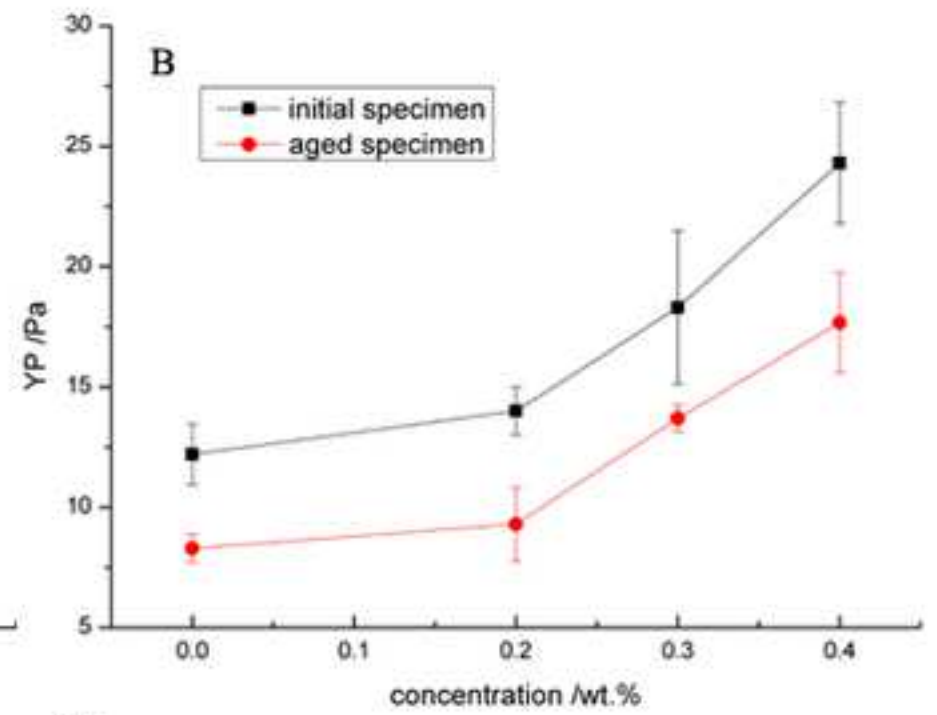
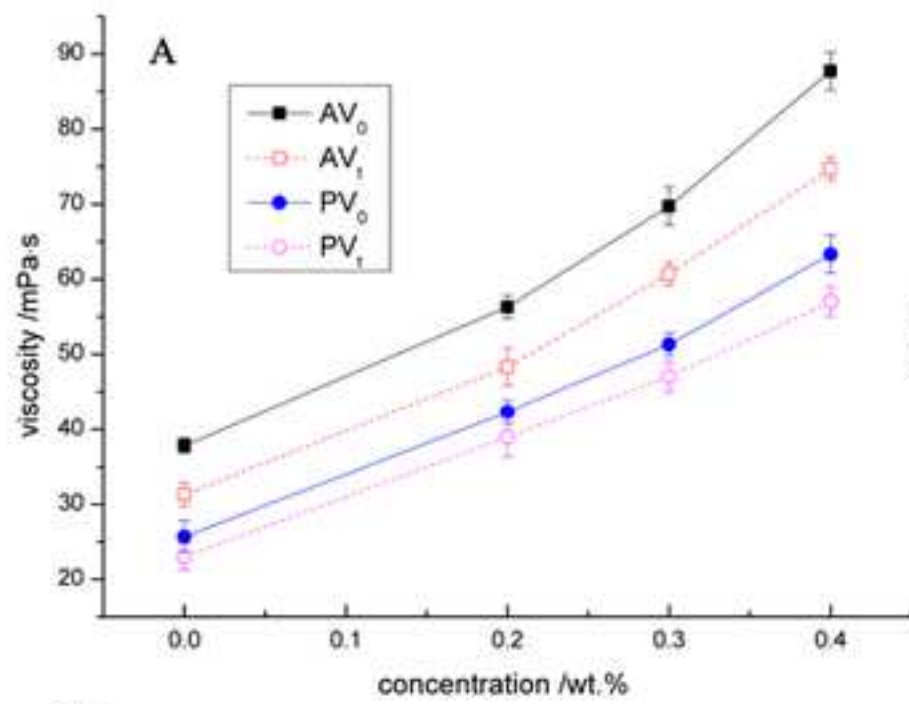
- 1  
2  
3 [21] Hakiki, F.; Maharsi, D.A.; Marhaendrajana, T.: Surfactant-polymer coreflood simulation and  
4 uncertainty analysis derived from laboratory study. *Journal of Engineering and Technological*  
5 *Sciences*. 47(6), 706-725 (2015). <http://doi.org/10.5614%Fj.eng.technol.sci.2015.47.6.9>  
6  
7  
8  
9 [22] Hakiki, F.; Salam, D.D.; Akbari, A.; Nuraeni, N.; Aditya, W.; Siregar, S. Is epoxy-based  
10 polymer suitable for water shut-off application? In: SPE-176457-MS presented at SPE/IATMI  
11 Asia Pacific Oil & Gas Conference and Exhibition, Bali, Indonesia (2015).  
12 <https://doi.org/10.2118/176457-MS>  
13  
14  
15 [23] Sreekumar, P.A.; Elanamugilan, M.; Singha, N.K.; Al-Harithi, M.A.; De, S.K.; Al-Juhani, A.:  
16 LDPE filled with LLDPE/starch materbatch: rheology, morphology and thermal analysis. *Arab.*  
17 *J. Sci. Eng.* 39: 8491-8489 (2014). <http://doi.org/10.1007/s13369-014-1467-y>  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65













Dear Reviewers:

We are truly grateful to your critical comments and thoughtful suggestions. Based on these comments and suggestions, we have made careful modifications on the original manuscript and, in particular, the section of “result and discussion” has been partially rewritten. Below you will find our point-by-point responses to the comments (or questions). In the paper, all the modified parts are marked in red.

## **Response to comment:**

### **Reviewer #1**

#### **Comment 1:**

Fig 1:

- Please explain in the caption what do the color codes mean? - Green, yellow, white boxes and the lines.
- Please put all abbreviations in the caption as well even though you have already mentioned them in the paper, e.g. SDF.
- Put space in before ( to be saline drilling fluid (SDF).
- AIM equals to purpose?
- No need all capital if it is not an abbreviation. - Start all word with capital (standardize them)

**Response:** According to this advice, Fig.1 has been re-presented, and the improper caption has been modified; the color code has been remarked and explained for better understanding; all abbreviations involved in the paper have been elucidated; space has been added;

#### **Comment 2:**

Fig 2: Please show the error bars. State in the caption the repeatability. Please put in the caption the full name of each chemicals (abbreviations).

**Response:** According to this advice, some experiments have been complemented, and error bars have been given in Fig. 2 to state the repeatability. The abbreviations of chemicals are the industrial codes, and they have been introduced in Table 1.

**Comment 3:**

Fig 3:

- Please show the error bars. State in the caption the repeatability.
- So, black and red refer to left? Put arrow - Write the word legend next to the curve (no need inside a box)
- Legend must use same color as the curve color

**Response:** According to these advices, Fig.3 has been reconstructed in the form of bar error. Some improper description has been eliminated. Some detailed information can be found in P14.

**Comment 4:**

I found many () or [] and you do not use space before ( or [. Please give a space.

**Response:** According to this advice, we checked the paper and the lost space has been added before all () or [].

**Comment 5:**

Please move all Tables 2-5 into a SUPPLEMENTARY INFORMATION (SI). Show in the paper as figures or bar charts; with known error bar and repeatability.

**Response:** According to this advice, Tables 2-5 have been provided as a supplementary information together with complementary experiments, and some key information such as rheological and filtrate data has been given in the form of bar chart. The detailed description can be found in the section “results and discussion” in P8-P15.

**Comment 6:**

Please consider more papers >7 from this journal itself. What is the suitability merit to get published here if there is no attachment of references to this journal itself?

**Response:** Arab. J. Sci. Eng. has involved limited papers on brine drilling fluid system. According to your advice, we have made an effort to cite 6 papers that are contacted with the present work from this journal.

**Comment 7:**

Please note that the presence of salts may break the polymer or viscosifier chain and results in a lower viscosity; and viscosity increases with increasing polymer concentrations due to the increasing intermolecular entanglement.

**Response:** According to this advice, we have provided simple description on relation of polymer concentration and intermolecular effect, and cited Hakiki's work.

**Comment 8:**

Please note that the viscosity of fluids is shear-rate dependent. Please declare not only the unit mPa.s but also measured at what shear rate? (1/s)

**Response:** As for rheological property of drilling fluids, the viscosity is always tested with a 6-speed rotator apparatus, which can exhibit relation between viscosity and shear rate. To clarify this point, we have supplied the experimental process in P6.

**Comment 9:**

Regarding comment #7 and #8 above, please cite and consider these papers in your references: - Hakiki, F, Maharsi, DA, Marhaendrajana, T. 2015. Surfactant-polymer coreflood simulation and uncertainty analysis derived from laboratory study. Journal of Engineering and Technological Sciences 47 (6), 706-725. DOI:

<http://dx.doi.org/10.5614%2Fj.eng.technol.sci.2015.47.6.9> - Hakiki et al. 2015. Is Epoxy-Based Polymer Suitable for Water Shut-Off Application? SPE-176457-MS.  
DOI: <https://doi.org/10.2118/176457-M>

**Response:** These two papers are instructive to our work, and we have cited them in the section of “screening of viscosifier”.

**Comment 10:**

Make sure all references are mentioned in the paper passage and also provide the DOI link (if any).

**Response:** all references have been mentioned, and the DOI link (if any) has been provided.

**Comment 11:**

In the optimization process, please show in new figures the variables you played with.

**Response:** New figures linked with the optimization process were presented in “results and discussion”.

**Comment 12:**

So, which one is the best viscosifier, filtrate reducer, and VIS content? At what concentrations? Could you please create a 3D map optimization? Please give a case study with a given reservoir properties to handle with.

**Response:** The advice would be helpful to explicitly determine the optimized ingredient, but it will inevitably demand a large quantity of experiments. To meet the requirement on-site, a single-factor experiment is enough and moderate, which is also cost-effective in building appropriate formula. Using the single-factor method, we

attained the optimized formula of saturated SDF: fresh water+ 0.25 wt.% Na<sub>2</sub>CO<sub>3</sub> + 0.10 wt.% NaOH + (30 wt.% NaCl + 6 wt.% KCl + 8 wt.% HCOONa) mixed-salt water+ 3.0 wt.% S-FLO + 0.2 wt.% VIS + barite (1.23 s.g.).

In addition, according to the advice, the title of paper has been modified as “Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq”

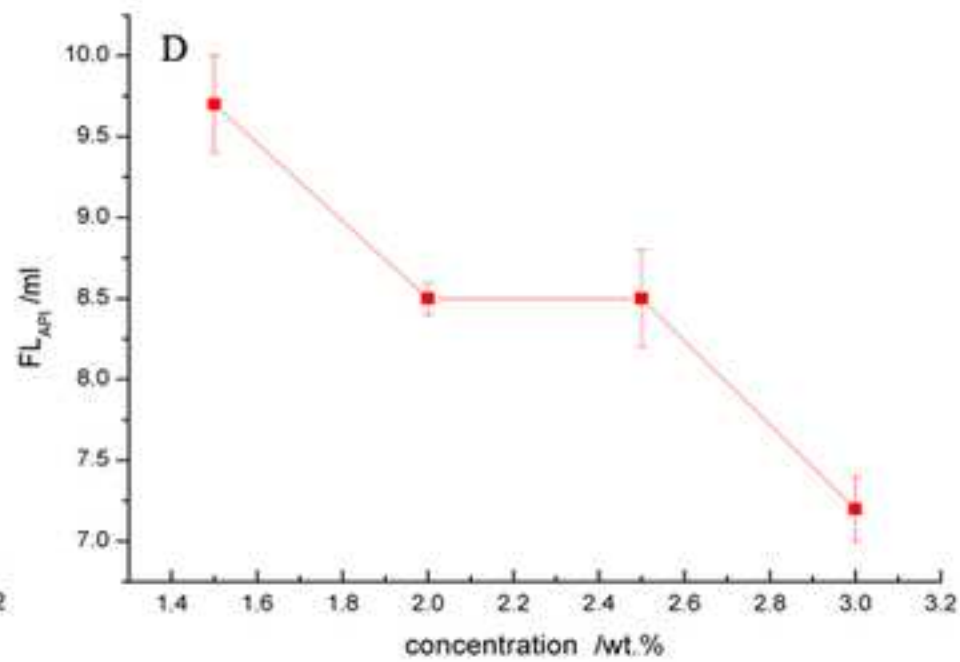
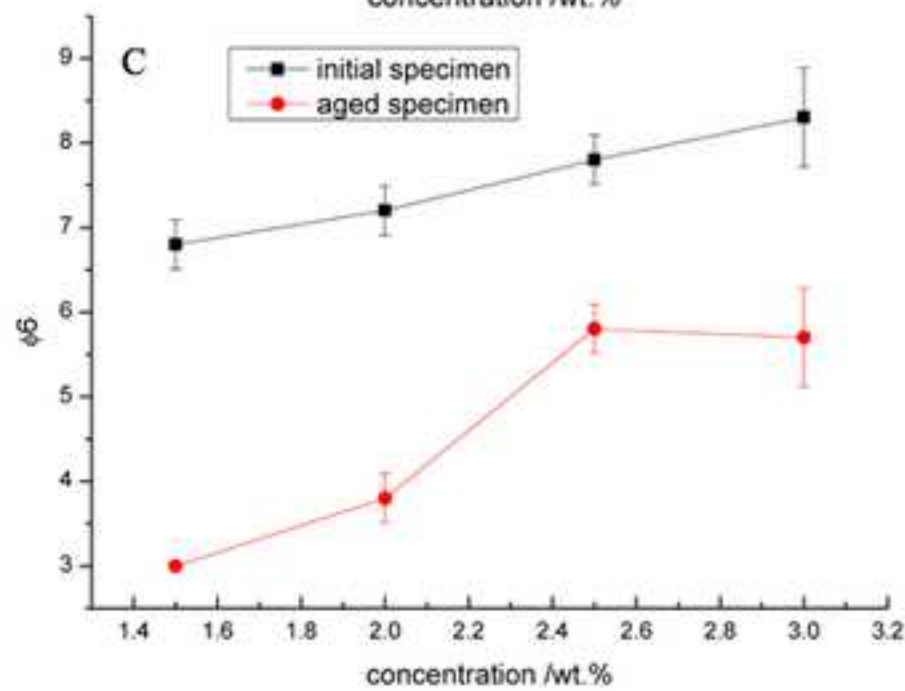
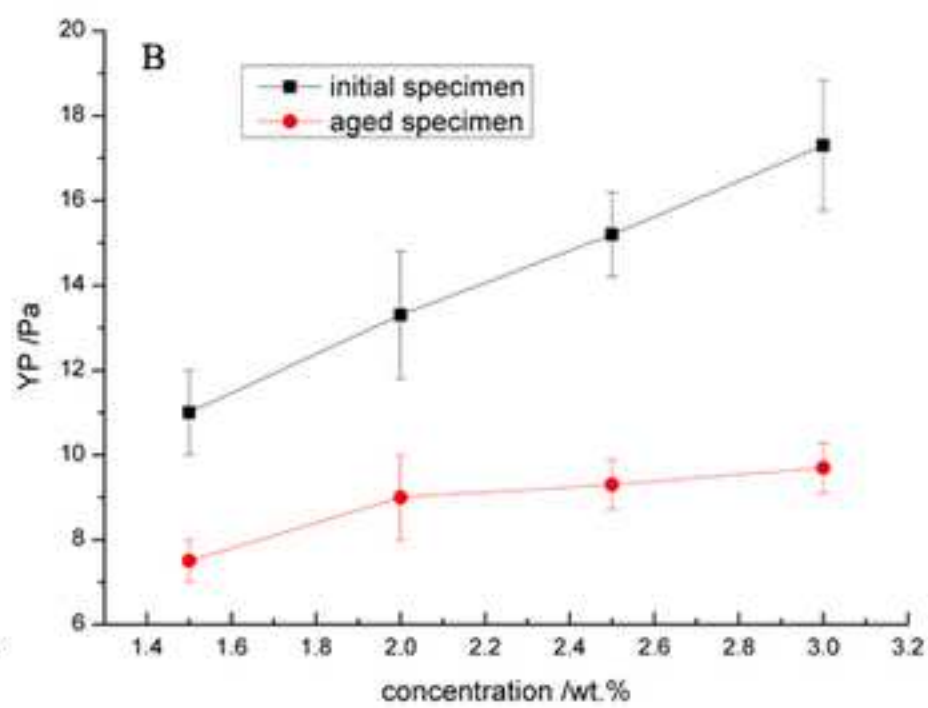
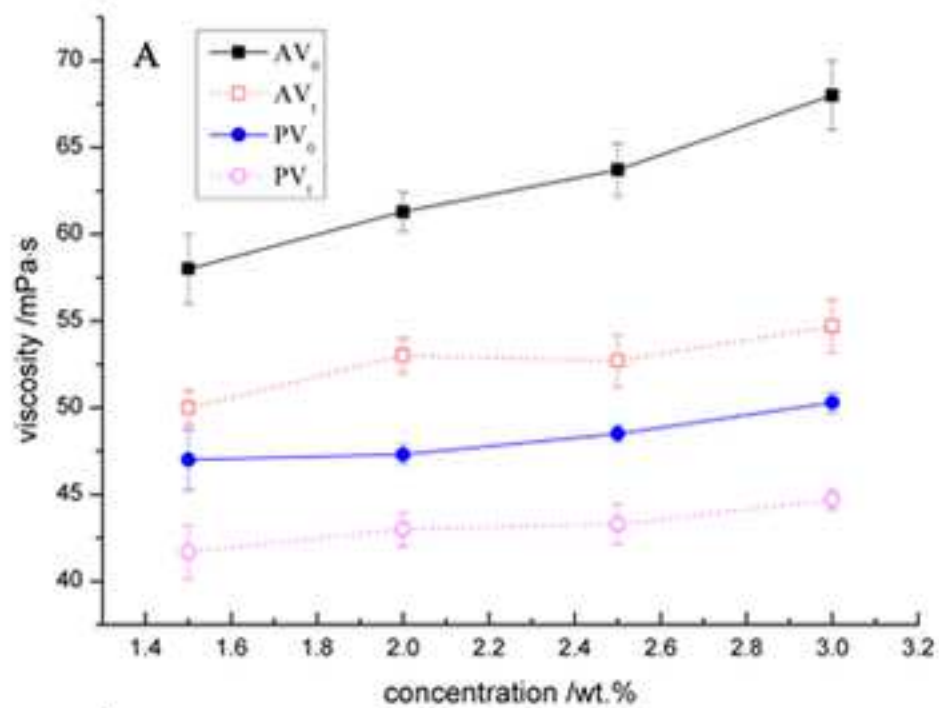
## **Reviewer #2**

**Comment 1:** The experimental part should be supplemented with a description of the experimental procedure used to analyze the dispersion of the drilling fluid, that is, measuring viscosity and fluid loss.

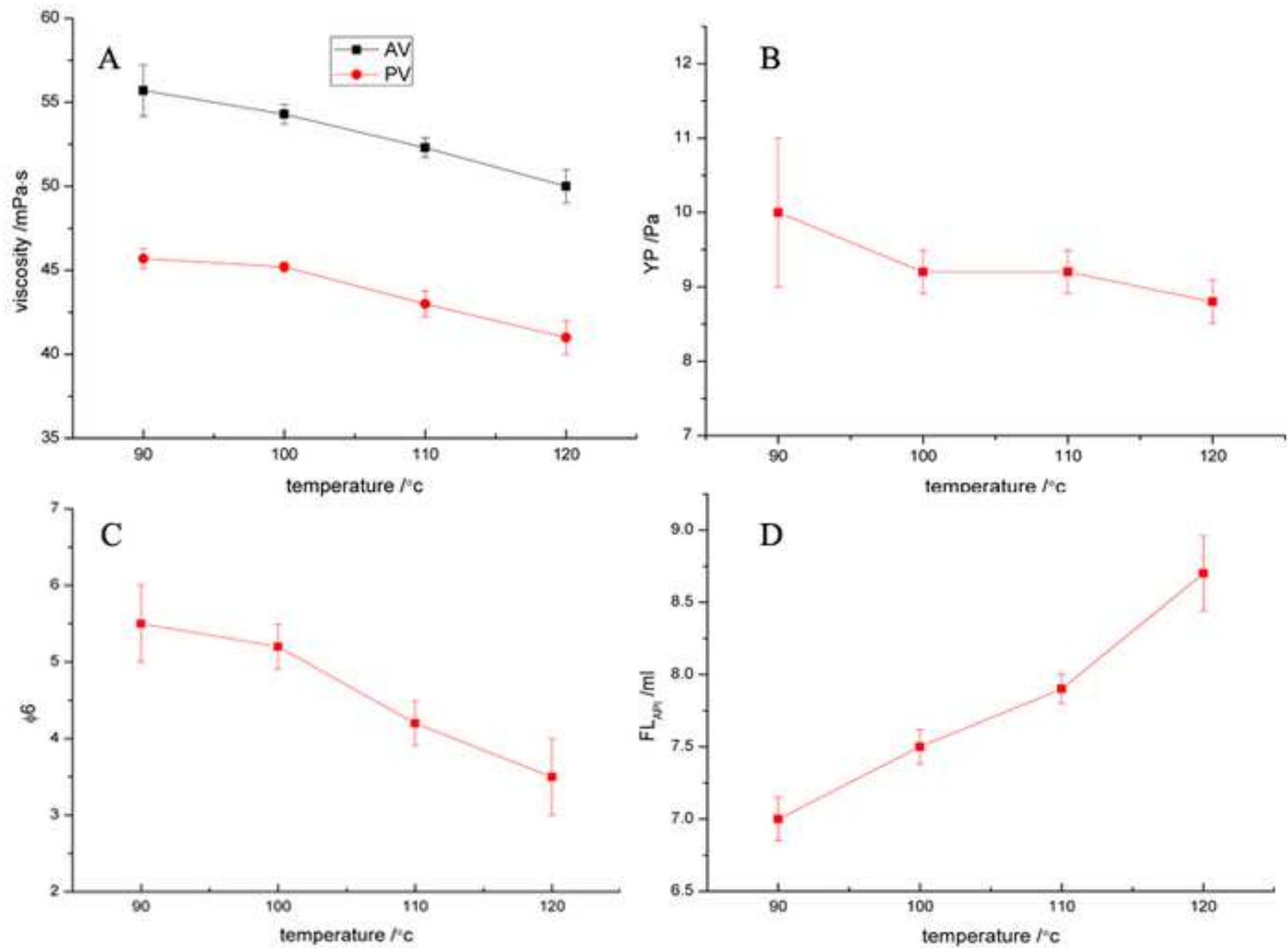
**Response:** According to this helpful advice, we have complemented experimental procedure.

**Comment 2:** The article also presents a wide range of different thickeners and filtrate reducing agents. The composition of all types of additives should be described or referred to.

**Response:** All types of additives are commercially used in petroleum industry, and we presented a description on additive composition in Table 1.



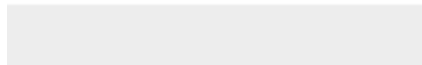






Click here to access/download

**Supplementary Material (Text)**  
Supplementary information.docx



# Change of authorship request form (pre-acceptance)

## Please read the important information on page 4 before you begin

This form should be used by authors to request any change in authorship including changes in corresponding authors. Please fully complete all sections. Use black ink and block capitals and provide each author's full name with the given name first followed by the family name.

Please note: In author collaborations where there is formal agreement for representing the collaboration, it is sufficient for the representative or legal guarantor (usually the corresponding author) to complete and sign the Authorship Change Form on behalf of all authors.

### Section 1: Please provide the current title of manuscript

(For journals: Please provide the manuscript ID, title and/or DOI if available.)

(For books: Please provide the title, ISBN and/or DOI if available.)

<b>Manuscript ID no. in case of unpublished manuscript:</b>
---

<b>DOI in case of published manuscript:</b>
---

<b>ISBN (for books):</b>
--------------------------

Title: Experimental Investigation into A Novel Supersaturated Saline Drilling Fluid Available in Anhydrite Formation: A Case study of Missan Oilfield, Iraq
---

### Section 2: Please provide the previous authorship, in the order shown on the manuscript before the changes were introduced. Please indicate the corresponding author by adding (CA) behind the name.

	First name(s)	Family name	ORCID or SCOPUS id, if available
1 <sup>st</sup> author	Lin	Xu	
2 <sup>nd</sup> author	Jie	Xu	
3 <sup>rd</sup> author	Fuchang	You	
4 <sup>th</sup> author	Mingbiao	Xu	
5 <sup>th</sup> author	Jun	Gao	
6 <sup>th</sup> author	Meilan	Huang	
7 <sup>th</sup> author			

Please use an additional sheet if there are more than 7 authors.

## Change of authorship request form (pre-acceptance)

**Section 3: Please provide a justification for change. Please use this section to explain your reasons for changing the authorship of your manuscript, e.g. what necessitated the change in authorship? Please refer to the (journal) policy pages for more information about authorship. Please explain why omitted authors were not originally included and/or why authors were removed on the submitted manuscript.**

Complementary work was mainly carried out by Xin Huang and, thus, Huang was listed as the second author for her contribution, which have been agreed by co-authors.

**Section 4: Proposed new authorship. Please provide your new authorship list in the order you would like it to appear on the manuscript. Please indicate the corresponding author by adding (CA) behind the name. If the corresponding author has changed, please indicate the reason under section 3.**

	First name(s)	Family name (this name will appear in full on the final publication and will be searchable in various abstract and indexing databases)
1 <sup>st</sup> author	Lin	Xu
2 <sup>nd</sup> author	Xin	Huang
3 <sup>rd</sup> author	Fuchang	You
4 <sup>th</sup> author	Jie	Xu
5 <sup>th</sup> author	Mingbiao	Xu
6 <sup>th</sup> author	Jun	Gao
7 <sup>th</sup> author	Meilan	Huang

Please use an additional sheet if there are more than 7 authors.

## Change of authorship request form (pre-acceptance)

**Section 5: Author contribution, Acknowledgement and Disclosures.** Please use this section to provide a new disclosure statement and, if appropriate, acknowledge any contributors who have been removed as authors and ensure you state what contribution any new authors made (if applicable per the journal or book (series) policy). **Please ensure these are updated in your manuscript - after approval of the change(s) - as our production department will not transfer the information in this form to your manuscript.**

**New acknowledgements:**

**New Disclosures (financial and non-financial interests, funding):**

**New Author Contributions statement (if applicable per the journal policy):**


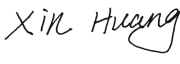

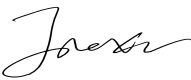



Xin Huang, as a new author, has completed most complementary experiments linked with reviewers' advices.

State 'Not applicable' if there are no new authors.

# Change of authorship request form (pre-acceptance)

**Section 6: Declaration of agreement. All authors, unchanged, new and removed *must* sign this declaration.**

**(NB: Please print the form, sign and return a scanned copy. Please note that signatures that have been inserted as an image file are acceptable as long as it is handwritten. Typed names in the signature box are unacceptable.)** \* Please delete as appropriate. Delete all of the bold if you were on the original authorship list and are remaining as an author.

	First name	Family name		Signature	Affiliated institute	Date
1 <sup>st</sup> author	Lin	Xu	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		Zhejiang Ocean University	July 17 2020
2 <sup>nd</sup> author	Xin	Huang	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		China University of Petroleum (Beijing)	July 17 2020
3 <sup>rd</sup> author	Fuchang	You	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		Jiahua Technology Co., Ltd Yangtze University	July 17 2020
4 <sup>th</sup> authors	Jie	Xu	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		Chinese Academy of Geological Sciences	July 17 2020
5 <sup>th</sup> author	Mingbiao	Xu	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		Yangtze University	July 17 2020
6 <sup>th</sup> author	Jun	Gao	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		CNOOC (China) Co., Ltd, Shanghai Branch	July 17 2020
7 <sup>th</sup> author	Meilan	Huang	I agree to the proposed new authorship shown in section 4 /and the <b>addition/removal*of my name to the authorship list.</b>		Queen's University Belfast	July 17 2020

Please use an additional sheet if there are more than 7 authors.

### Important information. Please read.

- Please return this form, fully completed, to Springer Nature. We will consider the information you have provided to decide whether to approve the proposed change in authorship. We may choose to contact your institution for more information or undertake a further investigation, if appropriate, before making a final decision.
- By signing this declaration, all authors guarantee that the order of the authors are in accordance with their scientific contribution, if applicable as different conventions apply per discipline, and that only authors have been added who made a meaningful contribution to the work.
- Please note, we cannot investigate or mediate any authorship disputes. If you are unable to obtain agreement from all authors (including those who you wish to be removed) you must refer the matter to your institution(s) for investigation. Please inform us if you need to do this.
- If you are not able to return a fully completed form within **30 days** of the date that it was sent to the author requesting the change, we may have to withdraw your manuscript. We cannot publish manuscripts where authorship has not been agreed by all authors (including those who have been removed).
- Incomplete forms will be rejected.